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ABSOLUTE \underline{k} -STABILITY OF LINEAR DISTRIBUTED n-PORTS

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Abstract

This paper considers exclusively linear time-invariant distributed n-ports specified by a convolution operator: $b = S * a$. It defines I/O stability in the time-domain and characterizes it for a broad class of such n-ports. It characterizes absolutely stable n-ports. Finally, it defines absolute k-stability - i.e. stability of given n-port under any loading by passive k_1 -ports, k_2 -ports, \dots , k_r -ports, where $k_1 + k_2 + \dots + k_r = n$. The necessary and sufficient conditions for absolute k -stability are obtained using Doyle's μ functional. The paper is self contained.

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1. Introduction

The problem of determining conditions under which a lumped active n -port is stable when each one of its ports is terminated by an arbitrary linear passive 1-port has long been studied. A considerable amount of the literature on this subject is devoted to the special case of linear lumped 2-ports [De. 1], [Woo. 1], [Kuh 1]. Youla in [You. 1] obtained necessary and sufficient conditions (n.a.s.c.) working with impedance matrices and later, in [You. 2], n.a.s.c. in terms of the scattering matrix of the n -port. [Zeh. 1] contains a different set of n.a.s.c. using the impedance matrix.

In this paper we generalize the classical problem in two directions by considering distributed n -ports and by allowing a less restrictive class of terminations. We consider exclusively linear, time-invariant, causal, active n -ports characterized by Laplace transformable convolution operators [Sch. 1], [Zem. 1], [Des. 1], [Vid. 1]; and define the I/O-stability in terms of I/O time-domain concepts in section 2. For a general class of such n -ports we characterize those that are stabilizable and those that are absolutely stable in section 3. In section 4 we define the new concepts of k -terminations and absolute k -stability and, finally, in section 5, using the function μ_k recently defined in [Doy. 1], we obtain necessary and sufficient conditions for the absolute k -stability of a class of distributed n -ports.

Notation

$a := b$ means a denotes b ; \mathbb{R} is the field of real numbers, \mathbb{C} is the field of complex numbers; \mathbb{R}_+ is the set of non-negative real numbers; \mathbb{C}_+ ($\mathbb{C}_{\sigma,+}$) is the set of complex numbers such that $\text{Re } z \geq 0$ ($\text{Re } z \geq \sigma$, respectively). For any positive integer k , $\underline{k} := \{1, 2, \dots, k\}$. For any

set A , $A^{n \times n}$ denotes the class of all $n \times n$ arrays with elements in A , and $\overset{\circ}{A}$ denotes the interior of A . $\mathbb{R}_p(s)$ denotes the class of all proper rational functions with coefficients in \mathbb{R} . For any $A \in \mathbb{C}^{m \times n}$, $\bar{\sigma}[A]$ is the $\sigma_{\max}[A]$, the maximum singular value of A . Given $\sigma \in \mathbb{R}$ (typically $\sigma > 0$), $f \in \mathcal{A}(\sigma)$ iff $f(t) = f_a(t) + \sum_0^{\infty} f_i \delta(t-t_i)$, where $f_a : \mathbb{R} \rightarrow \mathbb{R}$, with $f_a(t) = 0$ for $t < 0$ and $t \mapsto \exp(-\sigma t) f_a(t) \in L_1$; $t_0 = 0$, $t_i > 0$, $\forall i > 0$; $\forall i$, $f_i \in \mathbb{R}$ and $i \mapsto f_i \exp(-t_i) \in \ell_1$; $f \in \mathcal{A}_-(\sigma)$ iff, for some $\sigma_1 < \sigma$, $f \in \mathcal{A}(\sigma_1)$. \hat{f} denotes the Laplace transform of f . $\mathcal{A} := \mathcal{A}(0)$, $\mathcal{A}_- := \mathcal{A}_-(0)$ $\hat{\mathcal{A}} := \{\hat{f} : f \in \mathcal{A}\}$, $\hat{\mathcal{A}}_- := \{\hat{f} : f \in \mathcal{A}_-\}$. W.r.t. means "with respect to." U.t.c. means "under these conditions." W.l.o.g. means "without loss of generality."

2. Input-output -- stable linear time-invariant n-ports

2.1. Description of linear time-invariant n-ports and definition of I/O-stability.

We will view linear time-invariant n-ports as being represented by convolution operators. In order to do this, given an n-port \mathcal{N} , we choose n positive resistors r_1, \dots, r_n with respect to which the scattering matrix of \mathcal{N} , S , may be defined. To appreciate the generality of this point of view, recall that L. Schwartz has shown [Sch. 1, p. 162, 197] that any linear time-invariant operator that satisfies some slight continuity properties has a representation of the form $a \mapsto \check{S} * a$, where $\check{S}(t)$ is a distribution. In the context of this paper, $S(s) = \mathcal{L}[\check{S}(t)]$ is the scattering matrix of the n-port under consideration, a the incident wave and $b = \check{S} * a$, the reflected wave. \check{S} is a causal convolution kernel iff it is supported on \mathbb{R}_+ . We make the following assumption:

A.1: The linear time-invariant n-port is causal and is represented by a convolution operator \check{S} , and \check{S} is Laplace transformable.

We adopt the following definition of stability:

Definition: An n-port is said to be I/O-stable iff

i) for all $p \in [1, \infty]$, it takes an L_p -input, a , into an L_p -output, b , with a finite gain; equivalently for some $M < \infty$, $\|b\|_p < M\|a\|_p$;

ii) it takes continuous and bounded inputs (periodic inputs, almost periodic inputs, resp.) into outputs belonging to the same class, respectively.

Comment: In contrast to many authors [You. 1], [Zeh. 1], we do not define stability in terms of frequency domain concepts: first, stability is a time-domain concept; second, it is only for transfer functions that are known to be proper and rational that analyticity in the closed right half-plane (\mathbb{C}_+) is equivalent to exponential stability and to the requirements i) and ii) above. (For a proof of this fact, see [Cal. 1, p. 124]).

For example, the time-functions $f_1(t) := t^n e^t \sin(e^t)$; $f_2(t) := t^n \sin(t^\alpha)$ — where $n \in \mathbb{N}$, $\alpha > 1$ — have Laplace transforms that are analytic everywhere in \mathbb{C} (except at ∞). (Such time-functions have Laplace transforms that are not proper rational functions. The network functions of distributed circuits are, in general, not rational functions either). Since both $f_1(\cdot)$ and $f_2(\cdot)$ are unbounded on \mathbb{R}_+ and do not belong to $L_1(\mathbb{R}_+)$, these time-functions cannot be associated with "stable" circuits. Hence, for distributed circuits, the conventional definition of stability, based on analyticity in \mathbb{C}_+ , is totally inappropriate.

To alleviate technical difficulties, we forego a slight extension and make the following assumption:

A2: The kernel, $\overset{v}{S}(\cdot)$, (equivalently, the measure) representing an I/O-stable n-port has no singular continuous part.

Fact 2.1: Let the n-port \mathcal{N} , described by S , be I/O-stable and let it satisfy A1, A2; then $\overset{V}{S}(\cdot) \in \mathcal{A}^{n \times n}$.

Proof: A1 and I/O-stability give that $b = \overset{V}{S}a$ and $S^* : a \mapsto b$ maps L_p to L_p , $\forall p \in [1, \infty]$. Thus, by the Riesz representation theorem [Rud. 1] S can be represented by a measure. This measure is supported on \mathbb{R}_+ , by A1. From A2, $\overset{V}{S}(t) \in \mathcal{A}^{n \times n}$.

2.2. Interconnection of n-ports and transfer functions

Let an n-port \mathcal{N} be loaded by an n-port, \mathcal{N}_ℓ . If the interconnection of \mathcal{N} and \mathcal{N}_ℓ is driven in parallel (series) by current (voltage) sources, it is called \mathcal{N}_{t_i} (\mathcal{N}_{t_e}). See Fig. 1 (Fig. 2).

We call the interconnection of \mathcal{N} and \mathcal{N}_ℓ , \mathcal{N}_{t_i} in Fig. 1 and \mathcal{N}_{t_e} in Fig. 2. S_ℓ will be the scattering matrix representing the "load" n-port \mathcal{N}_ℓ and S the scattering matrix of \mathcal{N} . For the \mathcal{N}_{t_e} of Fig. 2 we may write the following equations in the frequency domain:

$$\begin{aligned} a_\ell + b_\ell + e &= a + b \\ a_\ell - b_\ell &= -a + b \\ b_\ell &= S_\ell a_\ell \\ b &= Sa \end{aligned}$$

In order to eliminate a_ℓ and b_ℓ ; we add (subtract resp.) the first 2 eqns. to get

$$a = b - \frac{e}{2} \quad (b = a - \frac{e}{2}, \text{ resp.}).$$

Using the last 2 equations we get,

$$(a - \frac{e}{2}) = S_\ell (b - \frac{e}{2})$$

and finally,

$$a = (I - S_\ell S)^{-1} (I - S_\ell) \frac{e}{2} \quad (2.2.0a)$$

$$b = Sa = S(I - S_\ell S)^{-1} (I - S_\ell) \frac{e}{2} \quad (2.2.0b)$$

A similar exercise may be carried out for π_{t_i} of Fig. 1. In summary, for the circuits of Figs. 1 and 2 we obtain the following transfer functions:

$$\pi_{t_i} \begin{cases} (I - S_\ell S)^{-1} (I + S_\ell) : i \mapsto a & (2.2.1a) \\ S(I - S_\ell S)^{-1} (I + S_\ell) : i \mapsto b & (2.2.1b) \end{cases}$$

$$\pi_{t_e} \begin{cases} (I - S_\ell S)^{-1} (I - S_\ell) : e \mapsto a & (2.2.1c) \\ S(I - S_\ell S)^{-1} (I - S_\ell) : e \mapsto b & (2.2.1d) \end{cases}$$

We will study the I/O-stability of interconnected n-ports π_{t_i} , π_{t_e} shown in Figs. 1 and 2. In order to do this, we make the following (technical) assumption: roughly speaking, we may state it as:

"For all $|s|$ "sufficiently large", $S(s)$ is analytic and bounded away from 1."

Let ρ be positive and large
and

$$M_\rho := \mathbb{C}_+ \cap \{s : |s| > \rho\}$$

Thus, we may state this assumption more precisely as follows:

A3: $\exists \rho > 0, \exists \epsilon > 0$ s.t. $\forall s \in M_\rho$, $S(s)$ is analytic and
 $\|S(s)\|_2 \leq 1 - \epsilon < 1$

(Here $\|S(s)\|_2$ is the ℓ_2 -induced norm of $S(s) \in \mathbb{C}^{n \times n}$.)

Comment: This is equivalent to assuming that the n-port represented by $S(s)$ is strictly passive in M_ρ [Kuh 1].

3. Stabilizability of linear time-invariant n-ports

3.1. Definition of stabilizability

Consider an n-port, \mathcal{N} , described by a scattering matrix $S(s)$ (with respect to some choice of positive normalizing resistances, $r_i > 0, i \in \underline{n}$). Let assumptions A1, A2 and A3 hold. We say that such an n-port is stabilizable iff there exists a lumped "load" n-port, \mathcal{N}_ℓ , (described by a scattering matrix $S_\ell(s) \in \mathbb{R}_p(s)^{n \times n}$ with respect to (the same) $r_i > 0, i \in \underline{n}$), such that i) \mathcal{N}_{t_e} and \mathcal{N}_{t_i} are I/O-stable and ii) each of the four transfer functions of (2.2.1) belong to $\hat{\mathcal{A}}^{n \times n}$.

Comment: This is a little stronger than just I/O-stability which would require that the four transfer functions of (2.2.1) each belong to $\hat{\mathcal{A}}^{n \times n}$.

Consider:

$$(I - S_\ell S)^{-1} \quad (3.1.1.a)$$

$$(I - S S_\ell)^{-1} \quad (3.1.1b)$$

$$S_\ell (I - S S_\ell)^{-1} \quad (3.1.1c)$$

$$S (I - S_\ell S)^{-1} \quad (3.1.1d)$$

The following algebraic fact is true:

Fact 3.1.1: Let \mathcal{M} be a commutative algebra. U.t.c. the four transfer functions of (2.2.1) belong to the matrix algebra $\mathcal{M}^{n \times n}$ iff the four transfer functions of (3.1.1) belong to the same matrix algebra $\mathcal{M}^{n \times n}$.

Note: In the context of this paper, \mathcal{M} is $\hat{\mathcal{A}}$ or $\hat{\mathcal{A}}_-$.

Proof: Note that $S(I - S_\ell S)^{-1} = (I - S S_\ell)^{-1} S$ and $I - (I - S S_\ell)^{-1} = S(I - S_\ell S)^{-1} S_\ell$. Then note that each of the 4 transfer functions of (2.2.1) is a linear combination of the 4 transfer functions of (3.1.1), and conversely. \square

Comments: a) Thus an n-port \mathcal{N} satisfying A1, A2, A3 is stabilizable iff there exists \mathcal{N}_ℓ (described by some $S_\ell \in \mathbb{R}_p(s)^{n \times n}$) such that the four transfer functions of (3.1.1) belong to $\hat{\mathcal{A}}_-^{n \times n}$.

b) Note that some 1-ports are not stabilizable by any stable 1-ports: e.g., $S(s) = \frac{2(s-1)}{(s+1)(s-2)}$ describes a 1-port that is not stabilizable by a stable 1-port.

It is now possible to detail a consequence of stabilizability.

Fact 3.1.2: Let the n-port \mathcal{N} satisfy A1, A2 and A3. U.t.c., if \mathcal{N} is stabilizable, then $S(s)$, the scattering matrix of \mathcal{N} w.r.t. some choice of normalizing resistors $r_i > 0$, $i \in \underline{n}$, has only a finite number of \mathbb{C}_+ -poles.

Proof: \mathcal{N} is stabilizable hence $\exists S_\ell(s) \in \mathbb{R}_p(s)^{n \times n}$ such that $(I - S_\ell S)^{-1}$, $(I - S S_\ell)^{-1}$, $S_\ell (I - S S_\ell)^{-1}$, $S(I - S_\ell S)^{-1} \in \hat{\mathcal{A}}_-^{n \times n}$. Let $H_1 := (I - S_\ell S)^{-1}$; $H_2 := S(I - S_\ell S)^{-1}$. Then $H_1, H_2 \in \hat{\mathcal{A}}_-^{n \times n}$ and $\det H_1 \in \hat{\mathcal{A}}_-$. Hence, for some $\epsilon > 0$, H_1, H_2 and $\det H_1$ are analytic and bounded in $\mathbb{C}_{-\epsilon, +}$.

$S_\ell(s)$ is bounded at ∞ since $S_\ell(s) \in \mathbb{R}_p(s)^{n \times n}$ and, by A3, $\exists \rho > 0$ such that $S(s)$ is bounded in M_ρ . Hence, $\det(I - S_\ell S) = \det[H_1^{-1}]$ is bounded in M_ρ . Since $\det[H_1^{-1}] = 1/\det H_1$ we conclude that $s \mapsto \det[H_1(s)]$ is bounded away from zero in M_ρ . We know that $s \mapsto \det[H_1(s)]$ is analytic in $\mathbb{C}_{-\epsilon, +}$ hence the zeros of $s \mapsto \det[H_1(s)]$ are isolated [Dieu. 1, Thm. 9.1.5] and do not belong to M_ρ . Now $\mathbb{C}_+ \setminus M_\rho$ is a compact set in the domain of analyticity of $\det H_1(s)$; consequently $\det H_1$ has only a finite number of zeros in $\mathbb{C}_+ \setminus M_\rho$. Now $(I - S_\ell S) = H_1^{-1}$ has a pole in \mathbb{C}_+ if and only if $\det[H_1(s)] = 0$. Since H_2 is analytic in $\mathbb{C}_{-\epsilon, +}$, $S = H_2 \cdot H_1^{-1}$ has only a finite number of \mathbb{C}_+ -poles. We may write

$$S(s) = \sum_{i=1}^{\ell} \sum_{k=0}^{m_i-1} r_{ik} (s-p_i)^{-m_i+k} + S_0(s), \text{ where } \operatorname{Re}(p_k) > -\epsilon < 0 \text{ and}$$

$$S_0(s) \in \hat{\mathcal{A}}_-^{n \times n}.$$

Comment: Suppose that, in Definition 3.1, we did not require ii).

Then by i) (I/O-stability), each of the four transfer functions of (3.3.1) would belong to $\hat{\mathcal{A}}^{n \times n}$ (but not necessary to $\hat{\mathcal{A}}_-^{n \times n}$) and we could then prove the following (weaker) version of Fact 3.

Let the n-port \mathcal{N} satisfy A1, A2, and A3. U.t.c., if \mathcal{N} is stabilizable, then, for any $\epsilon > 0$, $S(s)$ the scattering matrix of \mathcal{N} w.r.t. some choice of normalizing resistors $r_i > 0$, $i \in \underline{n}$, has only a finite number of $\mathbb{C}_{\epsilon+}$ -poles. The point is that there might be an infinite number of poles in \mathbb{C}_+ with an accumulation point in \mathbb{C}_+ on the $j\omega$ -axis.

3.2. Absolutely stable n-ports -- a characterization

Definition: An n-port is said to be absolutely stable iff the interconnections $\mathcal{N}_{t_e}, \mathcal{N}_{t_i}$ are I/O-stable for all lumped passive "load" n-ports, \mathcal{N}_ℓ .

Comments: a) Recall that the n-port \mathcal{N}_ℓ (described by $S_\ell(s)$) is lumped and passive $\Leftrightarrow S_\ell(s) \in \mathbb{R}_p(s)^{n \times n}$ and $\sup_{\text{Re}(s) \geq 0} \|S_\ell(s)\|_2 \leq 1$ [New. 1].

b) Consider the n-port \mathcal{N}_0 , described by S_0 . Then, $S_0(s) \in \mathbb{R}_p(s)^{n \times n}$ and $S_0(s)$ analytic in \mathbb{C}_+ and bounded on the $j\omega$ -axis imply that \mathcal{N}_0 is I/O-stable.

The following theorem characterizes absolutely stable n-ports.

Theorem 3.1: Let assumptions A1, A2, A3 hold for a distributed n-port, \mathcal{N} , described by a scattering matrix, $S(s)$. U.t.c. \mathcal{N} is absolutely stable iff

- i) $s \mapsto S(s)$ is analytic in \mathbb{C}_+ and bounded in \mathbb{C}_+ ;
- ii) $\forall \omega \in \mathbb{R}_+, \|S(j\omega)\|_2 < 1$.

Comments: a) Recall that in Fact 2.1.1 above, we have shown that satisfies A1, A2 and is I/O-stable iff $S(s) \in \hat{\mathcal{A}}^{n \times n}$; thus $\omega \mapsto S(j\omega)$ is bounded but the bound may be larger than 1.

b) In appendix 2 we exhibit a class of linear time-invariant distributed n-ports (more concretely specified in appendix 2, p.) which have scattering matrix in $\hat{\mathcal{A}}^{n \times n}$.

c) Theorem 3.1 is a generalization, to the distributed case, of a known theorem for the lumped case.

Proof: (\Rightarrow) Consider the particular interconnection, \mathcal{N}_{t_e} , in which \mathcal{N}_ℓ^R is the n-port of normalizing resistors (hence $S_\ell^R = 0$). Then, from eqn. (2.2.0a)

$$a = \frac{1}{2} e \quad \text{and} \quad b = S a = \frac{1}{2} S e; \quad \text{or, } 2b = S e .$$

I/O-stability implies that

$$\forall e \in L_2^n, \quad \frac{1}{2\pi} \int \|S(j\omega) e(j\omega)\|_2^2 d\omega = \|2b\|_2 \leq (\text{const.}) \|e\|_2,$$

hence $\omega \mapsto S(j\omega)$ is bounded on \mathbb{R}_+ . Now, \mathcal{N} absolutely stable implies, in particular, that \mathcal{N}_{t_e} is I/O-stable. Thus, $\forall \check{e}(t)$ s.t. $\check{e} \in L_2^n$ and $\text{supp}[\check{e}] \subset \mathbb{R}_+$, by I/O-stability $b \in L_2$ and b is analytic in \mathbb{C}_+ so that $S(s)$ must be analytic in \mathbb{C}_+ . And, by the theorem of the maximum, $S(s)$ is bounded in \mathbb{C}_+ . This proves i)

To prove ii) we use contradiction. Suppose that $\exists \omega_0 \in \mathbb{R}_+$ s.t. $\|S(j\omega_0)\|_2 = 1$.¹ The numerical matrix $S(j\omega_0)$ can be written as UH , where

¹A1, A2 and I/O-stab. for $\mathcal{N} \Rightarrow S(s) \in \hat{\mathcal{A}}^{n \times n} \Rightarrow \omega \mapsto S(j\omega)$ uniformly continuous on \mathbb{R} . Thus we can assume, $\exists \omega_0 \in \mathbb{R}_+$ s.t. $\|S(j\omega_0)\|_2 = 1$ w.l.o.g. for if $\exists \omega_1 \in \mathbb{R}_+$ s.t. $\|S(j\omega_1)\|_2 > 1$, then, the (uniform) continuity of $\omega \mapsto S(j\omega)$ and A3, which says that for ω sufficiently large $\|S(j\omega)\|_2 \leq 1 - \epsilon < 1$, imply, by the intermediate value theorem, that $\exists \omega_0 \in \mathbb{R}_+$, s.t. $\|S(j\omega_0)\|_2 = 1$.

$U \in \mathbb{C}^{n \times n}$ is unitary and $H \in \mathbb{C}^{n \times n}$ is Hermitian. Note $\bar{\sigma}[S(j\omega_0)] = \bar{\sigma}(H) = 1$.

By a synthesis technique [Car. 1; p. 370, 412 ff.] we can construct a passive lossless "load" n-port π_ℓ^0 (scattering matrix S_ℓ^0 , w.r.t. normalizing resistances $r_i > 0$ for S) such that $S_\ell^0(j\omega_0) = U^*$. Consequently, $S_\ell^0(j\omega_0) S(j\omega_0) = H$. H is Hermitian, so H has all eigenvalues real and the largest is 1. Consequently, $\det(I - S_\ell^0(j\omega_0) S(j\omega_0)) = 0$. Hence $s \mapsto (I - S_\ell^0 S)^{-1}(s)$ has a pole at $j\omega_0$ and so $(I - S_\ell^0 S)^{-1} \notin \hat{\mathcal{A}}^{n \times n}$. This contradicts I/O-stability, by Fact 2.1.1.

(\Leftarrow) We know that i) and ii) hold and i) with A1, A2 gives that $S(s) \in \hat{\mathcal{A}}^{n \times n}$. Consider an arbitrary lumped passive "load" n-port π_ℓ , described by $S_\ell(s)$. Then, in particular, $S_\ell(s) \in \hat{\mathcal{A}}^{n \times n}$ and

$$\forall \omega \in \mathbb{R}, \|S_\ell(j\omega)\|_2 \leq 1. (*)$$

Since $S_\ell(s), S(s) \in \hat{\mathcal{A}}^{n \times n}$, $S(s)$ and $S_\ell(s)$ are analytic in \mathbb{C}_+ and bounded in \mathbb{C}_+ . Now,

$$\begin{aligned} \sup_{\omega \in \mathbb{R}} \bar{\sigma}[S_\ell(j\omega)S(j\omega)] &\leq \sup_{\omega \in \mathbb{R}} [\|S_\ell(j\omega)\|_2 \cdot \|S(j\omega)\|_2] \\ &\leq \sup_{\omega \in \mathbb{R}} \|S_\ell(j\omega)\|_2 \sup_{\omega \in \mathbb{R}} \|S(j\omega)\|_2 \\ &< 1 \end{aligned}$$

where in the last step (*) and A3 were used. The function $s \mapsto \bar{\sigma}[S_\ell(s)S(s)]$ is subharmonic, hence using a useful property of subharmonic functions [Rud. 1; Them. 17.4, p.362]², we may write $\sup_{\text{Re } s \geq 0} \bar{\sigma}[S_\ell(s)S(s)] < 1$ which implies that

$$\inf_{\text{Re } s \geq 0} |\det(I - S_\ell S)(s)| > 0 \Rightarrow (I - S_\ell S)^{-1} \in \hat{\mathcal{A}}^{n \times n}$$

²We use theorem 17.4, p. 362, of [Rud. 1] with the \leq signs replaced by strict inequality signs, in which form (it is easy to see !) it is still true.

Since $S_\ell, S \in \hat{A}^{n \times n}$ (by i)), the 4 transfer functions of (3.1.1) and hence (Fact 3.1.1) those of (2.2.1) are in $\hat{A}^{n \times n}$, so π_{t_e} and π_{t_i} are I/O-stable.

4. k-terminations and absolute k-stability

In this section we define k-terminations and absolute k-stability which is a generalization of absolute stability and then derive necessary and sufficient conditions for absolute k-stability.

4.1. Definitions

Let $\underline{k} = (k_1, \dots, k_r) \in \mathbb{N}_+^r$ and let the n ports of \mathcal{N} be partitioned into r sets of k_1, \dots, k_r ports each, where $\sum_{i=1}^r k_i = n =$ number of ports of the given n-port, \mathcal{N} .

Definition 4.1.1: A k-termination of \mathcal{N} is the following:

the first set of k_1 ports is terminated by a k_1 -port, π_{k_1} ;

the next set of k_2 ports is terminated by a k_2 -port, π_{k_2} ;

⋮

the last set of k_r ports is terminated by a k_r -port, π_{k_r} .

The n-port made up of $\pi_{k_1}, \dots, \pi_{k_r}$ is described by scattering matrix S_ℓ , w.r.t. r_1, \dots, r_n (which are the normalizing resistances for \mathcal{N} , which is then described by S). Note that S_ℓ is a block-diagonal matrix whose successive blocks are of size k_1, \dots, k_r .

Definition 4.1.2: A passive (resp. lumped, I/O-stable) k-termination is a k-termination with π_{k_i} passive (resp. lumped, I/O-stable) for all $i \in \underline{r}$.

Notation: Let \mathcal{P}_{ℓ_k} be the class of all lumped passive k-terminations.

Definition 4.1.3: An n-port, \mathcal{N} , is said to be absolutely \underline{k} -stable iff the interconnections $\mathcal{N}_{t_e}, \mathcal{N}_{t_i}$ are I/O-stable for all lumped passive \underline{k} -terminations, \mathcal{N}_ℓ , (i.e., for all $\mathcal{N}_\ell \in \mathcal{P}_{\ell_k}$).

4.2. Characterization of absolutely \underline{k} -stable n-ports

The following characterization is an easy algebraic consequence of facts stated earlier:

Theorem 4.1: Let the distributed n-port, \mathcal{N} , satisfy A1, A2 and be I/O-stable. Let $S(s)$ be the scattering matrix of \mathcal{N} w.r.t. some choice of normalizing resistances, $r_i > 0, i \in \underline{n}$. Let $S_\ell(s)$ be the scattering matrix of the n-port $\mathcal{N}_\ell \in \mathcal{P}_{\ell_k}$ w.r.t. (the same) $r_i > 0, i \in \underline{n}$. U.t.c.,

\mathcal{N} is absolutely \underline{k} -stable iff for all $\mathcal{N}_\ell \in \mathcal{P}_{\ell_k}, \inf_{\text{Re } s \geq 0} |\det(I - S_\ell(s)S(s))| > 0$.

Proof: (\Rightarrow) By definition \mathcal{N} is absolutely \underline{k} -stable iff the 4 transfer functions of (2.2.1) belong to $\hat{\mathcal{A}}^{n \times n}$ equivalently, by Fact 3.1.1 iff the 4 transfer functions of 3.1.1 belong to $\hat{\mathcal{A}}^{n \times n}$. In particular,

$(I - S_\ell S)^{-1} \in \hat{\mathcal{A}}^{n \times n}$ which is true iff $\inf_{\text{Re } s \geq 0} |\det(I - S_\ell(s)S(s))| > 0$

because both S and S_ℓ have elements in $\hat{\mathcal{A}}$.

(\Leftarrow) \mathcal{N} satisfies A1, A2 and is I/O-stable $\Leftrightarrow S(s) \in \hat{\mathcal{A}}^{n \times n}$,

(comment following thm. 3.1). Consider an arbitrary n-port $\mathcal{N}_\ell \in \mathcal{P}_{\ell_k}$ then $S_\ell(s) \in \mathbb{R}_p^{n \times n}(s)$, (Comment a) preceding thm. 3.1). $\inf_{s \in \mathbb{C}_+} |\det(I - S_\ell(s)S(s))| > 0 \Leftrightarrow (I - S_\ell S)^{-1} \in \hat{\mathcal{A}}^{n \times n}$. Now, by closure under multiplication in the algebra $\hat{\mathcal{A}}^{n \times n}$, the 4 transfer functions of (2.2.1) belong to $\hat{\mathcal{A}}^{n \times n}$ which is true iff the 4 transfer functions of (3.1.1) belong to $\hat{\mathcal{A}}^{n \times n}$. Since the \mathcal{N}_ℓ in \mathcal{P}_{ℓ_k} was arbitrary we have shown \mathcal{N} to be absolutely \underline{k} -stable.

□

In section 5.2 we will use the tools developed in section 5.1 below and our knowledge of the structure of $S_\rho(s)$ to obtain a more useful characterization than the one above.

5. Characterization of absolute \underline{k} -stability in terms of Doyle's $\mu_{\underline{k}}$ function

5.1. Definition and required properties of Doyle's function μ [Doy. 1]

Notation

$\mathbb{B}_\delta(\underline{k}) := \{\text{block diagonal matrices in } \mathbb{C}^{n \times n}, \text{ with } r \text{ square blocks } \in \mathbb{C}^{k_i \times k_i}, i \in \underline{r} \text{ and with } \|\cdot\|_2\text{-norm of each block } \leq \delta \in \mathbb{R}_+\}$

Recall that $\underline{k} := (k_1, \dots, k_r) \in \mathbb{N}_+^r$ and that $\sum_{i=1}^r k_i = n$

$\mathbb{B}_\infty(\underline{k}) := \bigcup_{\delta \in \mathbb{N}} \mathbb{B}_\delta(\underline{k})$; in words, $\mathbb{B}_\infty(\underline{k})$ is the set of block diagonal matrices with structure determined by \underline{k}

$\mathcal{U}(\underline{k}) := \{\text{unitary matrices}\} \cap \mathbb{B}_1(\underline{k})$; in words, $\mathcal{U}(\underline{k})$ is the set of all unitary matrices with block-diagonal structure determined by \underline{k} .

Definition 5.1: $\mu_{\underline{k}} : \mathbb{C}^{n \times n} \rightarrow \mathbb{R}_+$ is a function defined as follows:

$$\forall M \in \mathbb{C}^{n \times n} \begin{cases} \mu_{\underline{k}}(M) = 0 & \text{if } \exists \Delta \in \mathbb{B}_\infty(\underline{k}) \text{ such that } \det(I - M\Delta) = 0 \\ \frac{1}{\mu_{\underline{k}}(M)} = \min_{\Delta \in \mathbb{B}_\infty(\underline{k})} \{\bar{\sigma}(\Delta) \text{ such that } \det(I - M\Delta) = 0\} \end{cases}$$

Comment: Intuitively if we think of $\bar{\sigma}(\Delta)$ as measuring the "size" of $\Delta \in \mathbb{B}_\infty(\underline{k})$ then $1/\mu_{\underline{k}}(M)$ is the minimum size of $\Delta \in \mathbb{B}_\infty(\underline{k})$ such that $\det(I - M\Delta) = 0$ (for all "smaller" $\Delta \in \mathbb{B}_\infty(\underline{k})$, $\det(I - M\Delta) \neq 0$).

From Definition 5.1 the following proposition is immediate.

Proposition 5.1:

$$\forall M \in \mathbb{C}^{n \times n}, \forall \Delta \in \mathbb{B}_\delta(\underline{k}), \det(I - M\Delta) = \det(I - \Delta M) \neq 0 \Leftrightarrow \delta \cdot \mu_{\underline{k}}(M) < 1$$

Proposition 5.2: Given $s \mapsto M(s) \in \mathbb{C}^{n \times n}$ analytic in \mathbb{C}_+ ,

$$\forall \Delta \in \mathbb{B}_1(\underline{k}), \inf_{s \in \mathbb{C}_+} |\det(I - \Delta M(s))| > 0 \Leftrightarrow \sup_{s = j\omega} \mu_{\underline{k}}(M(s)) < 1$$

Proof: Appendix

The following proposition, first stated in [Doy. 1], is the last item we need:

Proposition 5.3: $\forall M \in \mathbb{C}^{n \times n}, \max_{U \in \mathcal{U}(\underline{k})} \rho(UM) = \mu_{\underline{k}}(M)$, where $\rho(A) :=$ spectral radius of $A = \max_{\lambda \in \sigma(A)} \{|\lambda|\}$.

Proof: Appendix

5.2. A characterization of absolute \underline{k} -stability

Using Proposition 5.2, the following equivalent formulation of Theorem 4.1 is immediate.

Theorem 5.1: Let the distributed n-port, \mathcal{N} , satisfy A1, A2 and be I/O-stable. Let $S(s)$ be its scattering matrix of \mathcal{N} w.r.t. some choice of positive normalizing resistances $r_i > 0, i \in \underline{n}$. U.t.c.

$$\mathcal{N} \text{ is absolutely } \underline{k}\text{-stable} \Leftrightarrow \sup_{s = j\omega} \mu_{\underline{k}}(S(s)) < 1$$

Proof: Immediate from Theorem 3.1 and Proposition 5.2 with $M = S(s)$ and the fact that $\mathcal{N}_\ell \in \mathcal{O}_{\underline{k}} \Rightarrow \forall s \in \mathbb{C}_+, S_\ell(s) =: \Delta \in \mathbb{B}_1(\underline{k})$ (see comment a) following definition 3.2). □

Now we use Proposition 5.3 to arrive at the most useful (from a computational point of view) equivalent formulation of Theorem 4.1.

Theorem 5.2: Let the distributed n-port \mathcal{N} satisfy A1, A2 and be

I/O-stable. Let $S(s)$ be its scattering matrix w.r.t. some choice of positive normalizing resistances, $r_i > 0, i \in \underline{n}$. U.t.c.

$$\mathcal{N} \text{ is absolutely } \underline{k}\text{-stable} \Leftrightarrow \sup_{s=j\omega} \left(\max_{U \in \mathcal{Z}(\underline{k})} \rho(US) \right) < 1$$

Proof: Immediate from Theorem 5.1 and Proposition 5.3.

Comments: a) A reactance n-port \mathcal{N}_ℓ (made up of k_1 -, ..., k_r -ports with $\sum_{i=1}^r k_i = n$) has a scattering matrix $S_\ell(j\omega) \in \mathcal{Z}(\underline{k}), \forall \omega$. Thus,

Theorem 5.2 is a precise statement and proof of the conjecture that the absolute \underline{k} -stability of an n-port can be checked by closing its ports, partitioned according to \underline{k} , on reactive k_1 -, k_2 -, ..., k_r -ports. In \underline{n} times

particular, the absolute $(\overbrace{1, \dots, 1}^{\underline{n}})$ -stability (simply called absolute stability in the literature) of an n-port can be checked by closing each of its ports on reactive one-ports. This special case of Theorem 5.2 above was proved for lumped LT-I n-ports by Youla [You. 2].

b) See [Doy. 1] for some details on the computation of $\mu_{\underline{k}}$.

Appendix 1

Proposition 5.2: Given $s \mapsto M(s) \in \mathbb{C}^{n \times n}$, analytic in \mathbb{C}_+ ,

$$\forall \Delta \in \mathbb{B}_1(k), \inf_{s \in \mathbb{C}_+} |\det(I - \Delta M(s))| > 0 \Leftrightarrow \sup_{\omega} \mu_k(M(j\omega)) < 1$$

Proof: (\Rightarrow) By assumption $\inf_{s \in \mathbb{C}_+} |\det(I - \Delta M(s))| > 0$, hence

$$\forall \Delta \in \mathbb{B}_1(k), \forall s \in \mathbb{C}_+ \det(I - \Delta M(s)) \neq 0; \text{ consequently } \forall s \in \mathbb{C}_+, \mu_k(M(s)) < 1$$

(from Proposition 1, with $\delta = 1$, since $\Delta \in \mathbb{B}_1(k)$). Furthermore,

$$\sup_{\omega} \mu_k(M(j\omega)) < 1, \text{ for if } \exists \{s_i\}, s_i \in \mathbb{C}_+, \forall i \text{ s.t. } \lim_{i \rightarrow \infty} \mu_k(M(s_i)) = 1$$

then $\exists \Delta \in \mathbb{B}_1(k)$ s.t. $\lim_{i \rightarrow \infty} |\det(I - \Delta M(s_i))| = 0$ contradicting the hypothesis.

(\Leftarrow) As shown in (A.1.2) (see the proof of Proposition 5.3 below)

$$\forall A \in \mathbb{C}^{n \times n}, \rho(A) \leq \mu(A). \text{ Thus,}$$

$$\sup_{\omega} \rho(\Delta M(j\omega)) \leq \sup_{\omega} \mu(\Delta M(j\omega)) = \sup_{\omega} \mu(M(j\omega)) < 1$$

where the equality holds because $\Delta \in \mathbb{B}_1(k)$. By the maximum modulus

theorem, $\sup_{s \in \mathbb{C}_+} \rho(\Delta M(s)) = \sup_{\omega} \rho(\Delta M(j\omega))$. Thus $\sup_{s \in \mathbb{C}_+} \rho(\Delta M(s)) < 1$ which

implies that

$$\inf_{s \in \mathbb{C}_+} |\det(I - \Delta M(s))| > 0. \quad \square$$

Lemma A1 (Block diagonal singular value decomposition (SVD))

$\forall \Delta \in \mathbb{B}_{\infty}(k), \exists U, V \in \mathcal{U}(k), \exists \Sigma$ a diag. matrix with diag. entries in \mathbb{R}_+ , s.t. $\Delta = U \Sigma V^*$

Proof: Clear from standard SVD and definitions of $\mathcal{U}(k), \mathbb{B}_{\infty}(k)$.

Lemma A2 (Doyle, [Doy. 1])

Let $f: \mathbb{C}^p \rightarrow \mathbb{C}$ polynomial in p complex variables, of degree no more than q in each variable.

Let $\hat{y} := \arg \min \{\|y\|_\infty : y \in \mathbb{C}^P \text{ and } f(y) = 0\}$. U.t.c.

$$\exists v \in \mathbb{C}^P : f(v) = 0 \text{ and } |v_j| = \|\hat{y}\|_\infty \quad \forall j \in \underline{p}$$

Proof by contradiction: If for some minimizer $\hat{y} \in \mathbb{C}^P$ defined above, $|y_j| = \|\hat{y}\|_\infty$, $\forall j \in \underline{p}$, \hat{y} satisfies the theorem and there is nothing to prove. (Introduce the notation $y =: (z, \omega)$ with $z \in \mathbb{C}^{P-1}$, $\omega \in \mathbb{C}$.) If not, choose the smallest component of \hat{y} , say $\hat{\omega} \in \mathbb{C}$, let $\hat{y} = (\hat{z}, \hat{\omega})$ and we have

$$|\hat{\omega}| < \|\hat{z}\|_\infty = \|\hat{y}\|_\infty .$$

Abusing notation we write $f(y) = f(z, \omega)$, $z \in \mathbb{C}^{P-1}$, $\omega \in \mathbb{C}$. We also have $f(\hat{y}) = f(\hat{z}, \hat{\omega}) = 0$. Now view f as a polynomial in ω with coefficients that are polynomials in z ; $f : \omega \mapsto f(z, \omega)$. By the Weierstrass preparation theorem [Die. 1], [Rud. 1] there exist an integer r and r functions $h_j(z)$, analytic in a neighborhood V of $\hat{z} \in \mathbb{C}^{P-1}$ such that

$$f(z, \omega) = (\omega^r + h_1(z)\omega^{r-1} + \dots + h_r(z)) g(z, \omega)$$

for all ω in some disc $D(\hat{\omega}; \epsilon)$ centered on $\hat{\omega}$ with radius ϵ ; g is analytic in $V \times D(\hat{\omega}; \epsilon)$. For ϵ sufficiently small, $f(z, \omega)$ has exactly r solutions $z = \phi_k(\omega)$ in $V \times D(\hat{\omega}, \epsilon)$. Choose $z_1 \in V$ and ω_1 in $D(\hat{\omega}; \epsilon)$ such that $u_1 = (z_1, \omega_1) \in \mathbb{C}^P$ is a zero of f , $f(u_1) = f(z_1, \omega_1) = 0$, and $\|u_1\|_\infty < \|\hat{y}\|_\infty$. Thus f has a zero at u_1 of smaller norm than \hat{y} which contradicts the definition of \hat{y} . Hence there is always a minimizer \hat{y} with the property claimed.

Corollary to Lemma A.2: If \hat{y} is real and nonnegative [$\text{Im}(\hat{z}_j) = 0$ and $\text{Re}(\hat{z}_j) \geq 0$, $\forall j$], then $\exists v \in \mathbb{R}^P$ nonnegative s.t. $f(v) = 0$ and

$$v_j = \|\hat{y}\|_\infty \quad \forall j \in \underline{p}$$

Proposition 5.3: $\forall M \in \mathbb{C}^{n \times n}$, $\max_{U \in \mathcal{Z}(\underline{k})} \rho(UM) = \mu_{\underline{k}}(M)$.

Proof: We first show:

$$\max_{U \in \mathcal{Z}(\underline{k})} \rho(UM) \leq \mu_{\underline{k}}(M) \quad (\text{A.1.1})$$

If $\underline{k} = (1, \dots, 1)$ then $\mathbb{B}_{\delta}(\underline{k}) = \{\lambda I : \lambda \in \mathbb{C}, |\lambda| \leq \delta\}$ and then $\mu_{\underline{k}}(M)$

$= \rho(M)$ ($:= \max_{\lambda \in \sigma(M)} |\lambda|$), and $\det(I - \lambda M) \neq 0, \forall |\lambda| \leq \delta$ iff $\delta \rho(M) < 1$.

But δ is the solution to a constrained minimization problem and $\mu_{\underline{k}}(M) = \frac{1}{\delta}$ and since $\mu_{\underline{k}}(M) = \rho(M)$ for $\underline{k} = (1, \dots, 1)$ it follows that, for general \underline{k} ,

$$\rho(M) \leq \mu_{\underline{k}}(M) . \quad (\text{A.1.2})^3$$

$\Delta \in \mathbb{B}_{\delta}(\underline{k}), U \in \mathcal{Z}(\underline{k})$ hence $U\Delta, \Delta U \in \mathbb{B}_{\delta}(\underline{k})$. Also, $\det(I - UM\Delta)$
 $= \det(UU^* - UM\Delta) = \det(U(I - M\Delta U)U^*) = \det(I - M\Delta U)$

Hence,

$$\mu_{\underline{k}}(MU) = \mu_{\underline{k}}(UM) = \mu_{\underline{k}}(M) \quad (\text{A.1.3})$$

From (A.1.2) and (A.1.3) we have $\max_{U \in \mathcal{Z}(\underline{k})} \rho(UM) \leq \mu(M)$ which is (A.1.1).

We now prove the proposition.

If $\mu_{\underline{k}}(M) = 0$ then the result follows immediately from (A.1.1).

Otherwise, let $\mu_{\underline{k}}(M) = (1/\delta) > 0$. Then $\exists \Delta \in \mathbb{B}_{\delta}(\underline{k})$ such that $\bar{\sigma}(\Delta) = \delta$ and $\det(I - \Delta M) = 0$. By lemma A.1 $\exists U, V \in \mathcal{Z}(\underline{k})$ and $\exists \Sigma$, a diagonal $n \times n$ matrix with diagonal entries in \mathbb{R}_+ such that $\Delta = U\Sigma V^*$ then $\det(I - \Delta M) = 0$ iff $\det(I - U\Sigma V^*M) = 0$ which is a polynomial in the diagonal elements of Σ and by definition of $\mu_{\underline{k}}$, Σ is the minimum norm solution to this polynomial equation. By the corollary to lemma A.2, Σ may be replaced by δI with $\delta = \|\Sigma\|_{\infty}$. Thus,

³Equation (A.1.2) was used in the proof of proposition 5.2.

$$\det(I - U\Sigma V^*M) = 0 \Rightarrow \det(I - \delta UV^*M) = 0$$

$$\Rightarrow \rho(UV^*M) \geq \frac{1}{\delta} = \mu_{\underline{k}}(M)$$

But, by (A.1.1), we also have $\rho(UV^*M) \leq \mu_{\underline{k}}(M)$, since $U, V^* \in \mathcal{U}(\underline{k})$.

Hence

$$\max_{U \in \mathcal{U}} \rho(UM) = \mu_{\underline{k}}(M).$$

Appendix 2

Theorem A1: Consider an n -port \mathcal{N} made up of linear time-invariant passive R, L, C elements, gyrators and voltage-controlled current-sources (VCCS's). Let the "gains" of the VCCS's have the following form:

$g_m \left(\frac{1}{1 + j \frac{\omega}{\omega_m}} \right)$ where $g_m \in \mathbb{R}$, $\omega_m \in \mathbb{R}_+$ ("large"). Let \mathcal{N} be described by scattering matrix $S(s)$ w.r.t. $r_i > 0$, $i \in \underline{n}$ and let $S(s)$ be analytic in \mathbb{C}_+ . Then $S(s) \in \hat{\mathcal{A}}^{n \times n}$.

Comments: a) It is sufficient to consider only VCCS's since it can be shown that one can represent any other kind of controlled source by pre- and/or port-cascading a VCCS with gyrator(s). It should also be noted that ideal transformers can be represented by controlled sources and hence by a suitable combination of VCCS's and gyrators.

b) It is the nature of the elements (passive R, L, C, gyrators, VCCS's with gains $g_m \left(\frac{1}{1 + j \frac{\omega}{\omega_m}} \right)$) that ensures that $S(s) \in \hat{\mathcal{A}}^{n \times n}$, so that

Theorem A1 is not a mathematical fact. In fact if the gain of the VCCS's were a constant, Theorem A1 would be false and, indeed, some entries of $S(s)$ could be made to behave like polynomials in s .

Proof: Since \mathcal{N} is made up of lumped linear time-invariant elements, its scattering matrix $S(s) \in \mathbb{R}(s)^{n \times n}$. Further, since $S(s)$ is analytic in \mathbb{C}_+ , it only remains to show that $S(s)$ is bounded at ∞ on the $j\omega$ -axis to conclude that $S(s) \in \hat{\mathcal{A}}^{n \times n}$.

Let \mathcal{N} "contain" k VCCS's. The first step is to "extract" all the VCCS 2-ports: after extracting the "voltage-sensing" ports and the corresponding controlled current-sources, an $(n+2k)$ -port, \mathcal{N}_e , is created. Since \mathcal{N}_e "contains" only passive R, L, C elements and gyrators we know that [New. 1, p.98]

$$S(s) \in \mathbb{R}_p(s)^{n \times n} \text{ is analytic in } \mathbb{C}_+ \quad (\text{A.2.1})$$

$$\forall \omega \in \mathbb{R}, I - S^*(j\omega) S(j\omega) \text{ is positive semi-definite} \quad (\text{A.2.2})$$

Inspection of Fig. A.1 shows that we need to examine 3 kinds of transfer functions for boundedness

i) the transfer function from an "original" port such as ① to a voltage-sensing "created" open-circuit port such as ②;

ii) the transfer function from a (controlled) current-source terminated "created" port, such as ③, to an "original" port such as ⑤; and

iii) the transfer function from a CCS-terminated "created" port, such as ③, to a "created" o.c. port, such as ④.

Inspection of Figs. A.2., A.3, and A.4 gives the following expressions for the transfer functions in terms of scattering-parameters and impedance parameters

$$V_2 = \frac{2s_{21}}{1-s_{22}} I_{s_1} \quad (\text{A.2.3})$$

$$E_2 = \frac{s_{21}}{1-s_{11}} I_{s_1} \quad (\text{A.2.4})$$

$$V_2 = z_{21} I_{s_1} \quad (\text{A.2.5})$$

It now remains to show that the transfer functions $\frac{s_{21}}{1-s_{22}}$ and $\frac{s_{21}}{1-s_{11}}$ of (A.2.3), (A.2.4) are bounded; and that under the assumption on the behavior of the "gains" of the controlled-current-sources the RHS of (A.2.5) is bounded at ∞ .

We first prove ii)

Claim: $\frac{s_{21}}{1-s_{11}}$ is bounded at ∞ on the $j\omega$ -axis.

Proof: Equation (A.2.2) implies that the s_{ij} 's are bounded and specifically that:

$$1 - (|s_{11}|^2 + |s_{21}|^2) \geq 0 \quad (\text{A.2.6})$$

$\frac{s_{21}}{1-s_{11}}$ can only be unbounded if $s_{11} \rightarrow 1$ faster than $s_{21} \rightarrow 0$ (which is required by (A.2.6) if $s_{11} \rightarrow 1$). We must therefore examine rates of convergence: s_{11} is rational, hence a Taylor expansion (evaluated at $s = \infty$) gives

$$s_{11} = (1 + \frac{\beta}{\omega^2} + \dots + \dots +) + j(\frac{\alpha}{\omega} + \frac{\gamma}{\omega^3} + \dots) \quad (\text{A.2.7})$$

From (A.2.7),

$$|s_{11}|^2 = 1 + \frac{\alpha^2 + 2\beta}{\omega^2} + o(\frac{1}{\omega^4}) \quad (\text{A.2.8})$$

Using (A.2.8) in (A.2.6) gives, $1 - [1 + \frac{\alpha^2 + 2\beta}{\omega^2} + o(\frac{1}{\omega^4})] \geq |s_{21}|^2$

$$\Rightarrow |s_{21}|^2 \leq \frac{\delta}{\omega^2} \quad ,$$

$$\Rightarrow s_{21} = o(\frac{1}{j\omega})$$

From (A.2.7) $1 - s_{11} = o(\frac{1}{j\omega})$

Thus, $\frac{s_{21}}{1-s_{11}}$ tends to a finite constant as $\omega \rightarrow \infty$.

We now prove i)

Claim: $\frac{s_{21}}{1-s_{22}}$ is bounded at ∞ on the $j\omega$ -axis.

Proof: (by contradiction) For $\frac{s_{21}}{1-s_{22}}$ to be unbounded at ∞ we must have s_{21} bounded away from 0 at ∞ while $s_{22} \rightarrow 1$ (since by passivity, all the s_{ij} 's of \mathcal{N}_0 are bounded). Thus, in terms of Taylor expansions,

$$s_{21} = \tau_0 + \frac{\tau_1}{j\omega} + \dots + \dots; \quad (\text{A.2.9})$$

$$s_{22} = 1 + \frac{\alpha}{j\omega} + \dots \quad (\text{A.2.10})$$

where we assume $\tau_0 \neq 0$.

$$\text{Let } I - S_0^*(j\omega) S_0(j\omega) =: \begin{bmatrix} a_{11} & a_{12} \\ a_{12}^* & a_{22} \end{bmatrix}$$

Then,

$$a_{11} := 1 - (|s_{11}|^2 + |s_{21}|^2) \quad (\text{A.2.11a})$$

$$a_{12} := s_{11}^* s_{12} + s_{21}^* s_{22} \quad (\text{A.2.11b})$$

$$a_{22} := 1 - (|s_{12}|^2 + |s_{22}|^2) \quad (\text{A.2.11c})$$

and passivity of π_0 (see Fig. A.2) implies that $I - S_0^*(j\omega) S_0(j\omega) \geq 0$ equivalently

$$a_{11} \geq 0 \quad (\text{A.2.12a})$$

$$a_{22} \geq 0 \quad (\text{A.2.12b})$$

$$a_{11} a_{22} - |a_{12}|^2 \geq 0 \quad (\text{A.2.12c})$$

From (A.2.10), (A.2.11.c) and (A.2.12b)

$$s_{12} = o\left(\frac{1}{j\omega}\right) \quad (\text{A.2.13})$$

and thus from (A.2.10) and (A.2.13)

$$a_{22} = 1 - (|s_{12}|^2 + |s_{22}|^2) = o\left(\frac{1}{\omega^2}\right) \quad (\text{A.2.14})$$

From (A.2.9) and (A.2.11a)

$$a_{11} = o(1) \quad (\text{A.2.15})$$

Now, from (A.2.15), (A.2.14) and (A.2.12c) we must have

$$a_{12}^* = s_{12}^* s_{11} + s_{22}^* s_{21} = o\left(\frac{1}{j\omega}\right) \quad (\text{A.2.16})$$

From (A.2.9), (A.2.10), $s_{22}^* s_{21} = o(1)$ and hence

$$a_{12}^* = s_{12}^* s_{11} + s_{22}^* s_{21} = o(1) \quad (\text{A.2.17})$$

(A.2.16) and (A.2.17) give the required contradiction.

Claim iii): z_{21} is, at worst, $O(j\omega)$.

Proof: \mathcal{N}_i (see Fig. A.4) has a positive-real Z matrix and by the direct PR test [New. 1, p. 117]

$$Z(j\omega) + Z^*(j\omega) \geq 0 \quad (\text{A.2.18})$$

$$\text{Let } Z = \begin{bmatrix} z_{11} & z_{12} \\ z_{21} & z_{22} \end{bmatrix}$$

The positive-real property implies that z_{11} , z_{22} are $O(j\omega)$ at most; using this information in (A.2.18) gives that z_{21} is, at worst, $O(j\omega)$.

Thus, in eqn. (A.2.5), (since the extracted controlled current-sources I_{s1} are assumed to be $O(\frac{1}{j\omega})$) the RHS $z_{21} I_{s1}$ is bounded at ∞ .

Since all transfer functions can be obtained by a suitable combination of type i), ii), iii) functions we have shown that $S(s)$ is bounded at ∞ .

We now generalize theorem A1 to include a class of distributed circuits.

P.A.2: Consider an n-port \mathcal{N} made up of passive R, L, C elements, gyrators, VCCS's whose "gains" are of the form $g_m \left[\frac{1}{1 + j(\frac{\omega}{\omega_m})} \right]$ and a finite number k of uniform, lossless transmission lines. Let the k transmission lines be attached to m "internal" ports (m is less than 2k by the number of open- and short-circuited "stubs").

Extracting the m ports to which the k transmission lines are connected, an (n+m)-port, \mathcal{N}_ℓ , (with corresponding scattering matrix S_ℓ) is created. Note that \mathcal{N}_ℓ , which is lumped, satisfies the hypotheses of Theorem A.1. Hence $S_\ell \in \hat{\mathcal{A}}^{(n+m) \times (n+m)}$. The distributed m-port of transmission lines, \mathcal{N}_d , has a scattering matrix $S_d \in \hat{\mathcal{A}}^{m \times m}$ (this

is easily seen for characteristic impedance terminations on all ports; entries are then either zero or of the form $e^{-\tau_i s}$, $i \in \underline{k}$. For other choices of normalizing resistances, the scattering matrix S'_d is similar to S_d , see [New. 1, p. 74]).

We now partition the $(n + m)$ ports of \mathcal{N}_ℓ according to "original" or external variables, subscripted with an e; and "created" or internal variables, subscripted with an i. Thus,

$$b_e = S_{ee} a_e + S_{ei} a_i \quad (\text{A.2.19})$$

$$b_i = S_{ie} a_e + S_{ii} a_i \quad (\text{A.2.20})$$

Note that: i) Since the partitioned matrix $\begin{matrix} n & m \\ \left[\begin{array}{cc} S_{ee} & S_{ei} \\ S_{ie} & S_{ii} \end{array} \right] \end{matrix}$ is a permutation of $S_\ell \in \hat{\mathcal{Q}}^{(n+m) \times (n+m)}$ we have $S_{ee} \in \hat{\mathcal{Q}}^{n \times n}$, $S_{ei} \in \hat{\mathcal{Q}}^{m \times n}$, $S_{ie} \in \hat{\mathcal{Q}}^{m \times n}$, $S_{ii} \in \hat{\mathcal{Q}}^{m \times m}$.

ii) To arrive at $S(s)$ we seek the relation between b_e and a_e when \mathcal{N}_ℓ is loaded at its m "internal" ports by the m -port \mathcal{N}_d . Denoting port-variables of \mathcal{N}_d with a \sim , we have,

$$\tilde{b}_i = S_d \tilde{a}_i \quad (\text{A.2.21})$$

The interconnection equations are:

$$b_i = \tilde{a}_i \quad (\text{A.2.22a})$$

$$a_i = \tilde{b}_i \quad (\text{A.2.22b})$$

We may now state theorem A.2.

Theorem A2: Consider an LT-I n-port \mathcal{N} made up of passive R, L, C elements, gyrators, VCCS's whose "gains" are of the form $g_m \left(\frac{1}{1 + j\frac{\omega}{\omega_m}} \right)$ and a finite number, k, or uniform lossless transmission lines attached to m "internal" ports. Assume that,

$$\forall \omega \in \mathbb{R}, \|S_{ii}(j\omega)\|_2 < 1 \quad (\text{see eqn, A.2.20 above for defn. of } S_{ii})$$

Then the scattering matrix of \mathcal{N} , $S(s) \in \hat{\mathcal{Q}}^{n \times n}$.

Proof: Solving equations (A.2.19), (A.2.20), (A.2.21) and (A.2.22) for b_e in terms of a_e gives

$$S = S_{ee} + s_{ei}(I - S_d S_{ii})^{-1} S_d S_{ie}$$

Thus if $(I - S_d S_{ii})^{-1} \in \hat{\mathcal{Q}}^{m \times m}$ then closure properties of the algebra $\hat{\mathcal{Q}}^{n \times n}$ imply that $S \in \hat{\mathcal{Q}}^{n \times n}$. $(I - S_d S_{ii})^{-1} \in \hat{\mathcal{Q}}^{m \times m}$ iff $\inf_{\text{Res} \geq 0} |\det(I - S_d S_{ii})| > 0$. Since \mathcal{N}_d is made up of lossless transmission lines S_d is unitary on the $j\omega$ -axis, i.e. $\|S_d(j\omega)\|_2 = 1$. Now,

$$\begin{aligned} \sup_{\omega \in \mathbb{R}} \bar{\sigma}[S_d(j\omega) S_{ii}(j\omega)] &\leq \sup_{\omega \in \mathbb{R}} [\|S_d(j\omega)\|_2 \cdot \|S_{ii}(j\omega)\|_2] \\ &\leq \sup_{\omega \in \mathbb{R}} \|S_d(j\omega)\|_2 \sup_{\omega \in \mathbb{R}} \|S_{ii}(j\omega)\|_2 \\ &< 1 \end{aligned}$$

By subharmonicity of $s \mapsto \bar{\sigma}[S_d(s)S_{ii}(s)]$ we may write $\sup_{\text{Res} > 0} \bar{\sigma}[S_d(s)S_{ii}(s)] < 1$ which implies that $\inf_{s \in \mathbb{C}_t} |\det(I - S_d S_{ii})| > 0$. (For details see pf. of thm. 3.1)

References

- [Cal. 1] F. M. Callier and C. A. Desoer, Multivariable Feedback Systems, New York-Heidelberg-Berlin: Springer-Verlag, 1982.
- [Car. 1] H. J. Carlin and A. B. Giordano, Network Theory, Englewood Cliffs, N.J.: Prentice-Hall, 1964.
- [Des. 1] C. A. Desoer and M. Vidyasagar, Feedback Systems, Input-Output Properties, New York: Academic 1975.
- [Die. 1] J. Dieudonné, Foundations of Modern Analysis, New York: Academic 1969.
- [Doy. 1] J. Doyle, "Analysis of Feedback Systems with Structured Uncertainties," IEE Proc. vol. 129, pt. D, no. 6, pp. 242-250, November 1982.
- [Kuh. 1] E. S. Kuh and R. Rohrer, Theory of Linear Active Networks, San Francisco: Holden-Day 1968.
- [Lle. 1] F. B. Llewellyn, "Some Fundamental Properties of Transmission Systems," Proc. IRE, vol. 40, pp. 271-283, 1952.
- [New. 1] R. W. Newcomb, Linear Multiport Synthesis, New York: McGraw-Hill, 1966.
- [Rud. 1] W. Rudin, Real and Complex Analysis, New York: McGraw-Hill, 1974.
- [Rud. 2] W. Rudin, Function Theory in Polydiscs, New York: W. A. Benjamin, 1966.
- [Sch. 1] L. Schwartz, Théorie des Distributions, Paris, France: Hermann, 1966.
- [Vid. 1] M. Vidyasagar, Nonlinear Systems Analysis, Englewood Cliffs, N.J.: Prentice-Hall, 1978.
- [Woo. 1] D. Woods, "Reappraisal of the Unconditioned Stability Criteria for Active 2-port Networks, in terms of S Parameters," IEEE Trans. Circuits and Systems, vol. CAS-23, no. 2, February 1976.

- [You. 1] D. C. Youla, "A Stability Characterization of the Reciprocal Linear Passive n-Port," Proc. IRE, vol. 47, pp. 1150-1151, June 1959.
- [You. 2] D. C. Youla, "A Maximum Modulus Theorem for Spectral Radius and Absolutely Stable Amplifiers," IEEE Trans. on Circuits and Systems, vol. CAS-27, no. 12, pp. 1274-1276, December 1980.
- [Zeh. 1] E. Zeheb and E. Walach, "Necessary and Sufficient Conditions for the Absolute Stability of Linear n-Ports," International Journal of Circuit Theory and Applications, vol. 9, pp. 311-330, 1981.
- [Zem. 1] A. H. Zemanian, Realizability Theory for Continuous Time Systems, New York: Academic, 1971.

Figure Captions

- Fig. 1. The circuit \mathcal{N}_{ti} consists of the given n-port \mathcal{N} terminated by the load n-port \mathcal{N}_l and driven by the current-source i .
- Fig. 2. The circuit \mathcal{N}_{te} consists of the given n-port \mathcal{N} terminated by the load n-port \mathcal{N}_l and driven by the voltage-source e .
- Fig. A.1. The figure shows the n-port \mathcal{N} after the extraction of the VCCS's.
- Fig. A.2. The type (i) transfer function relates V_2 to I_{S1} .
- Fig. A.3. The type (ii) transfer function relates E_2 to I_{S1} .
- Fig. A.4. The type (iii) transfer function relates V_2 to I_{S1} .

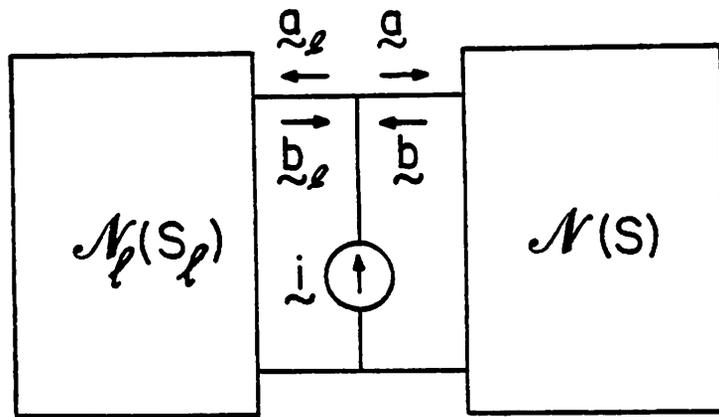


Fig. 1

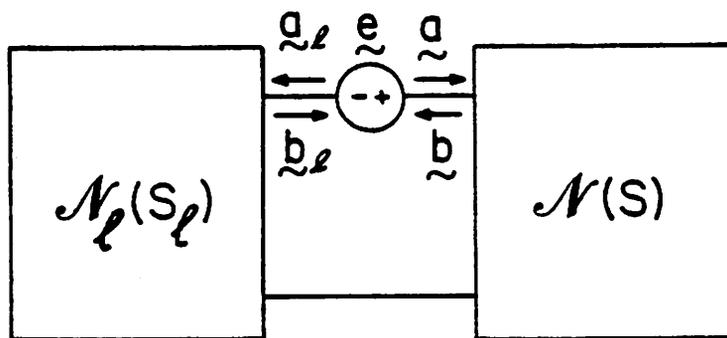


Fig. 2

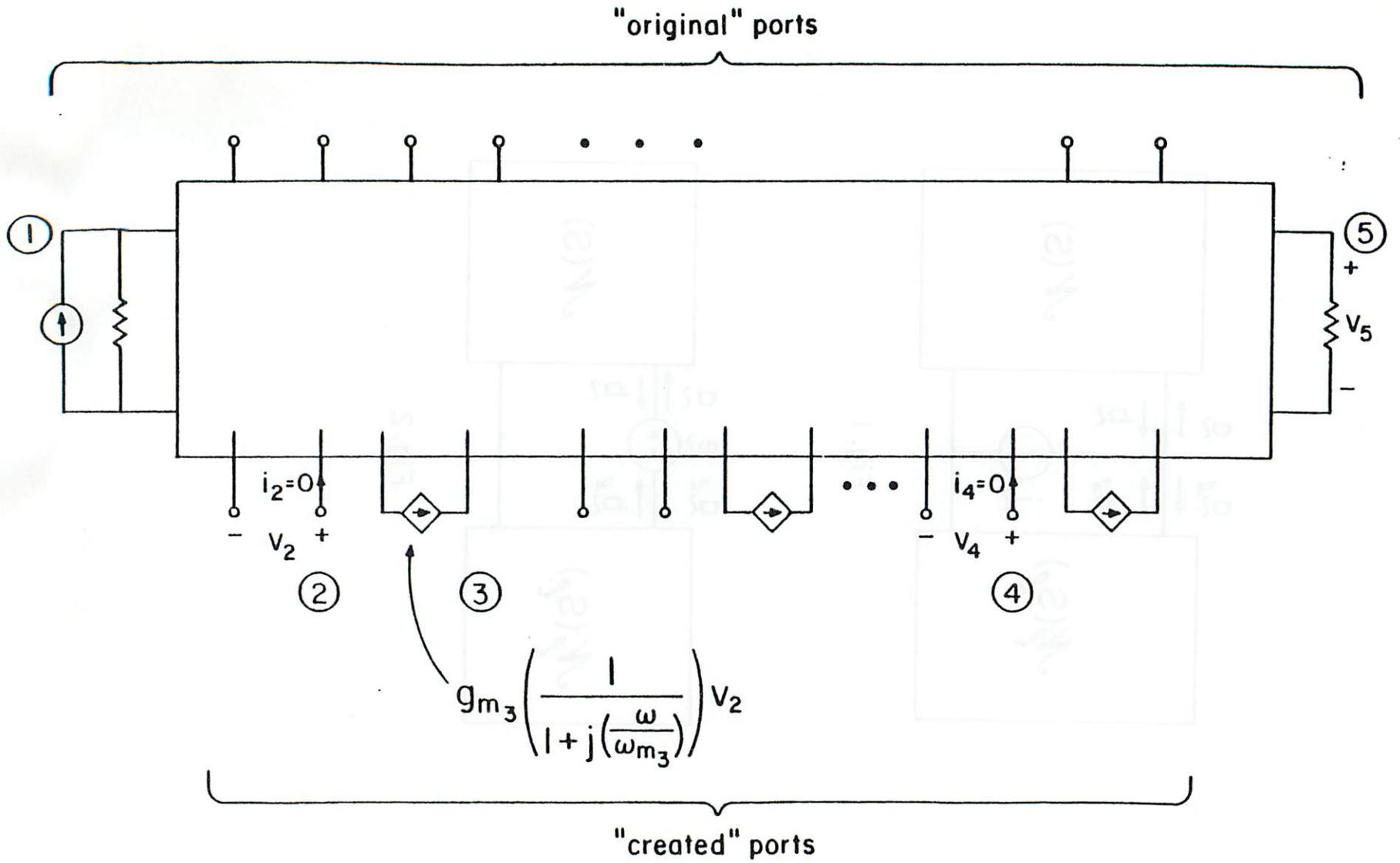


Fig. A.1.

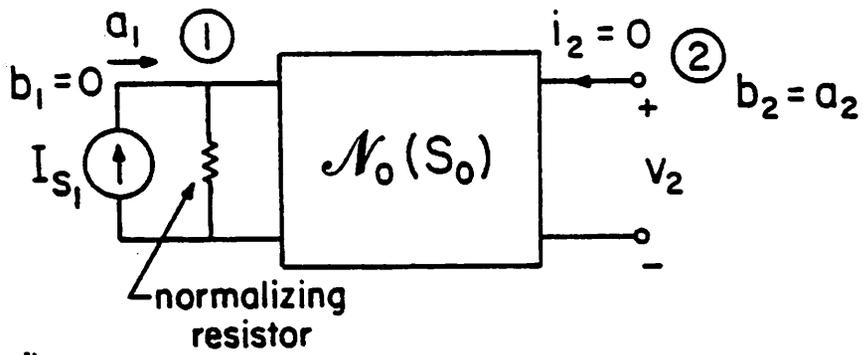


Fig. A.2.

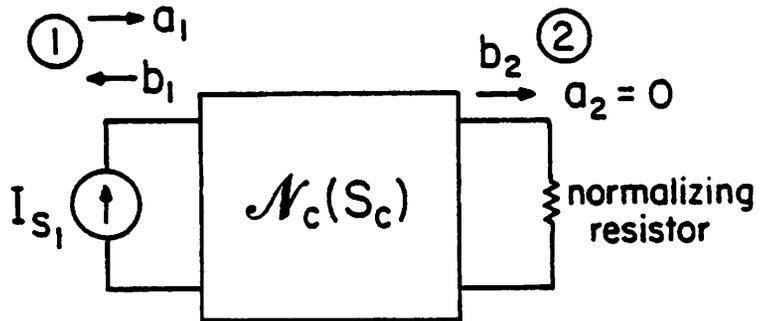


Fig. A.3.

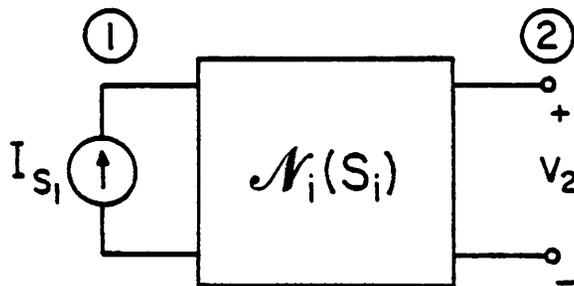


Fig. A.4.