

# Interfaces and Junctions in Nanoscale Bottom-Up Semiconductor Devices

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Interfaces and Junctions in Bottom-Up Nanoscale Semiconductor Devices

by

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Spring 2009

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\_\_\_\_\_ Date\_\_\_\_\_

University of California, Berkeley

Interfaces and Junctions in Bottom-Up Nanoscale Semiconductor Devices

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Yu-Chih Tseng

## **Abstract**

Interfaces and Junctions in Bottom-Up Nanoscale Semiconductor Devices

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Yu-Chih Tseng

Doctor in Philosophy in Engineering – Electrical Engineering and Computer Sciences

University of California, Berkeley

Professor Jeffrey Bokor, Chair

A semiconductor device is a system composed of multiple materials, and its functionality depends on the junctions and interfaces between these materials. This dissertation documents a study of junctions and interfaces in one-dimensional nanoscale semiconductor materials. Examined are the insulator interface and the dopant profile in vapor-liquid-solid (VLS)-grown silicon nanowires, the electronic properties of the native surface of InAs nanowires grown using bottom-up methods, and metal-carbon nanotube (CNT) Schottky contacts. The capacitance-voltage (C-V) measurement is refined to examine these junctions and interfaces. For a Si nanowire, the C-V measurement shows that the density of trap states on its interface with  $\text{Al}_2\text{O}_3$  insulator ranges from  $\sim 10^{11}/\text{cm}^2\cdot\text{eV}$  in the midgap to  $\sim 10^{13}/\text{cm}^2\cdot\text{eV}$  closer to the valence band edge. The boron profile in Si nanowires is found to agree well with predictions from interstitial and vacancy-assisted diffusion model, as in bulk Si. For an InAs nanowire, the C-V technique is used to extract the trap density of its native surface, which is  $\sim 3.8 \times 10^{11}/\text{cm}^2\cdot\text{eV}$  in the mid-gap and  $\sim 10^{13}/\text{cm}^2\cdot\text{eV}$  near the conduction band edge. The trap lifetime in

these InAs nanowires is extracted using the C-V method as well. Accurate measurement of the gate capacitance in back-gated InAs nanowires is found to be necessary to determine accurately the electron mobility. The impact of metal-CNT Schottky contacts on the transistor performance and leakage is examined as well. It is found that both the on-state current and off-state leakage depend strongly on the Schottky Barrier Height (SBH) at the contacts. The scaling of the SBH with the CNT diameter shows that the length of the electrical junction is about 25nm. The metal-CNT Schottky junction is also studied using a new instrument capable of measuring rapidly attofarad ( $10^{-18}$  F)-level capacitances. This study confirms the unpinned nature of the metal-CNT Schottky contact, and shows a way to directly determine the height of that energy barrier.

The dissertation abstract of Yu-Chih Tseng is approved:

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Professor Jeffrey Bokor, Chair

Date

*To My Parents*

*Ming-Ho Tseng and Ai-Chiao Liu*

*For Their Love*



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# Introduction

Any solid-state semiconductor device is a material system. Be it a MOS transistor, bipolar junction transistor, PN diode, Schottky diode, photodiode or solar cell, any functional solid-state device requires the coming together of materials across a large spectrum of electrical conductivity, ranging from oxides for gate insulator to semiconductors for transistor channel, to metals and their alloys for electrical contact. The electrical properties of each constituent of a device influence only partly the overall function. More often than not, the interface between two materials is equally important. The PN junction is the most fundamental example. It is because of the space-charge region at the interface between the two oppositely-doped materials that diodes can rectify, and that electron-hole pairs generated in solar cells can be separated. Another example is the metal-semiconductor contact, which can rectify because of the Schottky

barrier between the metal and the semiconductor. It can also be ohmic if the substrate is sufficiently doped. The oxide-semiconductor interface in a MOSFET is yet another important example. Because the current flowing in a MOSFET is located directly under the gate oxide, a poor interface can strongly degrade the transistor's performance.

# Periodic Table of the Elements

hydrogen

alkali metals

alkali earth metals

transition metals

poor metals

nonmetals

noble gases

rare earth metals

1 H																	2 He														
3 Li	4 Be																	5 B	6 C	7 N	8 O	9 F	10 Ne								
11 Na	12 Mg																	13 Al	14 Si	15 P	16 S	17 Cl	18 Ar								
19 K	20 Ca	21 Sc	22 Ti	23 V	24 Cr	25 Mn	26 Fe	27 Co	28 Ni	29 Cu	30 Zn	31 Ga	32 Ge	33 As	34 Se	35 Br	36 Kr														
37 Rb	38 Sr	39 Y	40 Zr	41 Nb	42 Mo	43 Tc	44 Ru	45 Rh	46 Pd	47 Ag	48 Cd	49 In	50 Sn	51 Sb	52 Te	53 I	54 Xe														
55 Cs	56 Ba	57 La	72 Hf	73 Ta	74 W	75 Re	76 Os	77 Ir	78 Pt	79 Au	80 Hg	81 Tl	82 Pb	83 Bi	84 Po	85 At	86 Rn														
87 Fr	88 Ra	89 Ac	104 Unq	105 Unp	106 Unh	107 Uns	108 Uno	109 Une	110 Unn																						
																		58 Ce	59 Pr	60 Nd	61 Pm	62 Sm	63 Eu	64 Gd	65 Tb	66 Dy	67 Ho	68 Er	69 Tm	70 Yb	71 Lu
																		90 Th	91 Pa	92 U	93 Np	94 Pu	95 Am	96 Cm	97 Bk	98 Cf	99 Es	100 Fm	101 Md	102 No	103 Lr

**Figure I1:** Elements used in an integrated circuit, compiled from a survey of published literature [1-9]. Red: elements used in first integrated circuits, circa 1970. Blue: new elements incorporated in ICs, circa 2004. Orange: under research.

Early semiconductor devices and circuits involved few materials: silicon and its natural oxide, a few dopant elements, and a few metals to make contacts and interconnects. Today, integrated circuits involve many more elements in the periodic table (figure I1), and more exotic compounds to meet advanced performance and reliability benchmarks, while being ever smaller. Examples include Ge for straining the channel[1],  $\text{HfO}_2$  and  $\text{ZrO}_2$  for gate dielectric[2,3], Mo and its associated compounds

for gate[4], C in low-k interlayer dielectrics [5], W in vias[6], Co, Ni in silicides [7], and As, Sb for low-diffusivity dopants. Many other elements and compounds, such as PtSi[8], SrTiO[9], are also investigated as well.

As a result of this material “diversification”, interface properties are ever more important, and start to impose limits on device design and performance. The requirements for the interface between the gate dielectric and silicon complicate considerably the material choice for high-k dielectric. In highly-scaled transistors, the contact between highly doped source/drain and metal is the largest contributor of parasitic resistance that lowers the drive current. Controlling short-channel effects requires ever shallower and more abrupt junctions that are increasingly difficult to make using existing process technologies.

As individual transistor shrinks in size, there is a growing interest in a new class of one-dimensional semiconductor materials. These, represented by carbon nanotubes and nanowires of various semiconductor materials, are synthesized using chemical and self-assembly methods, and cannot be easily manufactured starting from bulk materials. These nanowires and nanotubes offer new possibilities. In carbon nanotubes, for example, carrier scattering is greatly reduced, leading to high carrier mobility, suitable for high-performance transistors[10]. The mere shape of these nanotubes and nanowires makes it easy to fabricate devices with new geometry, such as surround-gate transistors with optimal electrostatic control[11].

The performance of these nanotube and nanowire transistors depends, just like their counterpart in bulk, on proper engineering of their interfaces and junctions with other materials. Semiconductor carbon nanotubes, for example, usually form Schottky contacts with metals, and such a junction can dictate completely the device's behavior [12]. In Si nanowires, it has been shown that the conditions at the surface can alter the carrier mobility considerably[13]. A similar behavior is observed in other type of nanowire devices.

Unlike bulk materials, there are no systematic studies of the interfaces of these bottom-up materials, with the exception of transport across CNT Schottky contacts. The primary reason is the small size of these nano-objects, which precludes the usage of common surface characterization techniques such as XPS, capacitance-voltage, DLTS, admittance spectroscopy, or SIMS. Additionally, these nano-objects generally vary greatly in size, and assembling many of them with a long-range order, in a way that unambiguous information can be obtained, is still a challenge.

This thesis describes the investigation of some basic junctions in these novel one-dimensional semiconductors using capacitance-voltage measurements, extended to very low levels. Conventional instrumentation for this technique requires test capacitors with an area in the order of  $100\mu\text{m} \times 100\mu\text{m}$ . As a result, this technique was only applicable to bulk materials. In this work, this technique is extended to a much higher precision in order to directly characterize an individual junction of small area. The first application is to examine the dopant distribution in a VLS-grown silicon



nanowire and surface trap density at the interface between it and  $\text{Al}_2\text{O}_3$  dielectric. Second, the native surface of an InAs nanowire is examined. Third, a widely studied junction, the metal-carbon nanotube Schottky junction, is re-examined to study its impact on the performance of CNT transistors, and we further investigate this junction in detail using the capacitance-voltage technique.

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# Chapter 1

## Ultra Low-Level Capacitance Measurement

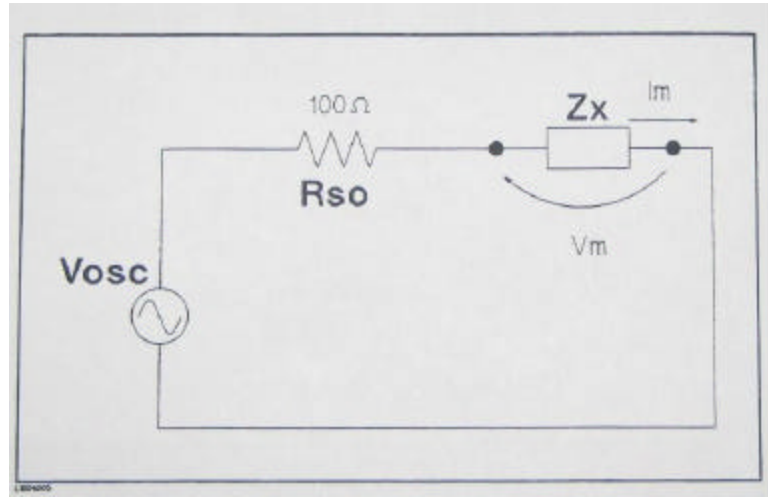
There are several related techniques for characterizing the electronic properties of surfaces, interfaces and junctions in semiconductor materials. Probably the most commonly used method is the capacitance-voltage (C-V) measurement. It is a versatile and straightforward way of measuring simple parameters such as the static dielectric constant  $\epsilon$ , and the effective dielectric thickness  $T_{ox}$ . Frequency- and temperature-dependent C-V measurements give information on interface trap density ( $D_{it}$ ), and the lifetime of these traps. When applied to a diffused junction or a Schottky junction, one can extract material parameters such as the spatial distribution of dopants, as well as the Schottky barrier height.

## 1.1 Requirements for the C-V measurement and the usual laboratory apparatus

The requirements for making good C-V measurements are very straightforward. First, the C-V meter should be able to operate across a wide frequency range and to resolve both capacitive and resistive components. Commercial C-V meters, usually RLC analyzers, do this very well. Second, the test structure must be of sufficient size and quality. A typical on-chip capacitor test structure needs to have an area of about  $100\mu\text{m} \times 100\mu\text{m}$ , to provide enough area for making contact with probe tips, and to provide enough signal to be resolved by the C-V meter. In addition, the dielectric needs to be insulating and robust enough to ensure low leakage, such that the resistive component does not overwhelm the capacitive component, and that the dielectric does not breakdown too easily during the measurement.

A commonly used RLC analyzer is the HP4284A, which applies an AC voltage across the device under test (DUT) and measures the amplitude and phase of the current through the DUT using a built-in ammeter. A circuit schematic (figure 1.1) from the HP4284A operating manual shows the general working principle. Depending on the chosen circuit model, the R,L,C parameters can be extracted. Unfortunately, the HP4284A is limited by its poor current resolution (1nA) [1]. For an applied AC amplitude of 25mV, the smallest impedance that can be resolved is about 25Mohm, which translates to about 300aF at 20MHz. In practice, measurements are often performed at much lower frequencies, and the resolution is significantly worse as a result. Also, to obtain an accurate measurement, the applied AC amplitude can not be

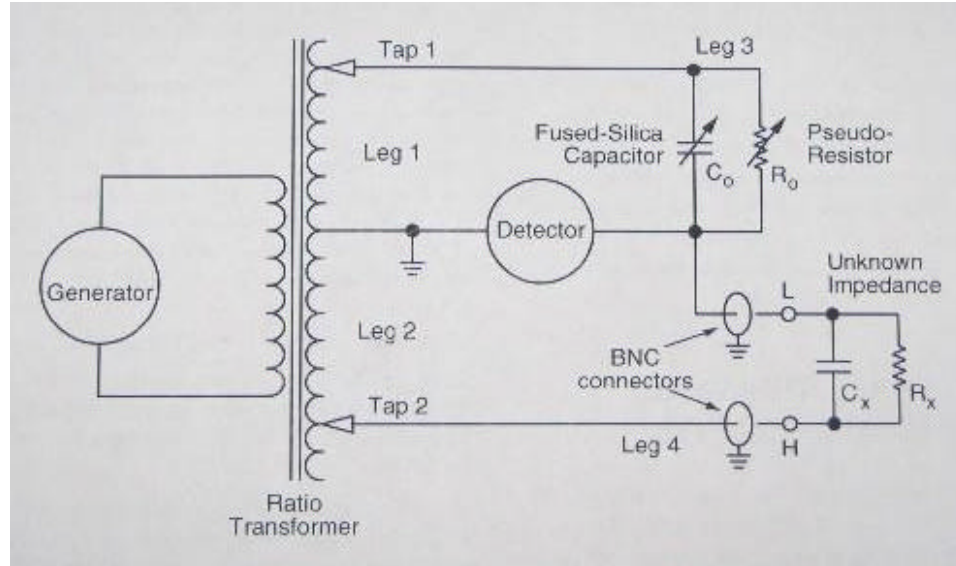
larger than the voltage step size, placing therefore a lower limit to the signal-to-noise ratio.



**Figure 1.1:** Basic working principle of the HP4824A impedance analyzer.

$I_m$  is measured for known  $V_{osc}$ .

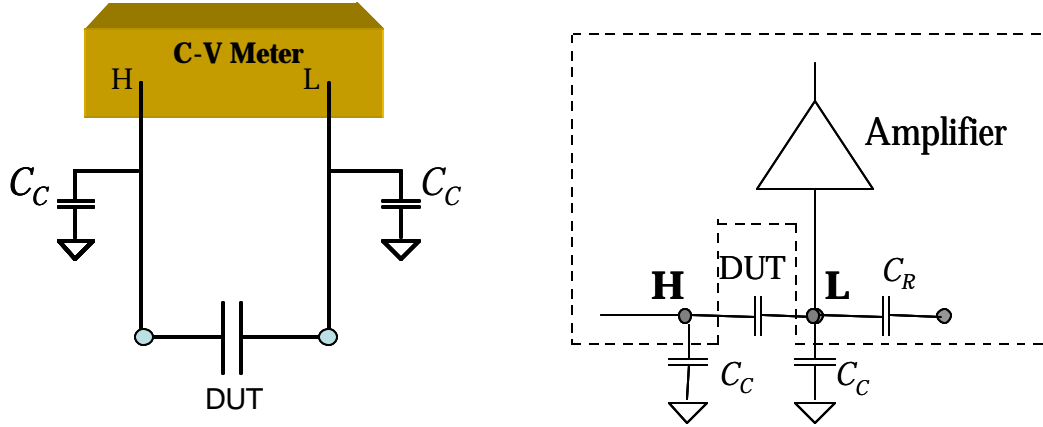
Alternatively, a capacitance bridge such as the Andeen-Hagerling AH2700A can be used to perform the C-V measurements with a much higher precision. This instrument is very similar to a Wheatstone bridge, and owes its precision to low-noise capacitance standard elements and built-in electronics. AH2700A has been employed recently with great success to measure a variety of small capacitances [2,3], and is used in part of the work that follows. When using this instrument, the DUT is connected as shown in figure 1.2 [4]. By adjusting the passive elements  $R_o$  and  $C_o$  in figure 1.2, the bridge can be balanced by nulling the input to the detector. When very long averaging times are used (>24hrs), a resolution of  $\sim 2\text{aF}$  can be obtained.



**Figure 1.2:** Circuit Schematics of the AH2700A capacitance bridge.

In the capacitance bridge described above, a basic limitation is the parasitic capacitance  $C_c$  associated with the cables connecting the DUT to the meter. The parasitics from the cables can be represented schematically in figure 1.3. In the bridge, the AC signal is supplied from the ‘high’ node (H). While  $C_c$  at the high node (H) of the DUT causes at most a slight phase rotation of the incoming signal,  $C_c$  at the low node (L) acts as a capacitor divider and shunts the AC signal to ground, especially when the capacitance of the DUT is very small in comparison to  $C_c$ . As a result, the signal reaching the detector is extremely feeble and not obviously different from zero, even when the bridge is not balanced. When this meter is set up in a typical laboratory, cable length in the order of 2m is needed, resulting in a capacitance  $C_c$  in the order of 200pF. For a typical AC excitation of 25mV, and a sample capacitance of 200aF (typical of micron-scale objects), the parasitic  $C_c$  reduces the AC signal reaching the detector to 25nV, which is difficult to resolve unless a long averaging time is used. If an even

smaller energy resolution is needed, especially in a low temperature experiment, then an even smaller AC excitation is required. For smaller capacitances this “brute-force” method would take an impractically long averaging time.



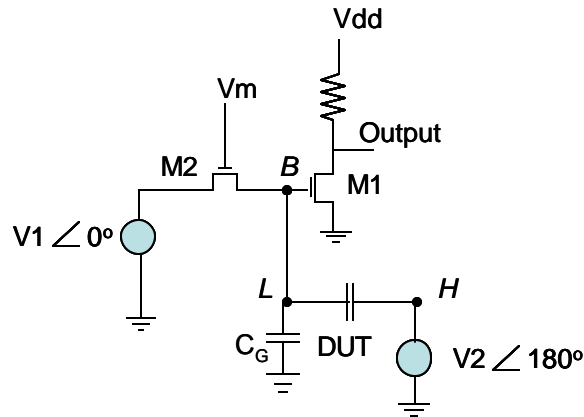
**Figure 1.3:** Schematic representation of the parasitic capacitances from the cables. The dashed line encloses components internal to the C-V bridge. DUT: Device Under Test.  $C_x$ : internal reference capacitor.  $C_c$ : parasitic capacitance between the signal and ground of the BNC cable.

## 1.2 The Cold Bridge

While the commercial bridge AH2700A is adequate for fairly large capacitances ( $>100\text{aF}$ ), it is less so for much smaller ones because of the cables. A simple solution is to reduce the distance between the DUT and the meter, but the cables can not be shortened very much if a probe station is required to make contact to the DUT. Furthermore, the electronics inside the AH2700A would still operate at room temperature, where the Johnson noise places a lower limit to the input noise of the detector.

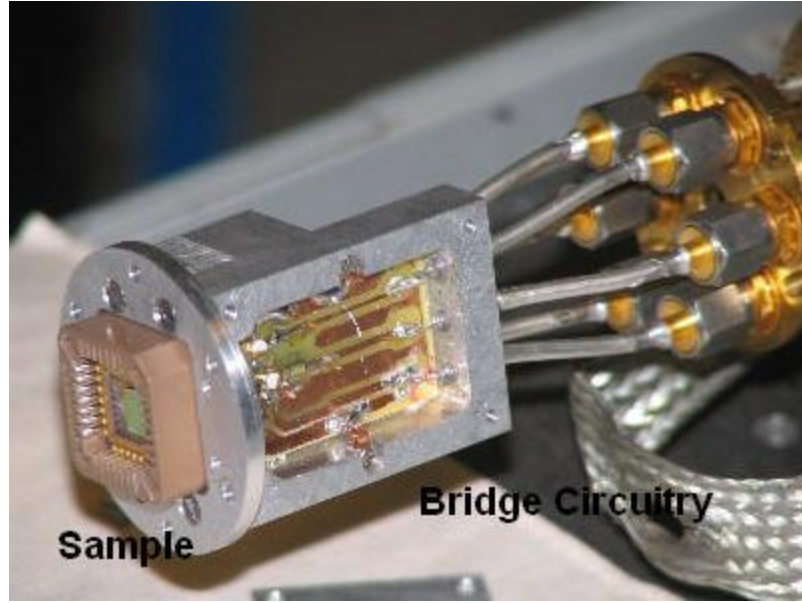
However, the basic improvements are clear: shorten the cables and operate at low temperatures. Ashoori pioneered the use of ultra-low capacitance spectroscopy to examine single electron charging in low-dimensional structures[5], by placing the bridge on the same chip as the sample. Subsequent refinement by his group[6] consists of mounting a similar apparatus on the tip of a scanning probe to perform spatially-resolved capacitance spectroscopy. While impressive, the apparatus they developed lacks the modularity that would allow the measurement of an arbitrary device. The instrument described in this thesis allows one to apply this technique in a much more general and flexible way to an arbitrary device.

The circuit schematic of the cold bridge is described in figure 1.4, and the photo of the actual apparatus in figure 1.5. By shortening the distance between the low end of the DUT and the detector input to about 0.5cm, the parasitic shunt capacitance to ground is about 6pF, or less than 1/20 of the cable length needed in a typical laboratory setting.



**Figure 1.4:** Circuit schematic of the Cold Bridge.  $V_1$ ,  $V_2$  are AC sources  $180^\circ$  apart in phase. M1 is a discrete HEMT transistor used to amplify the signal at B. M2 is also a discrete HEMT transistor.  $C_G$  represents the total capacitance between B and ground. Note that the amplifier M1 is inverting.





**Figure 1.5:** Photo of the actual Cold Bridge.

### 1.3 Operating the Cold Bridge

To measure capacitances with the cold bridge, one balances the bridge so that voltage at the balance point ‘*B*’ illustrated in figure 1.4 is minimized (to zero in theory), by varying the amplitude of one of the AC sources ( $V_1$ ,  $V_2$ ). These two AC sources are  $180^\circ$  apart in phase so their contribution subtract from each another. The voltage at the balance point *B* is simply:

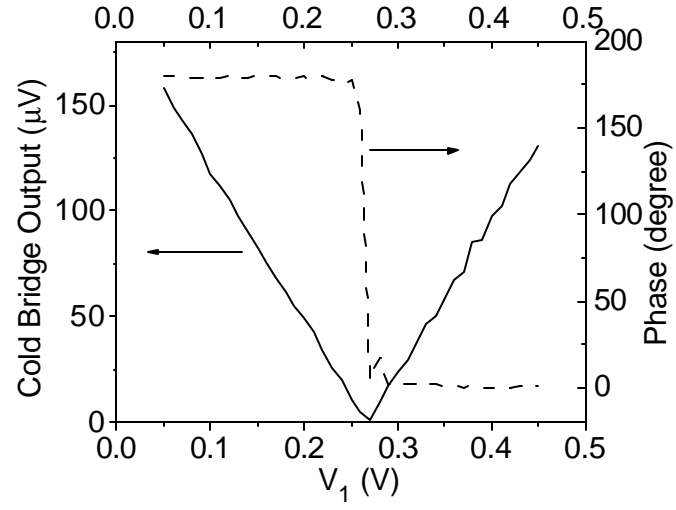
$$V_B = V_1 \left( \frac{C_R}{C_R + C_G + C_{DUT}} \right) - V_2 \left( \frac{C_{DUT}}{C_R + C_G + C_{DUT}} \right) \quad (1.1)$$

, where the negative sign is due to the out-of-phase  $V_2$ . When balanced,  $V_B=0$ , and the numerical value of the capacitance can then be extracted using this simple formula:

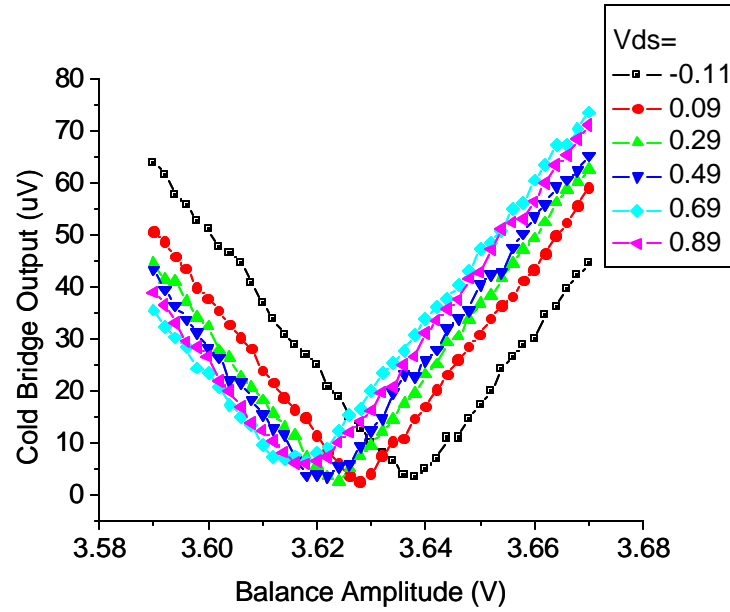
$$V_1 C_R = V_2 C_{DUT} \quad (1.2)$$

, where  $C_R$ ,  $C_G$ ,  $C_{DUT}$  are respectively the capacitor representing the reference, parasitics to ground and device under test. When biased by  $V_M$  to be almost completely off, the discrete HEMT transistor (M2) serves as the reference capacitor  $C_R$ . This scheme has the added advantage that a separate high-resistance DC path to bias the amplifier M1 is unnecessary. In fact, the presence of that high resistance DC path, in the form of a large resistor, would be detrimental to the signal-to-noise ratio since it further reduces the incoming AC signal by shunting it to ground, and acts as a significant noise source for M1. The voltage-adjustable M2 provides a convenient way to bias M1 and acts as a reference capacitor simultaneously. An added bonus is that, by turning on M2, I-V characterization of the DUT can be performed in-situ, without having to remove the device from the setup. The precise value of  $C_R$  can be measured it using the AH2700A commercial bridge, and is 0.37pF in our case.

A typical balancing curve is shown in figure 1.6. It is simply the output of the bridge as a function of the amplitude of  $V_I$  (see figure 1.4). As expected, the bridge goes through a minimum (the balance point), accompanied by an abrupt change in the phase from 0 to 180 degree, evidence that contribution from AC source  $V_I$  has become larger. In all devices of interest in this work, the capacitance of the DUT changes with bias applied across it. When this happens, we should expect the balance curve to simply shift horizontally with applied bias, as illustrated in figure 1.7.



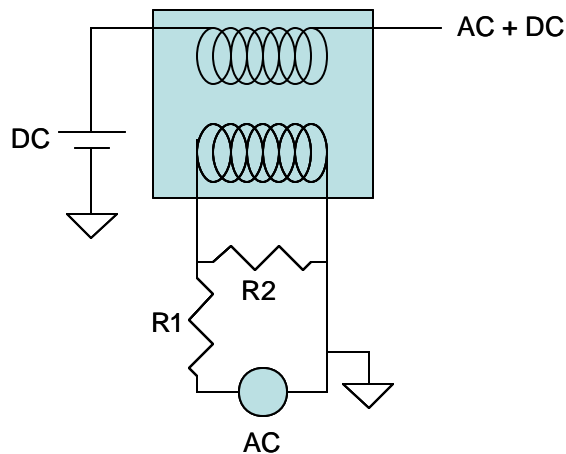
**Figure 1.6:** Output of the cold bridge as a function of the amplitude of AC source  $V_I$ . Solid: amplitude. Dashed: phase.



**Figure 1.7:** Output of the cold bridge as a function of the amplitude of AC source  $V_I$ , with varying DC bias applied across the DUT. The DUT is a carbon nanotube Schottky diode.

## 1.4 Full setup

The full measurement setup outside of the cold bridge is described below for future reference. First, the phase between the two AC sources is carefully trimmed to be as close to  $180^\circ$  apart as possible. The instruments used for the AC sources are the internal sine generator of the SR830 lock-in amplifier and the HP3312A function generator, whose phase can be adjusted relative to an external trigger. This phase adjustment is necessary to ensure that the bridge output is as small as possible when balanced, and that the simple formula 1.2 can be applied to extract the capacitance of the DUT. Also, as obvious from figure 1.4, the DC bias applied across the DUT for C-V measurement needs to be added to  $V_2$ , and another DC voltage is needed to bias the transistor M1, and should be added to  $V_1$ . The addition of the AC source to the DC source is done passively to avoid introducing additional noises. This is done using an audio-frequency transformer (TRIAD magnetics TF5S1ZZ), as illustrated in figure 1.8. The appropriate AC voltage levels are obtained using resistor-based voltage dividers.



**Figure 1.8:** Adding AC voltage to DC passively using an audio-frequency transformer (TRIAD magnetics TF5S1ZZ). When needed, the AC source is divided resistively using R1 and R2, with typical  $R2/R1 \sim 10^{-4}$ .

## 1.5 Noise Performance of the Cold Bridge

With all components of the bridge optimized and using a lock-in amplifier to reject unwanted noise, the bridge has a noise figure of about 0.3 electrons /  $\text{Hz}^{1/2}$  at 77K. Using a typical AC excitation of 20mV and an averaging time of about 120s per data point, the noise figure translates into a capacitance resolution  $\Delta C$  of:

$$\Delta C = \text{Noise Figure} \times \sqrt{\text{Effective Bandwidth}} \times \text{AC Voltage} \quad (1.3)$$

$$\Delta C = 0.3 \frac{e}{\sqrt{\text{Hz}}} \times \sqrt{1/120} \times 20\text{mV} = 1.4\text{aF} \quad (1.4)$$

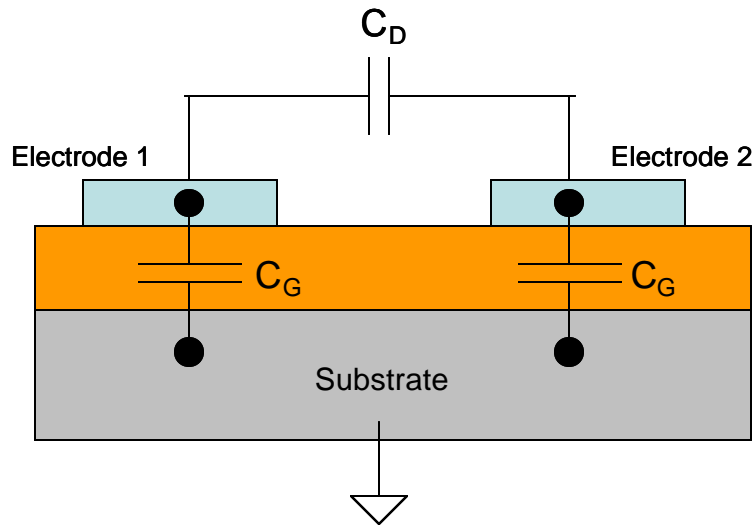
With a larger AC excitation or greater patience, the bridge can easily resolve capacitances lower than 1 aF.

The capability to measure small capacitances allows for the characterization of individual nanoscale semiconductor devices. As an example, the dimensions of an end-of-the-roadmap silicon MOSFET [7],  $L_g = W = 8.8\text{nm}$  and  $EOT = 0.5\text{nm}$ , lead to a capacitance of  $\sim 5.3\text{ aF}$ , well within the capability of the instrument described above.

## 1.6 Device layout and design to minimize background capacitance

Although the cold bridge is designed to accept an arbitrary device, there are restrictions to the device layout. Illustrated in figure 1.9 are the various parasitic

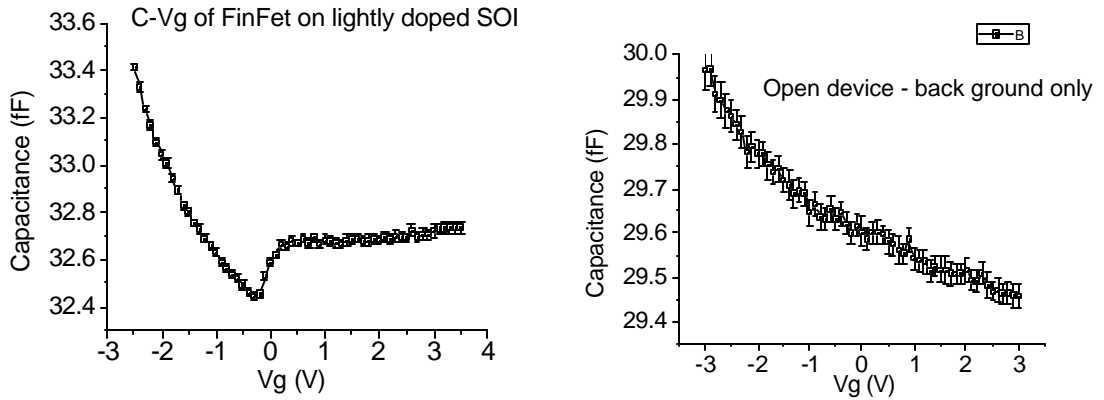
capacitances. The first restriction is the density of devices. Unfortunately, floating electrodes increase the background capacitance significantly, and resolving a small change in capacitance relative to a large background, even if it stays constant, presents a challenge since the instruments (e.g. lock-in amplifier) have only a resolution of at most 4 decimal places, and can therefore resolve only changes of 1 part in  $10^4$ , and only barely so. A 3mm x 3mm chip (typical size of the sample) densely packed with floating electrodes has about 20 to 30fF of background capacitance. In contrast, when the device density is reduced to one per 5mm x 5mm chip, with no floating electrodes, the stray capacitance diminishes to 0.2~0.4fF, coming from  $C_D$  in figure 9. Increasing the distance between the electrodes reduces  $C_D$  further, with <0.1fF for electrodes 4um apart (figure 1.9).



**Figure 1.9:** On-chip parasitics between two electrodes and the substrate.  $C_D$  is the capacitance between the metal electrode 1 and 2.  $C_G$  is the capacitance between the substrate and the metal electrodes.

The second design constraint concerns the substrate. The DUT should ideally be on a SOI substrate with a heavily doped handle wafer. The heavy doping is

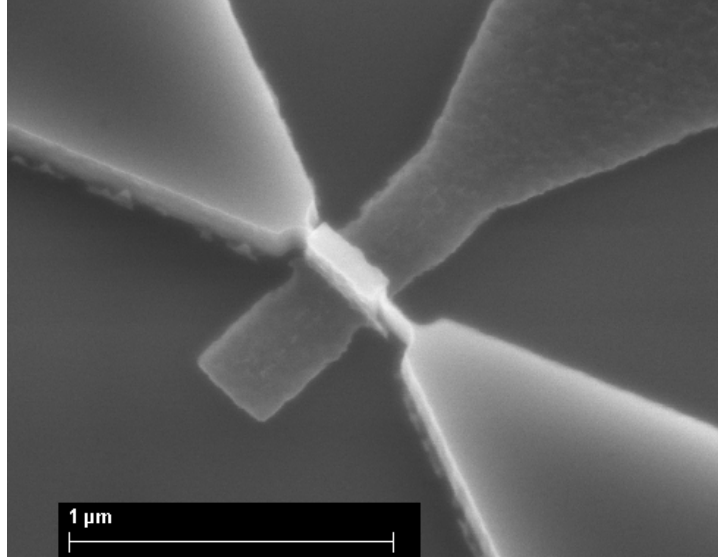
necessary to prevent the substrate from being depleted by voltage applied to the electrodes. If the substrate can be depleted, the background capacitance will not stay constant with applied bias, even if there is no device between the two electrodes. Figure 1.10 illustrates this difficulty when measuring a FinFET fabricated on a lightly doped SOI (figure 1.11). In general, it would also be difficult to subtract the background signal from a control device, since each device has a slightly different background contribution from bonding wires. However, it should be noted that the capacitance step in the left of figure 1.10 is about 160aF, agreeing reasonably with an estimated  $C_{ox} = 220\text{aF}$  based on device geometry alone.



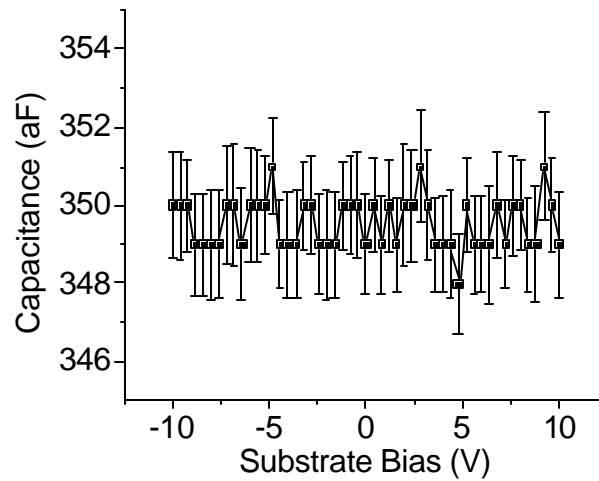
**Figure 1.10:** C-V measurement of a FinFET ( $L_g=150\text{nm}$ , fin width= $30\text{nm}$ , fin height= $200\text{nm}$ ,  $T_{ox}\sim 10\text{nm}$ ). Left: C-V of the device. Right: C-V between two contact pads of the same geometry, but with no transistor between them.

The third design limitation is the size of the bonding pads. Since the substrate is grounded, the bonding pads increase the shunt capacitance to ground  $C_G$ , in parallel with the cables. As discussed previously, a large  $C_G$  leads to low signal-to-noise ratio

and reduces resolution. A typical bonding pad is a  $75\mu\text{m} \times 75\mu\text{m}$  square on an oxide layer 500nm in thickness, giving a tolerable  $C_G = 0.38\text{pF}$ . When these design limitations are satisfied, the background capacitance is constant to better than 2aF, within the error bars, as illustrated in figure 1.12.



**Figure 1.11:** SEM image of the FinFET measured in figure 1.10. Capacitance is measured between the gate (top right), and the source/drain electrodes (upper left and lower right), which are shorted together.

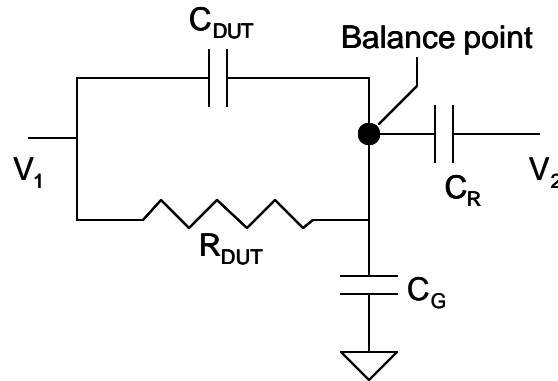




**Figure 1.12:** Capacitance between two metal electrodes 1 $\mu$ m apart, as function of the substrate bias. No device exists between the electrodes. The substrate is heavily doped with boron to at least  $10^{19}/\text{cm}^3$ .

## 1.7 Dealing with losses

When measuring small capacitances, even a seemingly large resistive component in parallel of the capacitor can make the loss unmanageable. Lossy capacitors are encountered in very thin or leaky dielectrics, heavily doped junctions, and Schottky diodes. As an estimate, for  $C=100\text{aF}$  measured at  $10\text{kHz}$ , a resistance of  $160\text{GOhm}$  is sufficient to produce a loss tangent of 1, making the simple formula 1.2 unapplicable. Instead, a more complicated circuit model that includes the resistor in parallel must be used (figure 1.13) and the capacitance extracted using linear circuit analysis.



**Figure 1.13:** Parallel model for lossy capacitor. The loss is modeled by the resistor  $R_{DUT}$  in parallel with the capacitor.

Linear circuit theory gives the voltage  $V_B$  simply as:

$$V_B = V_1 \left( \frac{Y_{DUT}}{Y_t} \right) - V_2 \left( \frac{Y_R}{Y_t} \right) \quad (1.5)$$

Where  $Y_x = 1/Z_x$  is the admittance between any node  $x$  to node  $B$  in figure 1.13, and  $Y_t$  is the sum of the admittances joining the balance point and the other three nodes. Further simplification gives the real and imaginary parts separately:

$$V_B = \frac{1}{j\omega C_G} \left( \frac{V_1}{R_{DUT}} \right) + \frac{j\omega}{j\omega C_G} (C_{DUT} V_1 - C_R V_2) \quad (1.6)$$

$$\angle V_B = \frac{V_1 / R_{DUT}}{\omega (C_{DUT} V_1 - C_R V_2)} \quad (1.7)$$

The approximation  $Y_t \sim Y_G$  was employed, since the parasitic  $C_G$  (6pF) is considerably larger than other capacitors. Using equations 1.5 to 1.7, both resistive and capacitive components can be deduced in principle.

## 1.8 Summary

The above describes the instrument and the methods used to measure very small capacitances. The innovation brought here is the modularity designed into the instrument to enable the measurement of an arbitrary device, provided that it satisfies the design constraints. Methods are also developed to reproduce essentially all the capabilities of a commercial bridge, only with much better capacitance resolution.

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# Chapter 2

## Diffused junction in a silicon nanowire

Semiconductor nanowires are useful in several applications, including biochemical sensing, computing and energy harvesting[1,2,3,4,5]. However, important material parameters such as the dopant distribution and surface state density have not been measured in nanowires. Here, C-V method is applied directly to a single silicon nanowire surround gate field effect transistor to extract the radial dopant distribution and interface state density. The methods previously used [6] to determine the dopant density rely on several untested assumptions that can lead to very large uncertainties. For example, the dopant concentration is typically extracted by making nanowire field effect transistors (FETs) and using the conductivity in conjunction with the measured

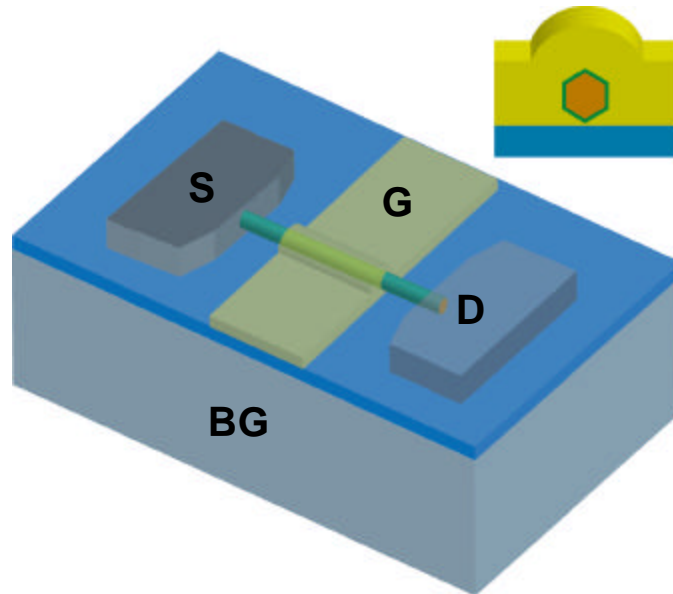
mobility and threshold voltage[7,8,9]. These methods rely on the calculated gate capacitance and assume a uniform dopant distribution and known surface (or interface) charge density. In planar devices, the above assumptions can be tested using the capacitance-voltage (C-V) technique[10], and the same method is applied here to a nanowire device.

Previous reports on direct C-V measurements on nanowires exist, but these are concerned with measuring the oxide capacitance for the purpose of mobility extraction[11,12]. Accurate mobility measurements are important, and a similar study performed on individual InAs nanowires is presented in the next chapter. A recent study of InAs nanowires addresses the issue of interface trap density, but it was performed on a large ensemble of wires having a large size distribution, and inconsistent electrical contacts[13].

The work presented in this chapter demonstrates the application of C-V measurements on a silicon nanowire transistor, fabricated using a bottom-up method. The interface state density  $D_{it}$  as a function of the energy position inside the bandgap is extracted with the high-low method and the radial dopant profile is determined from high frequency C-V measurement. Finite element modeling (FEM) is used to support the results and to show the limitations in resolving the dopant profile using the C-V method. The results are also compared with those from planar metal oxide semiconductor capacitors.

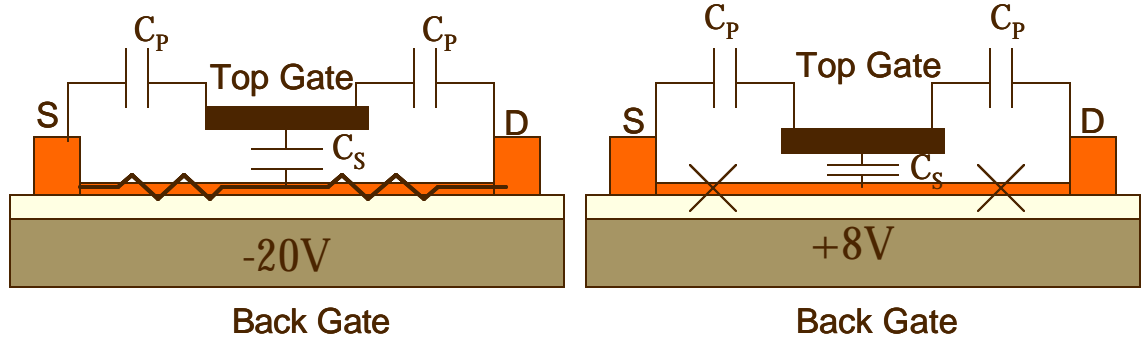
## 2.1 Design of test structure and measurement scheme

The test structure is similar to that proposed by Ilani et al[14]. Figure 2.1 illustrates the design of the structure. On an SOI wafer, a silicon nanowire bridges two heavily boron-doped silicon pads (S and D), about  $4\mu\text{m}$  apart. A high-k/metal gate stack surrounding the nanowire acts as the top gate. This gate stack, in series with the nanowire, effectively forms a MOS capacitor (MOSCAP). However,  $1\mu\text{m}$  of the nanowire from the source and the drain electrode is not covered by the top gate, and is instead gated by the back gate (BG). The back gate is used to extract the background parasitic capacitances.



**Figure 2.1** Device test structure for CV measurement. S/D: source and drain. G: top gate. BG: back gate. The cross section shows the wire under the top gate. A thin layer of aluminum oxide separates the nanowire channel from the top gate electrode. Credit: E.Garnett.

Capacitance is measured between the top gate and the source/drain electrodes, the latter two shorted together. In the first measurement, the back gate is negatively biased to turn on the exposed parts of the nanowire, and both the MOSCAP and the background parasitics contribute to the measured capacitance. In the second measurement, a large positive voltage applied to the back gate turns off the exposed parts of the nanowire, and the nanowire MOSCAP is not measured. The difference between these two measurements yield only the capacitance from the nanowire MOSCAP. The measurement scheme is illustrated in figure 2.2.



**Figure 2.2** Measuring scheme to extract background capacitance. Left: Negatively biased back gate leads to low resistance contact to the MOSCAP. Right: positively biased back gate turns off access the nanowire MOSCAP.

## 2.2 Device fabrication

Starting with (110) SOI wafers with heavily doped handle and device layers, standard microfabrication techniques are used to define silicon islands that serve as the source/drain electrodes. Gold nanoparticles with an average diameter of 80nm are then dispersed from solution onto the silicon islands. Vapor-liquid-solid growth of the nanowires at 830°C follows, catalyzed by the gold nanoparticles[15,16]. The silicon

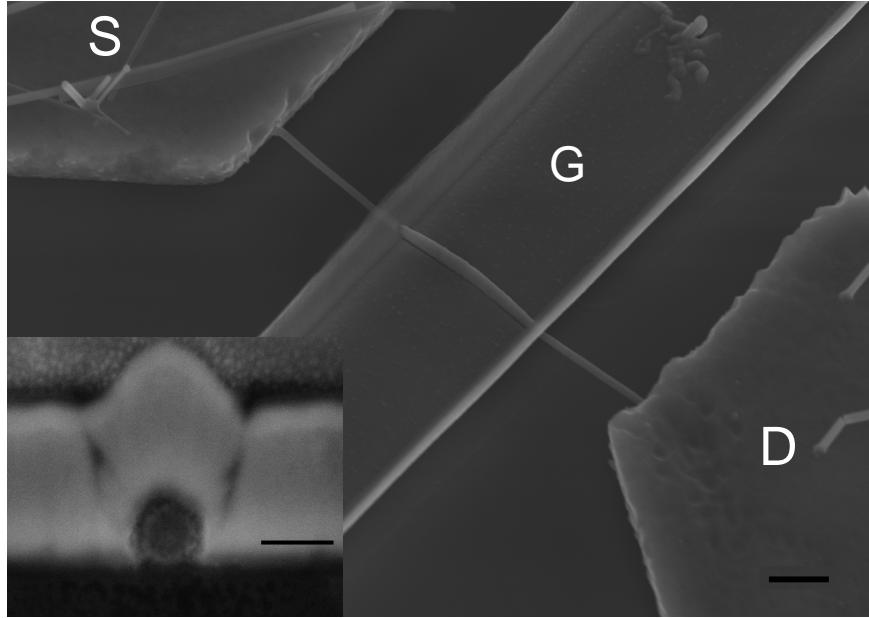


precursor is liquid  $\text{SiCl}_4$  kept at  $0^\circ\text{C}$ , bubbled into the furnace using a mixture of Ar and  $\text{H}_2$  (50 and 158 sccm, respectively). Since the growth is epitaxial, the long axis of the nanowires are generally perpendicular to the (111) planes of the silicon surface. It should be noted that the islands are aligned such that the direction the nanowires are expected to bridge is parallel to the (111) directions. A (110) wafer is used because it can be patterned such that the (111) surfaces are exposed, and that the (111) directions, to which the nanowires align, are in the plane of the wafer [17].

The nanowires are then doped with boron by annealing for 1 hour at  $675^\circ\text{C}$  with 500 sccm of carrier gas and 0.5 sccm of 1%  $\text{BCl}_3$  in Ar, followed by 15 minutes at the same temperature with the  $\text{BCl}_3$  line turned off. Using these process conditions, a dopant profile can be simulated using Tsupreme, a commercial semiconductor process simulation tool. The expected dopant profile is shown as the dark solid line in figure 2.9 (Na-diffusion). The  $\text{Al}_2\text{O}_3$  gate dielectric is deposited in a ALD chamber using alternating pulses of trimethylaluminum and water precursors. The surround gate metal is patterned via photolithography and chromium sputtering, followed by lift-off.

Figure 2.3 shows a completed Si nanowire FET. After all measurements of interest are performed, focused ion beam (FIB) milling is used to expose the buried part of the wire in order to measure the actual diameter. The wire appears to be fully embedded in the surround gate metal and epitaxially integrated into the silicon electrodes. The cross-sectional SEM shows a distinct contrast between the bright Cr surround gate and the dark  $\text{Al}_2\text{O}_3$  gate oxide, with a somewhat smaller contrast

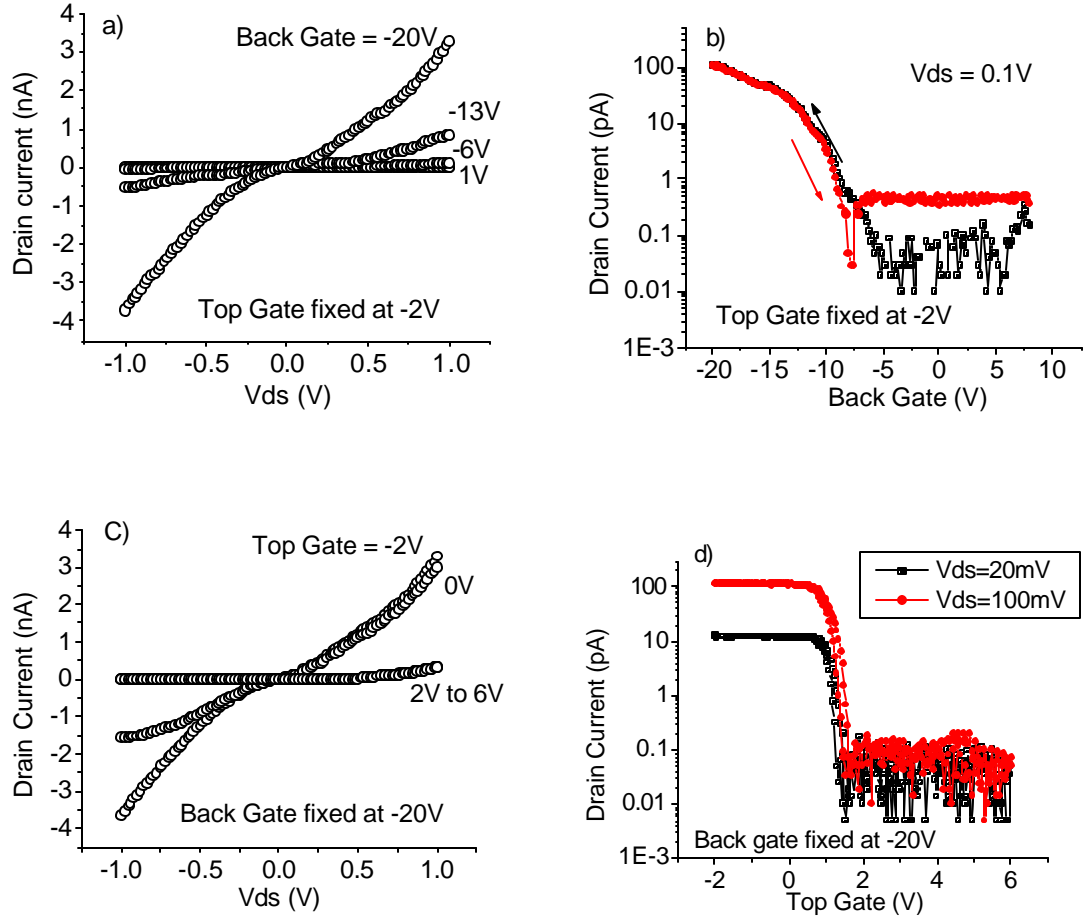
difference at the Si/Al<sub>2</sub>O<sub>3</sub> interface. The cross-sectional and top view SEM images show a gate length of 2.3 microns, Si nanowire diameter of about 75 nm and Al<sub>2</sub>O<sub>3</sub> thickness of about 15 nm. The thickness of the Al<sub>2</sub>O<sub>3</sub> is consistent across a large (cm<sup>2</sup>) area, and with a TEM measurement on control samples.



**Figure 2.3** SEM picture of an actual nanowire device. The inset is a cross-sectional view of the device taken after focused ion beam (FIB) milling. The scale bars are 1 μm (main panel) and 100 nm (inset). Credit: M. Fardy.

Figure 2.4a-d show the output characteristics ( $I_d$ - $V_d$ ) of the device and transfer characteristics ( $I_d$ - $V_g$ ) relative to the back gate and the top gate. Although the on-state resistance is rather high ( $\sim 0.3 \text{ G}\Omega$ ), it is not important for the purpose of extracting interface state densities and dopant profile. All that is required is a sufficiently low source/drain contact resistance so the MOSCAP can be accessed, and that the back gate can turn off the nanowire sufficiently well to allow the extraction of background capacitance. The slight non-linearity at low  $V_{ds}$  in figure 2.4a suggests that the source

or drain contact may be a Schottky contact, possibly because of residual oxide on the surface of the trench sidewall. It should also be noted that there is very little hysteresis in figure 2.4b, despite the application of very large voltages. This suggests that the effect of bias-induced stress and charge injection from the gates are very small.

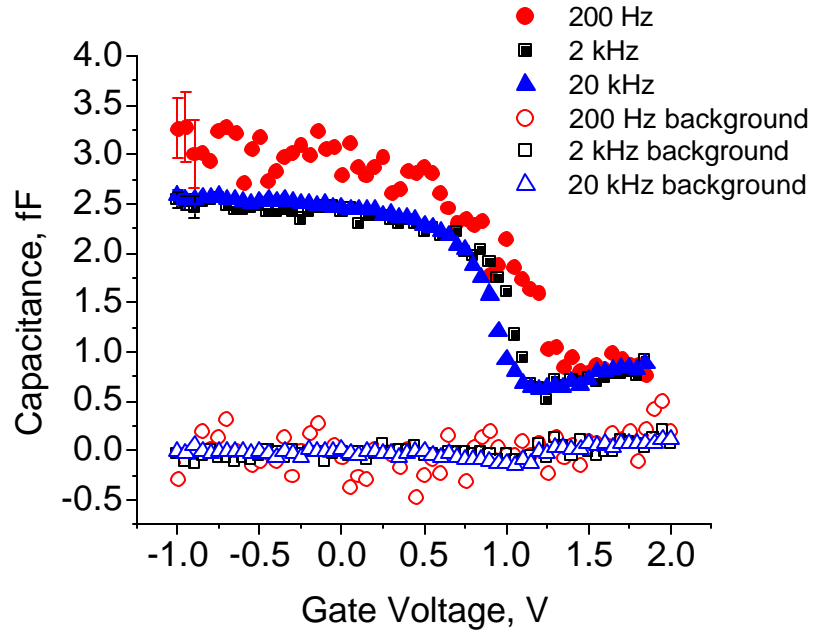


**Figure 2.4** a) Output characteristics ( $I_d$ - $V_d$ ) of the device in figure 2.3 as a function of the back gate. The top gate is fixed at -2V. b) Transfer ( $I_d$ - $V_g$ ) characteristics, vs the back gate, of the Si NW transistor shown in figure 2.3. c)  $I_d$ - $V_d$  for various top gate voltage. The back gate was -20V. d)  $I_d$ - $V_g$  characteristics, vs the top gate.

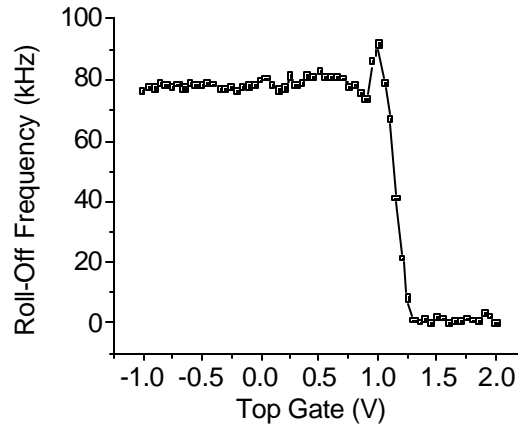
### 2.3 The capacitance measurement

Since the furnace for growing the nanowires accommodates only substrates no wider than 1", it is necessary to have a large device density on each chip to obtain a usable number of devices. On a single test chip, there can be more than 100 silicon islands, leading to a large parasitic background capacitance of about 20fF. Nevertheless, the measurement method is precise to less than 10aF, and the large background only presents a minor inconvenience. Electrical contacts are made to the source, drain and gate electrodes by wirebonding from a ceramic package to the degenerately boron-doped silicon source and drain pads and the chromium surround gate. Appropriate ultrasonic power is used to break through the  $\text{Al}_2\text{O}_3$  layer covering the source and drain. The series resistances from these wirebonds are negligible compared to that of the nanowire.

Following the scheme in figure 2.2, the capacitance is measured using the Andeen-Hagerling AH2700A with an AC amplitude of 20 mV at 77K, with sufficiently long averaging times. Figure 2.5 shows the silicon nanowire C-V response at 200 Hz, 2 kHz and 20 kHz with the back gate set at -20 V. The background capacitance is measured with the back gate set at +8 V. Both measurements are repeated at the 3 frequencies. The C-V curves clearly show the expected accumulation and depletion regions. At larger positive gate biases (not shown), inversion does seem to occur, but the data in that regime is not expected to be accurate since the contact to the wire is p-type, and the access resistance to a n-type inversion layer would be a large one.



**Figure 2.5** Capacitance-voltage measurements. Capacitance-voltage curves measured at 77K and 200 Hz (red), 2 kHz (black) and 20 kHz (blue), with the background shown in the corresponding open symbols. The error bars are shown only for the first 3 data points for clarity.



**Figure 2.6** The calculated 3dB roll-off frequency using figure 2.4(d) and figure 2.5.

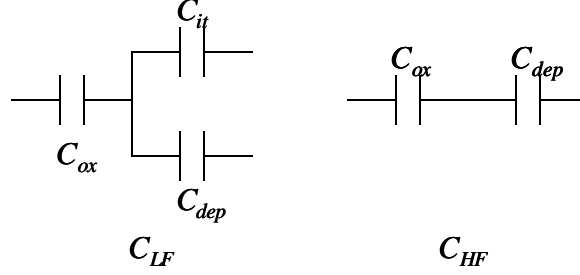
The experimental  $C_{ox}$  of 2.58 fF, taken from the strong accumulation region of the 20 kHz C-V, is within 7% of the calculated  $C_{ox}$  value, using the measured geometrical

dimensions ( $L=2.3\mu\text{m}$ ,  $D=75\text{nm}$ ),  $\gamma=7.3$  for  $\text{Al}_2\text{O}_3$ , and  $T_{ox} = 15 \text{ nm}$ . If we assume instead that the 15 nm oxide consists of 1 nm native  $\text{SiO}_2$  and 14 nm of  $\text{Al}_2\text{O}_3$  as would be expected according to a previous TEM study[15], then there is only a 1% deviation between the experiment and the calculation. The agreement also suggests that quantum confinement effect is comparatively unimportant, which is expected for a thick oxide layer. The roll-off frequency, defined as the reciprocal of the product of the measured resistance and capacitance, is shown in figure 2.6, and it is well above the measurement frequencies for the range of top gate voltages of interest (-1 to +1V). The measured changes in the C-V curves are therefore not artifacts of the access resistance.

## 2.4 The interface state density

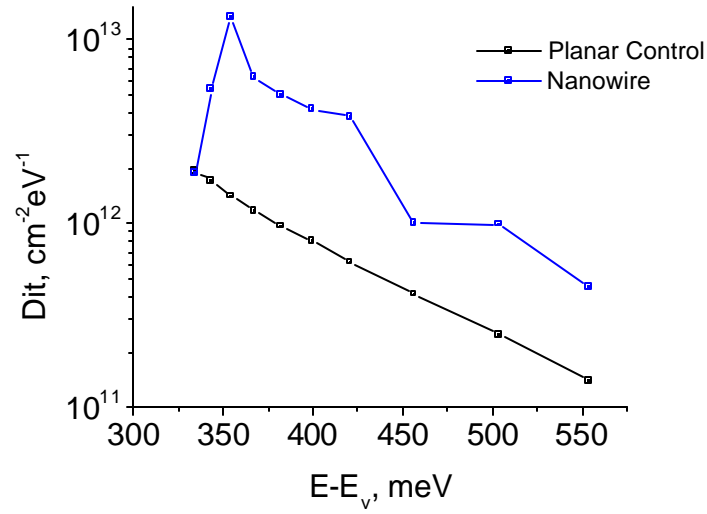
There is significant frequency dispersion in the C-V curves shown in figure 2.5. The dispersion is typically attributed to the finite lifetime of the interface trap states, which cannot respond quickly enough to high frequencies[10]. We can extract the interface state density ( $D_{it}$ ) as a function of position in the band gap by comparing the high and low frequency capacitance curves. Figure 2.7 shows the approximate circuit model in each case. At frequencies much slower than the trap lifetime, contribution from the traps are measured in addition to the depletion and oxide capacitance, whereas at high frequencies the traps effective “freeze out”, and do not contribute. A straightforward circuit analysis gives the following expression for  $D_{it}$ :

$$D_{it} = \frac{(C_{LF} - C_{HF})}{q \left(1 - \frac{C_{LF}}{C_{ox}}\right) \left(1 - \frac{C_{HF}}{C_{ox}}\right) 2prL} \quad \text{states / cm}^2 \text{ eV} \quad (2.1)$$



**Figure 2.7** Circuit model at high and low frequencies.  $C_{ox}$ : oxide capacitance.  $C_{dep}$ : capacitance from the depleted region.  $C_{it}$ : capacitance coming from the interface traps.

Figure 2.8 shows the resulting  $D_{it}$  versus the energy position relative to the valence band energy.  $D_{it}$  varies from  $4 \times 10^{11}/\text{eV} \cdot \text{cm}^2$  at mid-gap to  $1 \times 10^{13}/\text{eV} \cdot \text{cm}^2$  closer to the band edge. The trend matches well with the result from on a control MOSCAP fabricated on planar (111) silicon, following the same doping and oxide deposition steps. The mid-gap density is about an order of magnitude above a high quality thermal  $\text{SiO}_2$ -Si interface, but similar to both literature and planar control experiment results for  $\text{Al}_2\text{O}_3$  on silicon [18,19,20,21].



**Figure 2.8** The interface state density  $D_{it}$  versus position with respect to the valence band, extracted from the C-V curves in figure 2.5.

The shape of the  $D_{it}$  curve and peak position within several hundred meV of the valence band edge are also qualitatively similar to what has been observed in planar  $\text{Al}_2\text{O}_3$ -silicon interface [10, 17]. Compared to the planar control,  $D_{it}$  is somewhat larger. A possible cause is that the surfaces probed here are not the same as the planar control(111), due to faceting seen in figure 2.3. The faceted surfaces are thought to be (211), since this direction is  $30^\circ$  to the surface normal, as observed in figure 2.3. The observation of the (211) surface was also made previously[22].

Note that our results should be taken as the lower limit of the true  $D_{it}$ , since AH2700A is limited to operate between 50Hz and 20kHz, and it is not possible to access the true high and low frequency characteristics. The high-low method is well-known to underestimate the interface state density due to the difficulties in obtaining

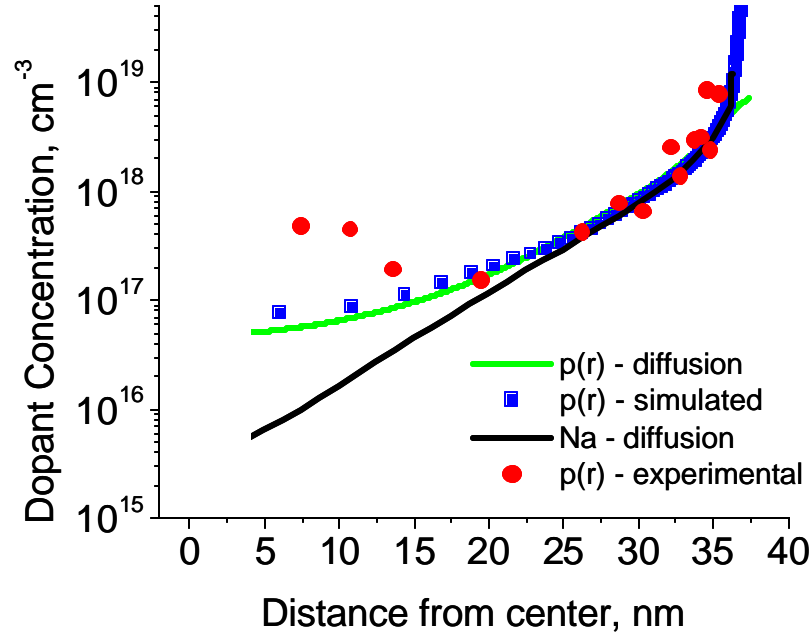


true high and low frequency behavior. However, from previous studies on planar silicon we expect a difference no more than a factor of two from the true profile[10, 23].

## 2.5 Dopant profile

We have also extracted the dopant profile using the high frequency C-V curve, using depletion approximation. The results are compared to the simulation from a commercial semiconductor process simulator, TSupreme, using the actual device dimensions and process conditions, including the interstitial- and vacancy-assisted diffusion models. In addition, we assume that the dopant concentration at the surface is fixed at the solid solubility ( $2 \times 10^{19}/\text{cm}^3$  at  $675^\circ\text{C}$ ). The depletion approximation is also verified using finite element electrostatic simulations (COMSOL Multiphysics), to include both the ionized dopants and the majority carriers. Figure 2.9 shows the agreement between the simulated diffusion profile and the experimental data. In addition, the FEM simulation shows that the profiles of the ionized dopant and the majority carrier match well, except at low doping levels near the core of the wire. It has been long noted that the C-V technique deduces the dopant concentration accurately only in regions where charge neutrality is exhibited [22,23]. Qualitatively, a gradient in the dopant density leads to a built-in electric field, which is screened out by a re-distribution of the majority carriers. The length scale of the re-distribution is simply the Debye screening length ( $L_d$ , equation 2.1), which at low density can be fairly long and is given by [24] :

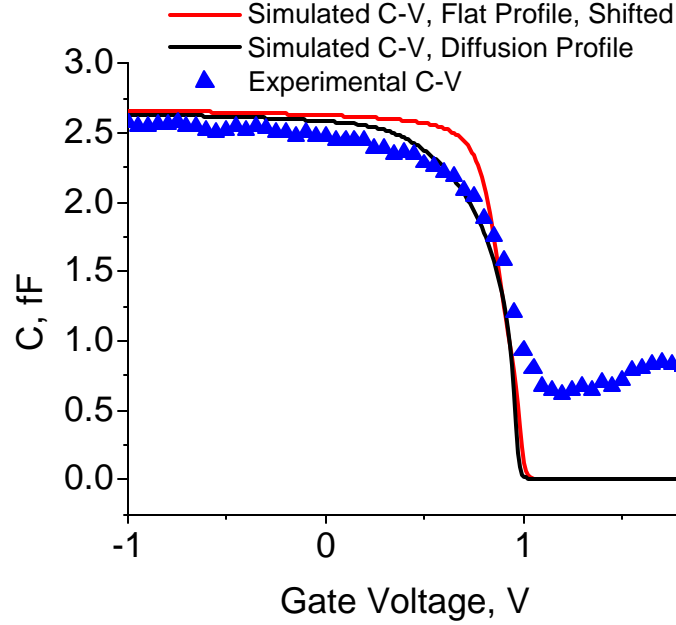
$$L_d = \sqrt{\frac{k\epsilon_0 k_B T}{q^2 N_A}} \quad (2.1)$$



**Figure 2.9** Radial charge and dopant profile extracted using the C-V measurement. The blue symbols are the majority carrier concentration extracted from a calculated C-V curve fitted to the measured high-frequency C-V curve. The black curve is the dopant profile simulated using TSupreme, using the process conditions. The green curve is the majority carrier concentration expected from the simulated dopant profile.

It has been well established that spatial resolution in C-V dopant profiling is limited to about  $2L_d$ , which at the measurement temperature of 77K should be about 2nm and 13 nm at the surface and core, respectively, due to the different doping levels[10]. Since the C-V method actually measures the free carriers and not the dopant atoms, the experimentally extracted majority carrier profile will only match the dopant profile in regions where the carrier redistribution has a minimal impact, typically around  $1 \times 10^{16} - 1 \times 10^{17} \text{ cm}^{-3}$  or higher[25,26]. Above these resolution limits, we can certainly differentiate between a graded and a uniform dopant distribution (figure 2.10). Using the same FEM 3-D simulations, we can compare the simulated and the experimental C-

V curves in order to determine the flat band voltage ( $V_{FB}$ ) and further validate our dopant profiling and  $D_{it}$  extraction techniques.



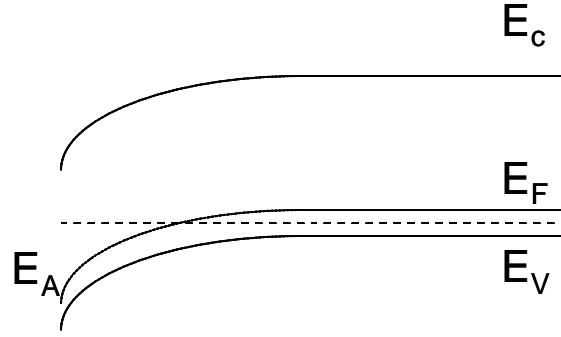
**Figure 2.10** Simulated C-V curves. Experimental high frequency 20 kHz C-V curve (blue) compared to the simulated C-V curves for the boron diffusion profile (black) and the flat profile (red) as shown in Figure 4a and 4b, respectively. Credit: D. Khanal.

Figure 2.10 shows the FEM simulated C-V curves calculated from the graded and the uniform profiles ( $N_a=10^{17}/\text{cm}^3$ ), and the high-frequency (20 kHz) experimental C-V curve. The simulated curves are shifted horizontally so they overlap one another, for the purpose of comparison. Without this shift,  $V_{FB}$  for the uniform profile would be about 0V. Clearly, the graded dopant profile leads to a C-V curve that matches the experimental C-V curve better than a uniform dopant profile.

The only major deviation comes at full depletion where the simulated capacitance reduces to 0fF, while the experimental curve does not go below 0.5fF. This extra capacitance in the experiment may come from direct coupling between the surround gate and the nanowire leads. The simulation does not account for this since it does not incorporate a back gate and thus allows for the leads (underlapped regions) to become depleted. Since the simulation did not account for interfacial defects, the minor deviation in slope likely stems from interface states, which are known to cause stretch-out even in high frequency C-V measurements[10].

In figure 2.10, it is necessary to shift the simulated C-V curve horizontally to match the measurement. Attributing this flat-band voltage shift to the built-in potential between the metal gate and the substrate and the contribution from fixed charges, we can extract a fixed oxide charge density of  $Q_f = -4.6 \times 10^{11} \text{ cm}^{-2}$ , when a literature value for chromium ( $\phi_M = 4.5\text{eV}$ ) is used. This value of  $Q_f$  is similar to previous literature reports for  $\text{Al}_2\text{O}_3$  deposited using ALD[16].

Lastly, it should be noted that although this experiment was conducted at 77K, dopant freeze-out need not to be considered. As illustrated in figure 2.11, dopants are still ionized in the depleted region because the impurity acceptor level  $E_A$  is pulled below the Fermi level, causing it to be filled, and the acceptor impurities to be fully ionized (figure 2.11). Thus, this technique can in principle be extended for even lower dopant densities, if the temperature is lowered further.



**Figure 2.11** Energy band diagram of a p-type semiconductor under freeze-out conditions. Dopants in the flat band (bulk) regions is assumed to be frozen out. Band bending causes the acceptor levels  $E_A$  (dotted) to be pulled below the Fermi level (dashed), causing the acceptor levels to be filled, and the dopant atoms ionized

## 2.6 Summary

The C-V measurement was used to determine all the relevant parameters of a silicon nanowire MOSCAP. Using frequency-dispersion measurement between 200 Hz and 20 kHz, it was demonstrated that the  $D_{it}$  profile as a function of energy position in the band gap is similar to results from bulk silicon. The radial boron dopant profile is also deduced and matches the expected profile from the dopant diffusion simulation with a surface concentration near the boron solid solubility of  $2 \times 10^{19} \text{ cm}^{-3}$ . This is in contrast to a flat dopant profile guessed from measured conductivity, mobility and threshold voltage in previous literature on Si NW transistors. These results unambiguously demonstrate that a quantitative understanding of the surface properties and dopant distribution within semiconductor nanowires will be critical to achieve reproducible high-performance devices.

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# Chapter 3

## Characterization of back-gated InAs nanowires

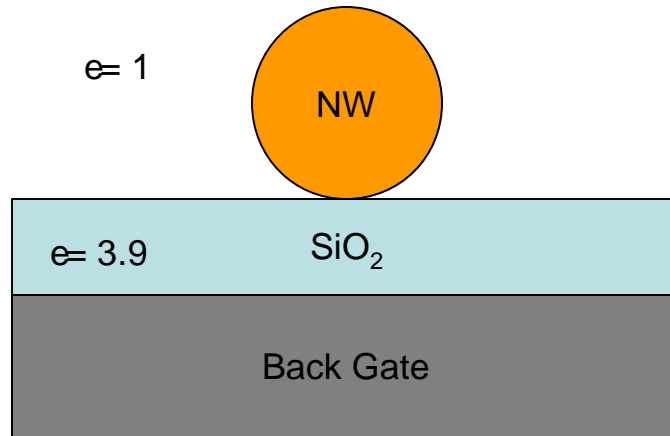
Transistors have been reducing in size ever since their introduction into integrated circuits. The international technology roadmap predicts that by the completion of this thesis, the gate length of a MOS transistor will be about 32nm. One of the reasons for transistor scaling is to improve switching performance. Even in the velocity-saturation regime, reducing the channel length of the transistor can still improve the drive current[1], as long as the transport is not completely ballistic.

It is well known that carrier mobility is much higher in III-V semiconductors compared to silicon. However, their usage as a channel material in a MOSFET structure is limited by the unavailability of a gate dielectric with sufficiently good



interface quality. Transistors based on bottom-up semiconductor materials such as nanowires of Si[2], Ge[3], InAs[4] or carbon nanotubes[5] are shown to have a carrier mobility generally much greater than transistors made in bulk silicon. However, most prior estimates of the mobility were based on rather simple calculation of the gate capacitance[1,2]. In these primitive devices, the channel is often back-gated because that geometry is easy to realize, and one can dispense with gate dielectrics that usually have a deleterious impact on the mobility, although a passivated surface is still necessary. As a result, the dielectric medium surrounding the channel (figure 3.1) is not uniform and the gate capacitance is somewhat difficult to model. A simple alternative is to measure the capacitance directly, and use this information to extract accurate mobility numbers.

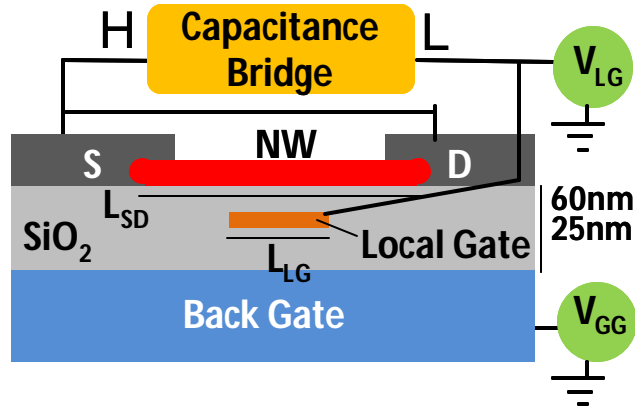
In this chapter the C-V technique is used to characterize individual InAs nanowire in its usual back-gated geometry, both to extract the oxide capacitance accurately, and to characterize the interface quality, in terms of usual parameters such as interface trap density and trap life time.



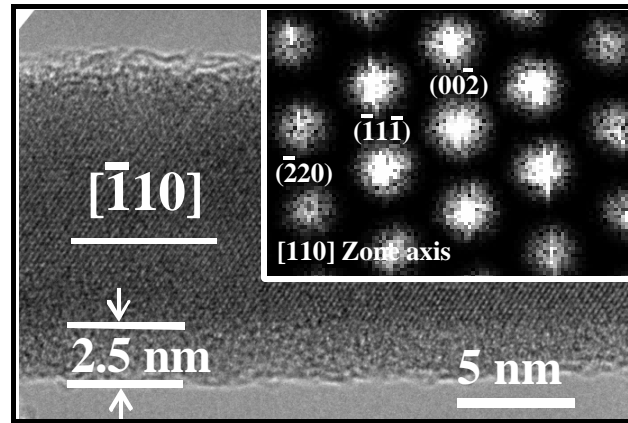
**Figure 3. 1** Cross-section of a commonly used geometry for nanowire devices. The back gate is used to modulate the conductivity of the nanowire channel.

### 3.1 The interface between the InAs nanowire and its native oxide

InAs is a small-bandgap and high mobility material. To characterize these InAs nanowires using the capacitance-voltage technique, we use the test structure illustrated in figure 3.2. It is very similar to the structure previously used in chapter 2, with the exception that both gates are buried, so that no mobility-degrading gate dielectric needs to be in contact with the nanowire. Instead, the InAs nanowire is surrounded by its native oxide, about 2.5nm thick as shown in figure 3.3.



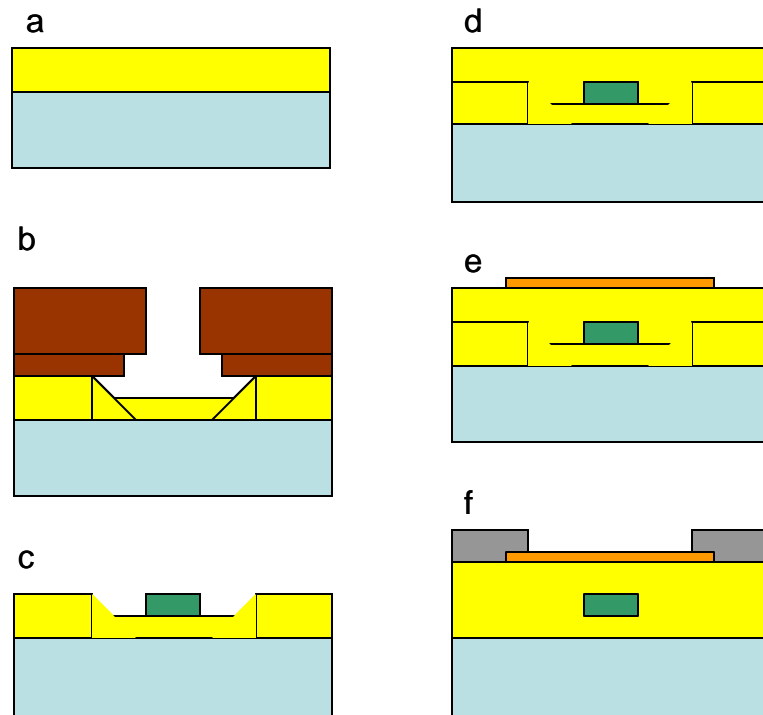
**Figure 3.2** Test structure for C-V measurement of InAs nanowires[6]. The underlapped region can be modulated by the back gate for extracting background capacitance. The capacitance is measured between the local gate and the source/drain.



**Figure 3.3** TEM image of an InAs nanowire, showing the crystallinity of the wire as well as the presence of a 2.5nm native oxide[5].

The InAs nanowires are grown using a solid-source CVD technique [3], using nickel nanoparticles as catalyst. The particles are formed directly on the growth substrate by thermally annealing a thin film (10nm~15nm) of nickel, deposited using thermal evaporation. The solid-source InAs, located in the same furnace tube but upstream from the growth substrate, is carried to the catalyst by hydrogen gas. The InAs source is in a powdered form and heated independently of the growth substrate.

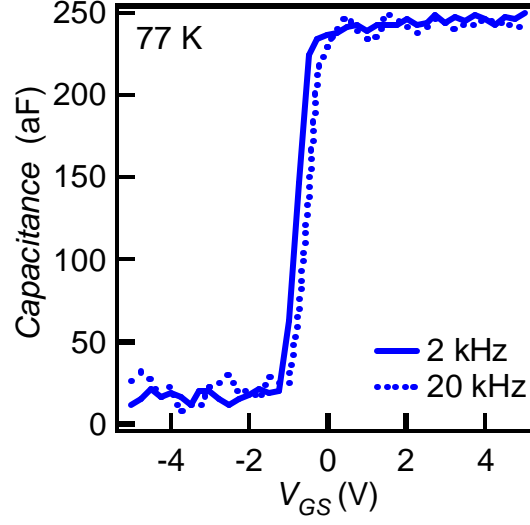
The test structure is fabricated following the process sequence illustrated in figure 3.4. Starting with a heavily doped p-type silicon wafer, a thick layer (200nm) of thermal oxide is grown (3.4a). The buried local gate is fabricated by partially etching away the thick oxide layer using buffered HF, in the area defined lithographically in a photoresist bilayer (3.4b). The drawn length of the gate varies from  $2\mu\text{m}$  to  $8\mu\text{m}$ . Metal (Pt) is then deposited and lifted off using the same photoresist bilayer. A thin (50nm) layer of CVD oxide is then deposited to insulate the buried local gate from the nanowire.



**Figure 3.4** Fabrication process sequence of the C-V test structure. a) Growth of thermal oxide (yellow). b) Definition of the buried electrode, by etching into the oxide using buffered HF. Pt (green) deposition and lift-off follows, resulting in (c). Lift-off is facilitated by the bilayer resist. d) Deposition of a 50nm silicon dioxide. e) Deposition of InAs nanowires from ethanol suspension onto the entire substrate. f) Definition of the nickel source and drain electrodes. Process designed by J.C.Ho.

The InAs nanowires are then desposited from a suspension in ethanol. The nanowire density is large enough such that about 5 to 10 devices with only a single nanowire can be found on each 1''x1'' chip. Lastly, nickel source and drain electrodes are defined using a second lift-off step. A brief (~30s) rapid thermal anneal follows to improve the contact resistance.

The method for accurate C-V measurement and background extraction follows the description in chapter 2. Figure 3.5 shows a typical C-V curve measured at 77K. At this temperature, the lifetime of the surface states is too long to respond to the applied signal frequency (1-20kHz). At a higher temperature, there is significant frequency dispersion in the C-V curves, as seen in figure 3.6. Above 200K, the lifetime of the traps is short enough to respond to even the highest frequency (20kHz) of the instrument. The capacitance from the traps completely dominates, such that the wire cannot be depleted and an accurate measurement of the background can not be done. Indeed, a recent report[7] shows that frequency as high as 20MHz is necessary at room temperature to stop the traps from responding.

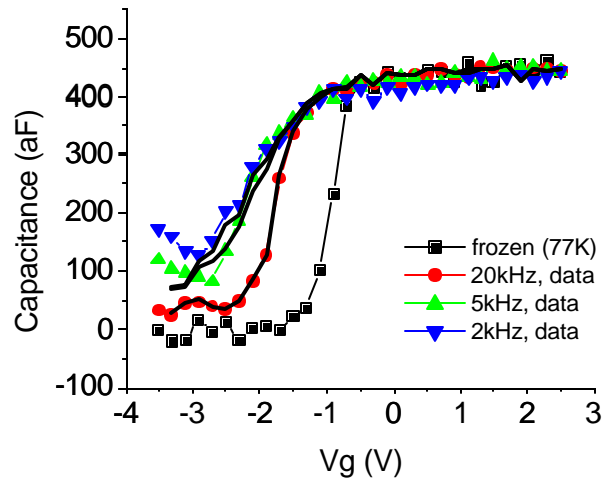


**Figure 3.5** Typical C-V curves at 77K for an InAs nanowire. There is a lack of frequency dispersion at such a low temperature.

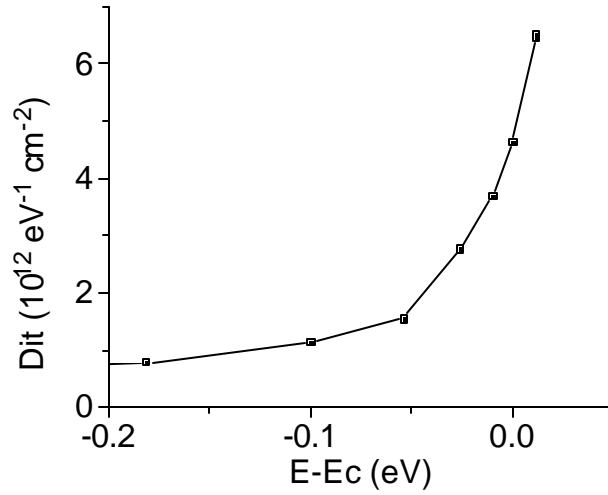
A single time constant model for the trap lifetime successfully reproduces the frequency-dispersion effect in figure 3.6. Based on this model, a surface trap density  $D_{it}$  of  $\sim 10^{11}$  to  $10^{12}/\text{eV cm}^2$  can be extracted from the C-V curves (figure 3.7). The capture cross-section  $s_p$  of the trap can also be estimated by using equation 3.1 [8]:

$$t = \frac{1}{v s_p n} \quad (3.1)$$

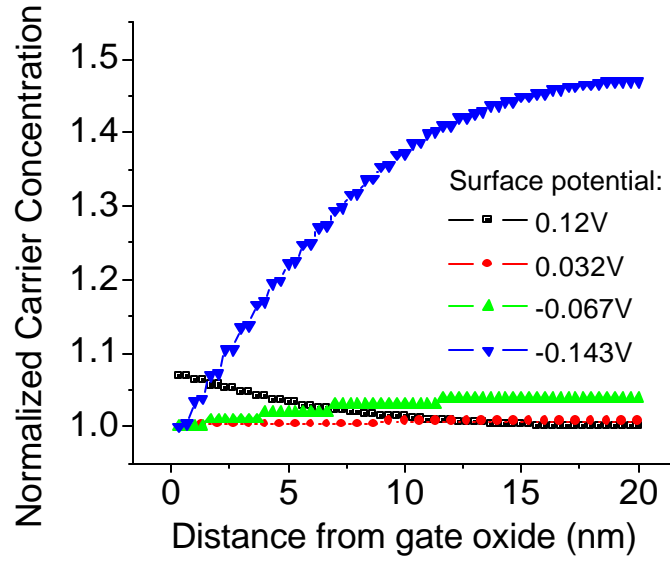
where  $t$ ,  $v$  and  $n$  are respectively the trap lifetime, thermal velocity and carrier density.  $n$  can be calculated using a commercial three-dimensional device simulator, Taurus 3D, and is remarkably uniform throughout the wire, despite the back-gate geometry (figure 3.8).



**Figure 3.6** C-V curves of an InAs nanowire measured at 200K. The “frozen” curve measured at 77K is assumed to be equivalent to the true high-frequency behavior, where all traps stop to respond.



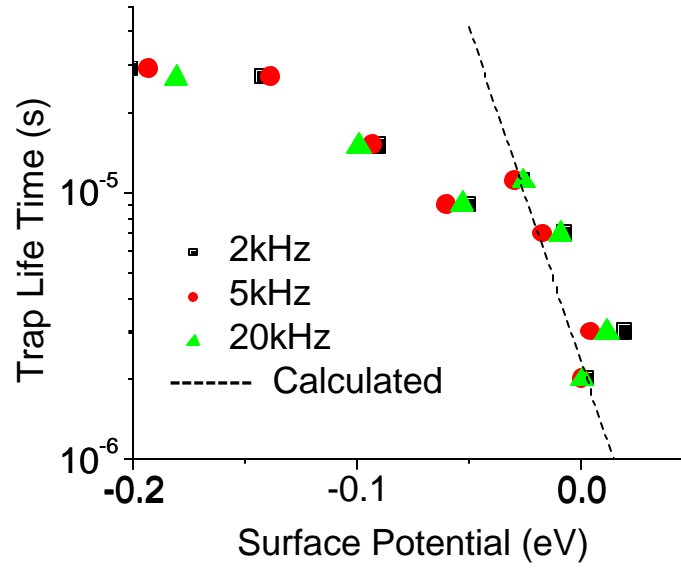
**Figure 3.7** Trap density  $D_{it}$  vs position in the band gap, deduced from single life time fit to figure 3.5.



**Figure 3.8** Normalized carrier density vs distance from gate oxide for several surface potentials. Since the carrier density varies exponentially with the surface potential, it is normalized to the smallest value along the profile for ease of comparison.

Figure 3.9 shows the trap lifetime deduced from the C-V curves, and its comparison to the expected values calculated from equation 3.1. There is a relatively good agreement for traps near the conduction band, when a capture cross-section of  $2 \times 10^{-15} \text{ cm}^2$  is used. This cross-section is significantly larger than traps at the Si-SiO<sub>2</sub> interface ( $\sim 3 \times 10^{-16} \text{ cm}^2$ )[7]. Literature search reveals no prior estimates of capture cross-section of traps at the interface of InAs and its native oxide. At a larger surface potential where the lifetime is relatively independent of the surface potential, other processes may cause the frequency dispersion seen in figure 3.9.



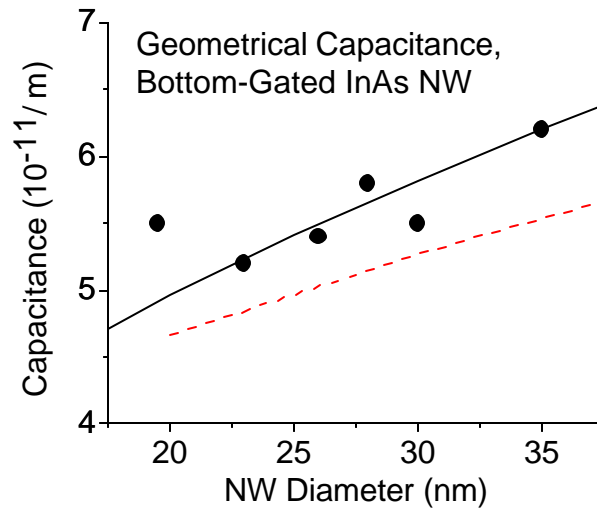


**Figure 3.9** Deduced trap lifetime compared to calculated values from equation 3.1. A capture cross section  $s_p = 2 \times 10^{-15} \text{ cm}^2$  is used.

### 3.2 Capacitance measurement for mobility extraction

InAs nanowires grown using solid-source CVD can have a diameter ranging from 20nm to 40nm[3]. The measured gate oxide capacitance of back-gated InAs nanowire transistors is shown in figure 3.10. Electrostatic simulation reproduces well but underestimates the capacitance slightly, probably due to an error in the oxide thickness measurement. The oxide at the edge of the buried gate can also be much thinner than expected due to non-conformal step coverage of the CVD process. More importantly, figure 3.10 shows that a simple analytical expression:

$$\frac{C_{ox}}{L} = \frac{2pe_r e_0}{\cosh^{-1}\left(\frac{T_{ox} + R_{NW}}{R_{NW}}\right)} \quad (3.2)$$



**Figure 3.10** Capacitance per unit length for InAs nanowires in a back-gated geometry. The solid line is a fit using equation 3.2, with  $\epsilon=1.77$ . The dotted line is the result of electrostatic simulation using a commercial tool (Maxwell). The measured oxide thickness is 50nm, which is also used in the simulations.

fits well only when the non-uniform dielectric medium is taken into account. This can be simply done by making the relative permittivity  $\epsilon_r$  a fitting parameter, which at 1.77 gives a reasonable fit. This is because the electric field lines go through air as well as the oxide. This result is similar to approximations used for striplines in microwave circuits [9].

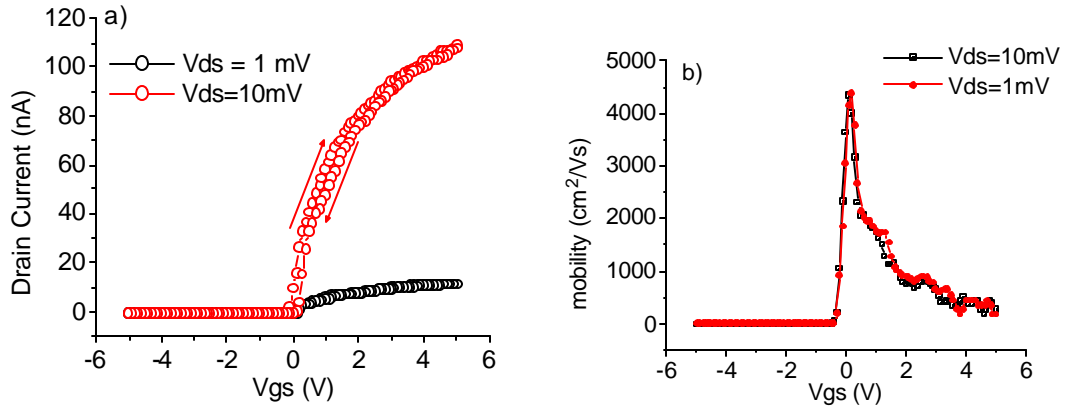
With the gate oxide capacitance accurately known, the low-field mobility can be confidently extracted, and is shown in figure 3.12. The low-field mobility is extracted from the transfer characteristics (figure 3.11) of long-channel devices ( $L_g > 2\mu\text{m}$ ) at small drain bias  $V_{ds}$ , and small values of  $V_{gs}-V_t$  such that the effects of velocity saturation and large vertical field can be ignored. More precisely, the  $I_d$ - $V_{gs}$  curve is differentiated vs  $V_{gs}$  to yield the conductance  $g_m$ , and the low-field mobility taken as the

peak value of the quantity  $g_m L/C_{ox}/V_{ds}$ . At large  $V_{gs}-V_t$ , the mobility is degraded by the vertical field, similar to what is observed in planar Si MOSFETs. At very low  $V_{gs}-V_t$  the device is still not well above the threshold to be modeled correctly by a simple square-law model (eqn 3.3). For long channel, the drain current and the conductance  $g_m$  are simply given by:

$$I_d = \mathbf{m} \frac{C_{ox}}{L} (V_{gs} - V_t - V_{ds}) V_{ds} \quad (3.3)$$

$$g_m = \frac{dI_d}{dV_{gs}} = \mathbf{m} \frac{C_{ox}}{L} V_{ds} \quad (3.4)$$

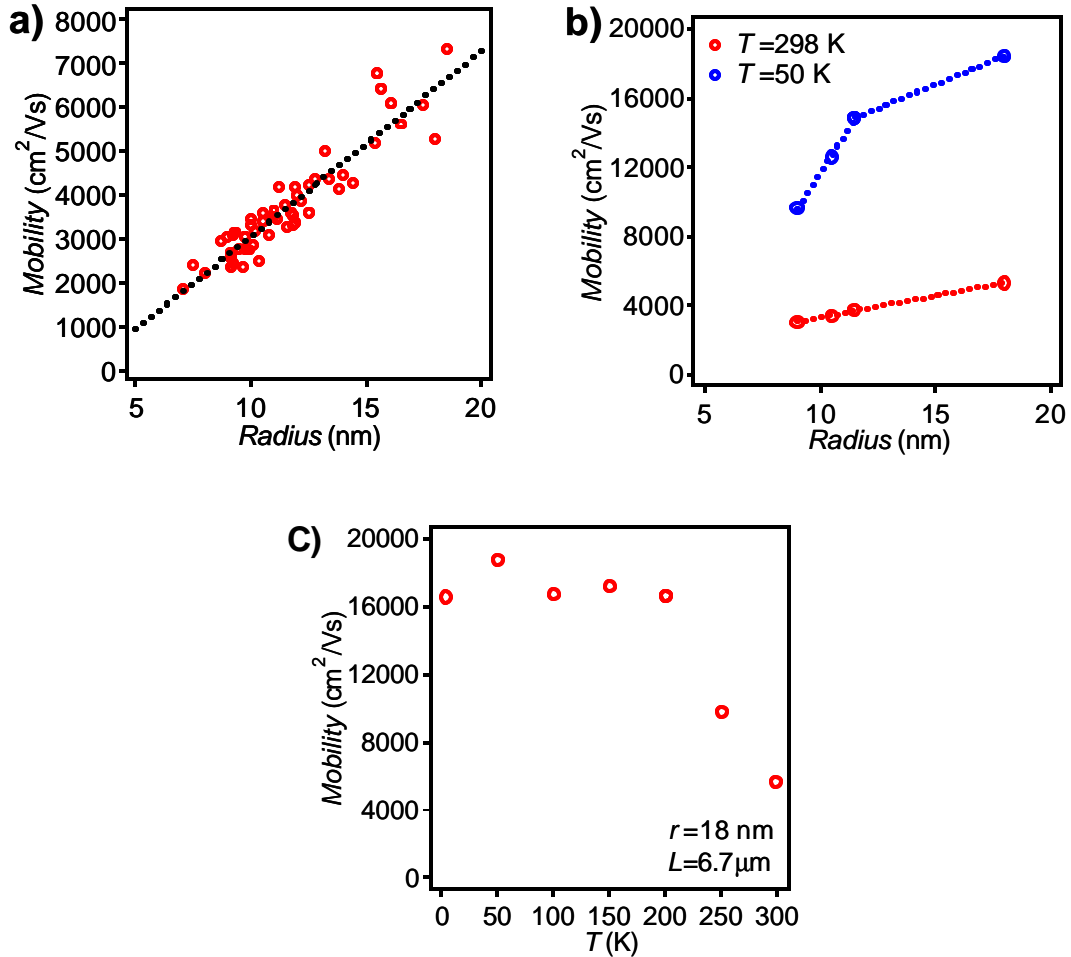
Since the device is one-dimensional, the oxide capacitance per nanowire,  $C_{ox}$ , is in the units of (F/m), as opposed to (F/m<sup>2</sup>) for a planar device. The diameter of the nanowire is measured using AFM and  $C_{ox}$  taken from the best analytical fit (figure 3.10) at that diameter.



**Figure 3.11** a) Transfer characteristics ( $I_d$ - $V_g$ ) and b) mobility of a InAs nanowire transistor

At sufficiently low temperatures, phonon scattering is suppressed, and there is an overall increase in mobility. In a universal mobility model, the surface scattering-

limited mobility does not depend on temperature[10], evident from figure 3.11c. Figure 3.11b indicates that mobility decreases more rapidly for nanowire radius below  $\sim 11\text{nm}$ . Since the Bohr radius in InAs, at  $34\text{nm}$ , is larger than the nanowire radius, quantum confinement can be important and may explain the stronger dependence of mobility on diameter in small wires, perhaps due to increased effective mass as demonstrated by recent theoretical calculations[ 11 ]. Quantum confinement can also modify the bandstructure such that the scattering rate is different from bulk, although this is speculative until a rigorous theoretical treatment is made.

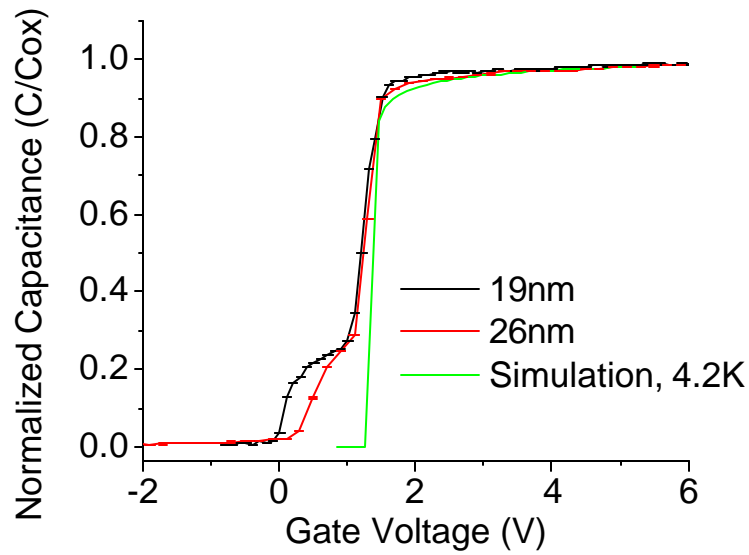


**Figure 3.12** a) Low-field electron mobility vs nanowire radius at room temperature. b) Mobility vs radius at room temperature and 50K. c) Mobility vs temperature for a large diameter wire. The lack of temperature dependence suggests that surface roughness scattering is the dominant scattering mechanism at low temperatures. From [5].

### 3.3 Summary and Future Work

In this chapter, low-level C-V measurement and analysis are used to deduce the relevant parameters that describe the surface states of a single InAs nanowire. In addition, it is shown that a simple analytical expression predicts well the geometrical gate oxide capacitance, provided that the non-homogeneous dielectric medium is accounted for. The accurate measurement of the oxide capacitance allows for an accurate determination of the carrier mobility in InAs nanowires. When phonon scattering is suppressed at low temperatures, the dominant mechanism for small-diameter nanowires seems to be surface scattering.

There are other properties of InAs nanowires that can be probed using this technique, one of which is the quantization effect arising from the small diameter. Ilani *et al* used the same technique to probe the density of states in a single carbon nanotube[12]. Figure 3.12 shows much more precise C-V measurements of two small InAs nanowires at liquid helium temperature, and the comparison to simulation. There are small but interesting features that cannot be reproduced by a straightforward electrostatic simulation employing bulk density of states.



**Figure 3.13** Measured C-V curves of two small diameter InAs nanowires at 4K. The measurement frequency is 100kHz. Simulation: diameter=20nm

At the temperature of liquid helium, the traps should have ceased to respond, as implied from the results at liquid nitrogen temperature (figure 3.5). Since the nanowire is undoped, the observed features in the C-V curves cannot be caused by ionized dopants either. The most plausible explanation is that there is a transition of the density of state in the nanowire from bulk-like to that of a one-dimensional quantum wire. At this moment, there is no known method to make much thinner InAs nanowires without increasing significantly the surface roughness. Should a solution be found, the one-dimensional band structure of an individual InAs nanowire can be directly probed using this method.

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# Chapter 4

## Metal-Carbon Nanotube Schottky Contacts

The metal-semiconductor (MS) contact is ubiquitous in semiconductor devices. By itself, a Schottky MS contact, with low substrate doping and large barrier height, can be used as a high-speed rectifier. In other devices such as MOSFETs and BJTs, the MS contact is absolutely necessary for their integration into circuits. These contacts need to have a low specific resistance in order for the devices to function properly. This is usually achieved by doping the contact region heavily to allow tunneling through a thinned Schottky barrier. In the current Si-based MOS technology, the MS contact is a major contributor to serial, parasitic resistances that degrade transistor performance. As



the dimensions of MOS transistors diminish further, the resistance of the MS contact can become much more detrimental, since the source/drain junction will need to become even more shallow and abrupt to combat short-channel effects, and the dopant concentration in the source and drain can not go higher, being already limited by the dopants' solid solubility.

Similarly, in transistors made from high-mobility materials such as carbon nanotubes, the Schottky barrier (SB) at the source and drain contacts can severely degrade the device performance, to the point that they completely determine the behavior of the device[1,2,3]. CNT transistors with negligible Schottky barrier height (SBH) and with minimal series resistance can be realized[4], and have a performance that surpasses their silicon-based counterpart. However, there is a limited choice of metal that can achieve this, such as Pd[4] and Rh[7], and a nanotube with large diameter is invariably needed[4,5,7].

The SBH between a CNT and its metal contact depends on several material parameters, such as the metal contact work function[5], the environment to which the device is exposed[6], and the diameter of the nanotube[7]. Given the many possible sources of variation, it is desirable to study a large set of devices to obtain statistically meaningful results on how each parameter impacts upon the device characteristics. The electrical characteristics of several hundreds of CNT transistors are examined in this chapter. Analysis of this data shows the influence of the nanotube diameter and the contact metal on the operating characteristics of a CNT transistor. By examining the

variation of on- and off-state currents vs the diameter, conclusions can also be drawn, surprisingly, about the geometry of the MS junction for a nanotube.

#### **4.1 Prior work**

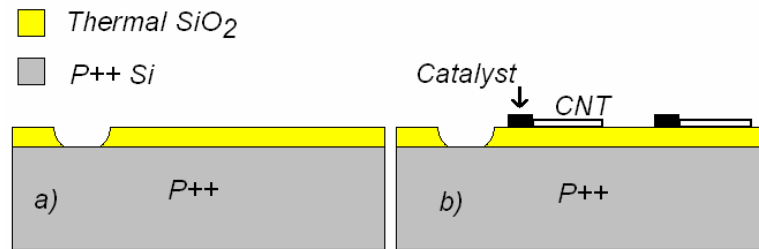
There is a rich literature on Fermi-level pinning in bulk semiconductors, after research in excess of 60 years[8,9,10]. Schottky proposed in 1938 that a potential barrier occurs naturally at a metal-semiconductor junction due to workfunction mismatch between the two materials. Contrary to the ideal Schottky model, experimental evidence shows that the SBH does not vary much with the metal workfunction[ 11]. This is because of the presence of electronic states inside the bandgap that effectively pins the Fermi-level at a fixed position. In a typical bulk semiconductor, the density of these states are sufficiently large that only a small fraction needs to be populated to compensate for the charge induced by the metal-semiconductor contact potential.

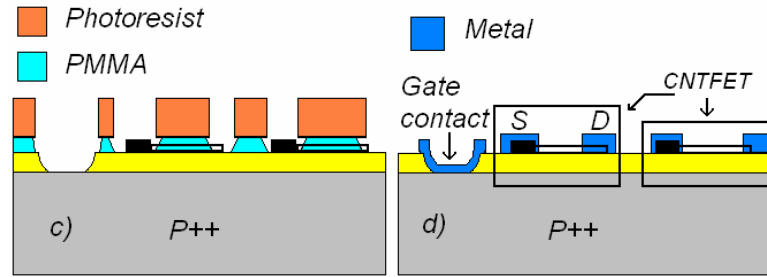
For contacts to one-dimensional semiconductors, an early theoretical study[ 12] predicted that Fermi-level pinning is of negligible consequence to the contact resistance, and that the junction is effectively unpinned. A few studies indicated that these theoretical predictions seem to hold true. Both Chen[5] and Kim[7] showed that the on-state current of a CNT transistor depends on the CNT diameter, and attributed the variation in the on-state current to a diameter-dependent Schottky barrier height at the contact. However, Chen *et al*[5] did not actually measure the diameter of each

individual nanotube, and Kim *et al*[7] estimated the SBH using a diameter-bandgap relationship of  $E_g = 1.1\text{eV}/d(\text{nm})$ , which does not agree with most other calculations[13,14,15] or experiments[16,17,19]. Neither of these works dealt with off-state leakage, or correlated the actual barrier height with the measured nanotube diameter. In this chapter, the effects of diameter variation will be examined more precisely.

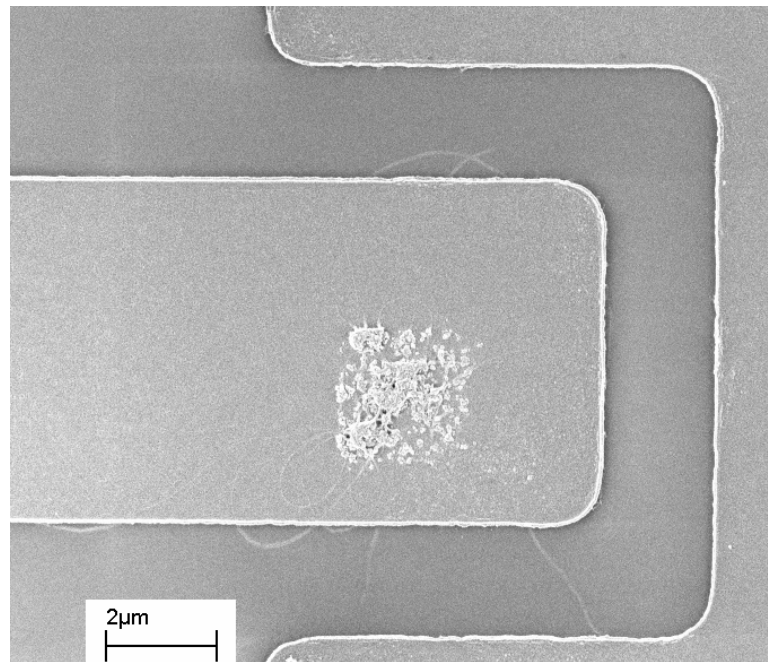
## 4.2 Array design, fabrication and testing

A large array of carbon nanotube transistors was fabricated using conventional microfabrication techniques illustrated in figure 4.1. Starting from a highly doped silicon substrate, a 160nm-thick silicon dioxide layer was grown under dry conditions. The contact to the substrate was defined, followed by the growth of carbon nanotubes on lithographically defined catalyst islands using previously reported processes[18]. Source and drain contacts were patterned using optical lithography for all nanotube devices simultaneously, in a bilayer lift-off stack. Metal contacts are then deposited using e-beam evaporation, followed by lift-off in acetone.





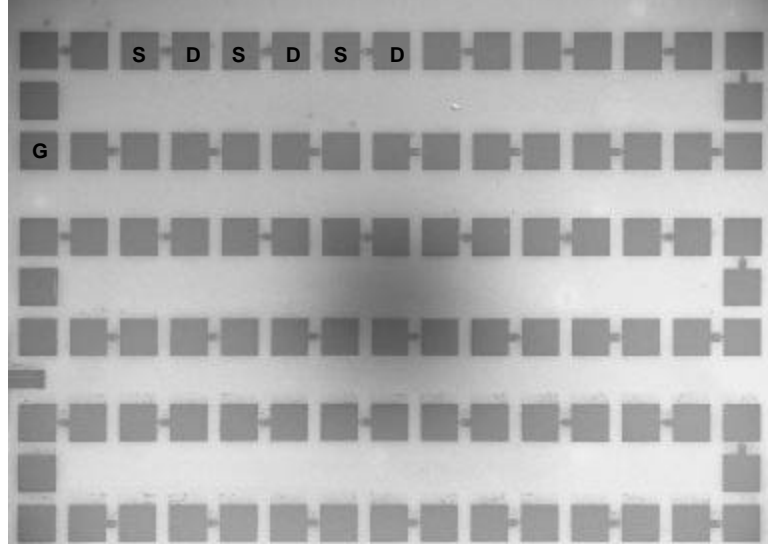
**Figure 4.1** Process steps for making a large number of CNT devices for automated measurement. a) Contact to substrate. b) Growth of nanotubes. c) Bilayer of lift-off stack, photoresist on top of PMMA, the latter of which is selectively dissolved in chlorobenzene. d) Deposition and lift-off of metal contacts.



**Figure 4.2** Scanning electron micrograph of an actual device. 896 such devices are packed into an  $1\text{cm}^2$  chip.

The gate length, set by the gap between source and drain, is  $2\text{ }\mu\text{m}$ . Figure 4.2 shows the top view of a device. Since the CNTs do not align in any particular direction during growth, the source and drain electrodes are designed to increase the probability of a CNT bridging the contacts.

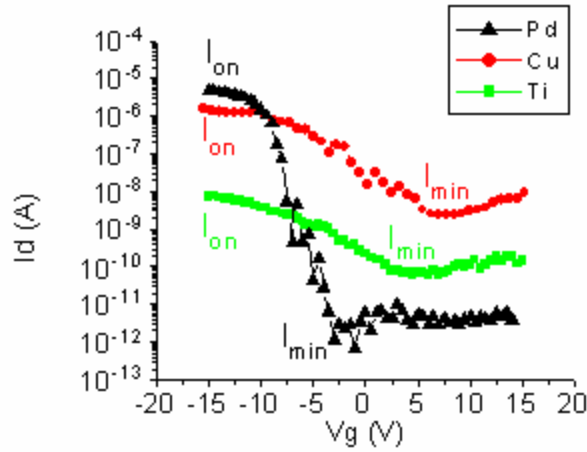
Since measuring a large number of devices manually would be intractable, automated measurement is necessary. Shown in figure 4.3 is the array designed for measurement using the Electroglas 2001X automatic prober. 896 devices are packed into a single  $\text{cm}^2$  chip, and the entire measurement requires approximately 3 hours. Since there is no control over the chirality and the number of nanotubes in each device, we can only sort the devices after the measurement, based on the I-V data. From the transfer characteristics of each device, those with metallic tubes (low on/off ratio) are found, and eliminated from consideration. Devices that remain are inspected individually using SEM, and only those with a single tube bridging the contacts are to be analyzed. The diameter of the nanotube is measured using tapping mode atomic force microscopy (AFM, Digital Instruments 3100), and is taken as the height of the nanotube relative to the substrate, averaged over a length of several hundred nanometers. The one-sigma uncertainty in each measurement is estimated to be 0.2nm and corresponds well to the RMS roughness of the oxide substrate itself, indicating that the precision of the measurement is probably limited by the substrate roughness.



**Figure 4.3** Array design for automatic probing. S: Source, D: Drain, G: gate. Shown here are 3 groups of devices. Each group has 14 devices, and there are 64 groups on each 1cm x 1cm die.

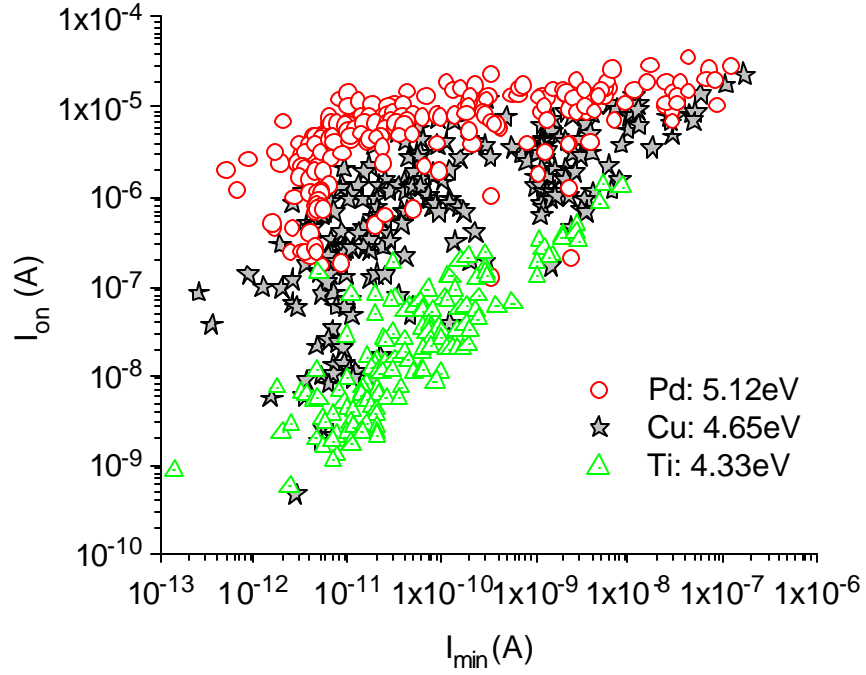
### 4.3 Statistical results

Two parameters from the transfer characteristics of each device are extracted. As shown in figure 4.4, we define the on-state current  $I_{on}$  as the current at  $V_g = -15V$ , and  $I_{min}$  as the minimum current reached in the entire range of  $V_g$  (-15V to +15V). We also define  $I_{min}$  as the ‘off-state’ current. This differs from the usual definition in device applications, where the off-state is at  $V_g=0$ . However, it is necessary for comparison between the devices used presently, since the threshold voltage of each device is not well controlled.



**Figure 4.4** Examples of  $I_d$ - $V_g$  characteristics for devices with different contact metal.  $I_{on}$  is the current at  $V_g = -15$  V.  $I_{min}$  is the minimum point in the sweep. Diameter for all devices: 1.7 nm.

By plotting  $I_{on}$  vs  $I_{min}$  (figure 4.5), for three different metal contacts, the following is revealed: For devices with Pd contacts,  $I_{min}$  is distributed across a wider range (variation of  $10^4$ ) than  $I_{on}$  (variation of  $10^2$ ), whereas Cu and Ti contacts lead to a 4-order of magnitude of variation in both  $I_{on}$  and  $I_{min}$ . It is also clear that, in general, devices having a large  $I_{on}$  also have a large  $I_{min}$ , so a high-performance device would also have the drawback of large off-state leakage. A plot such as figure 4.5 also provides a convenient way of comparing the merit between contact schemes.



**Figure 4.5**  $I_{on}$  vs  $I_{min}$  for the three sets of devices. All devices have the ratio  $I_{on}/I_{min}$  greater than 100. Pd: 209 devices. Cu: 232 devices. Ti: 138 devices. Devices having  $I_{on}/I_{min} >$  may contain at least one metallic tube. Workfunction of Pd: 5.12eV, Cu: 4.65eV, Ti: 4.33eV.

The variation in  $I_{on}$  and  $I_{min}$  observed among these devices is due in great part to the diameter of the nanotube. This is shown in figure 4.6, for three different contact metals. The relevant barrier heights for conduction in the on- and off-state decrease with the bandgap, leading to larger currents. A variety of experiments showed that the diameter  $d$  is related to bandgap  $E_g$  approximately as:

$$E_g = \frac{k_o}{d} \quad (4.1)$$

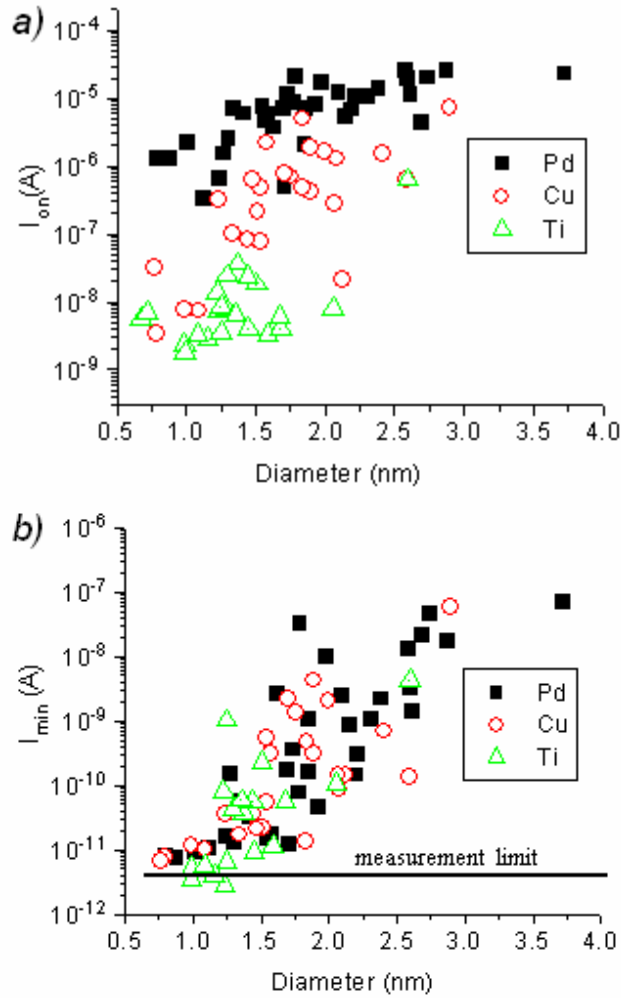
where  $E_g$  is in eV and  $d$  in nm, and  $k_o$  a number between 0.7 and 0.8 eV-nm. Kim [7] observed a strong dependence of the on-current with diameter as well, and suggested



that  $k_o$  is 1.1 eV-nm, significantly larger than other experiments. Tight-binding calculations [28] predict that:

$$E_g = \frac{2a_{cc}g_o}{d}$$

where  $a_{cc}=0.144\text{nm}$  and  $g_o$  are respectively the distance and the interaction energy between the two nearest carbon atoms. DFT calculations [15] give  $g_o=2.6\text{eV}$ , while a resonant Raman scattering experiment [17] employs  $g_o=2.9\text{eV}$  to unambiguously predict the resonant energy, and the associated chiralities of many nanotubes. Independent results by Wildoer and Odom [16] from scanning tunneling spectroscopy show that  $E_g \sim 0.7/d$ , which gives  $g_o=2.5\text{eV}$ . Bosnick *et al* [19] deduced from the I-V measurement of a few p-i-n CNT diodes that  $E_g \sim 0.8/d$ , leading to  $g_o=2.85\text{eV}$ . These experimental results differ considerably from the suggestion by Kim [7] that  $E_g=1.1/d$ , ( $g_o=3.8\text{eV}$ ) which in his case only served to conveniently explain a rapid drop-off in the on-current for diameters below 1.5nm. It will be shown in section 5.4 that the precise relationship between SBH and diameter (bandgap) has implications on the actual geometry of the electrical junction.



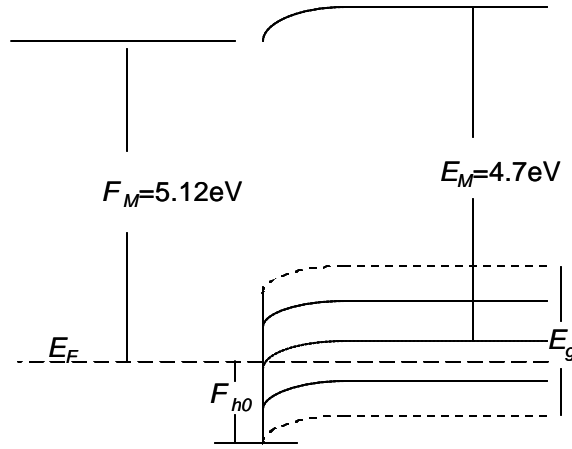
**Figure 4.6** Dependence of the on- and off-state currents on the nanotube diameter. a) on-state current vs diameter. b) off-state current vs diameter for the same set of devices.

The work function of Pd is expected to align closely to, or even below the valence band of a CNT. For large diameter tubes, the SBH is small or even negative, such that it does not limit the on-state current as much as the channel resistance. The resistance in the channel depends on carrier mobility, which does not vary by orders of magnitude on the CNT's length or diameter. The off-state current, on the other hand, is limited by thermionic emission over the drain barrier, and is extremely sensitive to the barrier height. Devices with Cu and Ti contacts will always have a large Schottky

Barrier in the range of diameters considered here, leading both  $I_{on}$  and  $I_{min}$  to vary across a wide range. The ideal Schottky model (figure 4.7) gives an expression for the SBH

$F_{h0}$  :

$$F_{h0} = E_g / 2 + E_M (eV) - \Phi_M \quad (4.2)$$



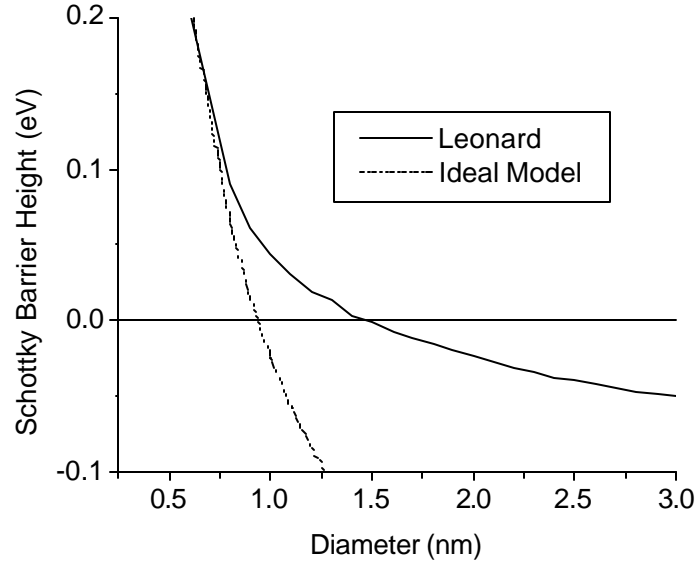
**Figure 4.7** Energy level alignment in an ideal Schottky model.  $F_M$ = metal work function.  $E_M$ =Mid-gap energy of the nanotube, relative to vacuum.  $F_{h0}$ =SBH for holes.  $E_F$ =Fermi level.  $E_g$ =bandgap. Short dashes: Change in the bandgap as a result of diameter variation. The numbers used are typical for Pd and CNT.

, where  $E_M$  (between 4.7eV and 4.8 eV[20,21]) is the mid-gap energy of the CNT relative to the vacuum, and  $F_M=5.12\text{eV}$  is the metal workfunction for Pd[22]. These numbers imply that  $F_B$  falls to zero at a diameter between 1nm and 1.3nm. Device modeling in the next section shows that while qualitatively correct, this model underestimates the diameter required for a zero barrier height, and has implications for the actual contact geometry.

#### 4.4 The geometry of the Pd-CNT contact

Ignoring Fermi-level pinning, the SBH of the metal-CNT contact should be given by equation 4.2, and devices with a nanotube diameter greater than 1~1.3nm should have no Schottky barrier at the contacts. However, experimental data [7] do not support that prediction. Instead, a more refined calculation of the SBH by Leonard [23], using a side-contact geometry, where the effects of charge transfer across a metal-semiconductor contact with concentric geometry are considered, show that the SBH for a Pd-CNT contact should fall to zero at around 1.5nm, instead of 1nm from as predicted by equation 4.2 (figure 4.8).  $\Phi_h$  does not follow equation 4.2 but is well approximated by equation 4.3[23]:

$$\Phi_h = \frac{kT}{b} \ln \left( \frac{a \sqrt{\frac{Eg}{2kT}}}{\ln \left( a \sqrt{\frac{Eg}{2kT}} \right) - \frac{\Phi_{h0}}{kT}} \right) \quad (4.3)$$



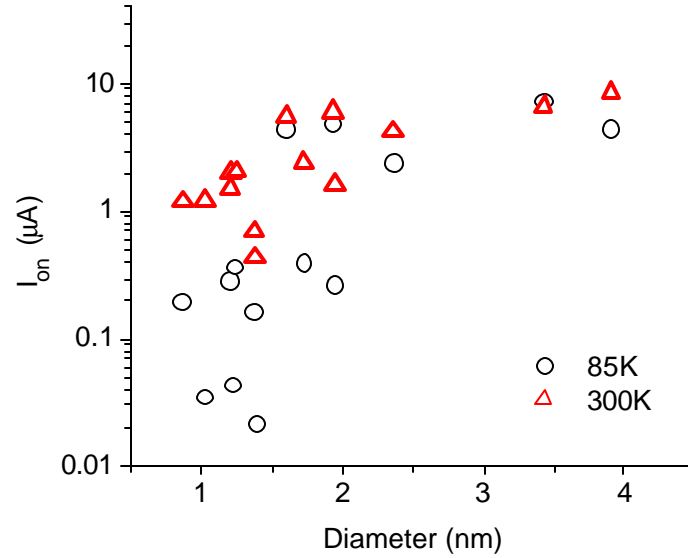
**Figure 4.8** Calculated SBH using the ideal model (equation 4.2), and Leonard's model[23]. The metal workfunction is such that  $F_M - E_M = 0.38 \text{ eV}$ .

, with  $\phi_{h0}$  given by equation 4.2,  $\beta = 0.7$  and  $a = 4.58 \times 10^{-11} / (R * \ln((R+s)/R))$ ,  $R$  = CNT radius,  $s$  = distance between metal and CNT  $\sim 3 \text{ \AA}$ . It can be shown that  $\phi_h$  in equation 4.3 is relatively insensitive to  $s$ .

A temperature-dependent transport measurement can show the presence of a significant Schottky barrier. Figure 4.9 shows that the on-state current in Pd-contacted devices drops sharply upon cooling for all diameters less than 1.5-2 nm, indicating that a Schottky barrier starts to develop, in agreement with theoretical predictions[23].

It would be desirable to measure directly the SBH. However, short of a method to directly measure the SBH of Pd-CNT contacts, it can only be extracted by fitting the I-V data to a device model[5]. For the large devices analyzed here, a compact model is

suitable because of its speed and simplicity. First-principle models based on non-equilibrium green's function (NEGF)[24] would be too expensive computationally because they require specifying the potential energy to atomic dimensions, much too fine compared to the device dimensions here.

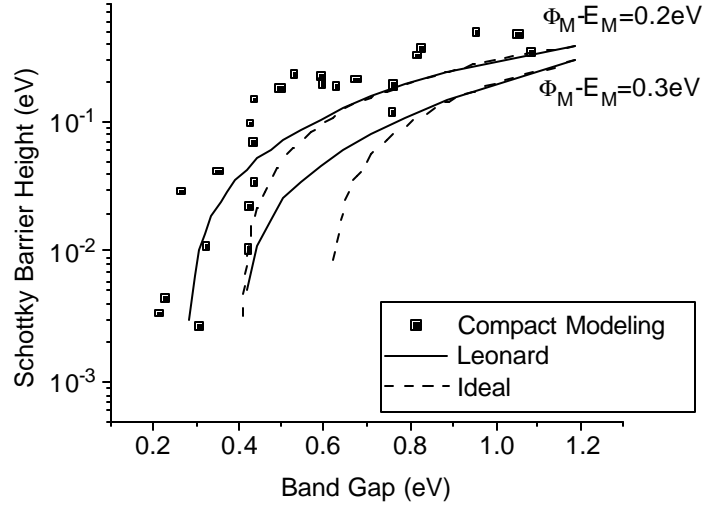


**Figure 4.9** On-state current vs diameter at two temperatures. A sharp drop is observed for all devices with diameters  $< 2$ nm. The uncertainty in the diameter measurement is about 0.5nm

The details of the compact model can be found elsewhere[25, 26]. Briefly, it calculates the charge in the nanotube by solving Poisson's and Schroedinger's equations self-consistently, using the measured device dimensions (length, oxide thickness and CNT diameter). The current is then calculated, taking into account thermionic emission over and tunneling through the Schottky barrier at each contact, and the effects of both acoustic and optical phonon scattering in the channel, via a mobility-vs-length model[27]. The SBH, series resistance  $R_s$  and the source-channel coupling capacitance  $C_d$  are adjusted iteratively such that a best fit to the  $I_d$ - $V_g$  characteristics is obtained for

each device.  $C_d$  captures the drain electrode's effect on the potential in the bulk of the channel, and is similar to DIBL in planar MOSFETs. The results of the compact modeling are relatively insensitive to  $C_d$  and  $R_s$ , but very sensitive to the SBH, and the mobility [25].

Figure 4.10 shows the SBH extracted from 25 devices using compact modeling. Although there is significant scatter, the results of compact modeling agree with the side-contact model (equation 4.3) [23] better than the predictions from equation 4.2, when the same contact potential  $F_M - E_M$  is used. Although the calculation from equation 4.2 agrees with compact modeling when  $F_M - E_M = 0.2\text{eV}$ , this would imply that the Pd workfunction is unexpectedly low, around 4.9 to 5.0eV. A better fit may result if the actual bandgap of each device is slightly larger than  $E_g = 0.7/d$  assumed in the modeling. Taken with figure 4.9, these results strongly suggest that Leonard's model [23], which accounts for the overlap region between the metal and nanotube, is a much better description of the geometry of the electrical junction. Indeed, recent 4-probe measurements concluded that electrical current does flow under the metal contacts[28,29], over a distance of several tens of nanometers.



**Figure 4.10** Schottky Barrier Height extracted using compact modeling compared to calculations from Leonard's model [23] (equation 4.3, solid lines) and the ideal Schottky model (equation 4.2, dashed lines). The calculations are done for two metal workfunctions  $F_M$  (relative to  $E_M$ , the mid-gap energy of the CNT).

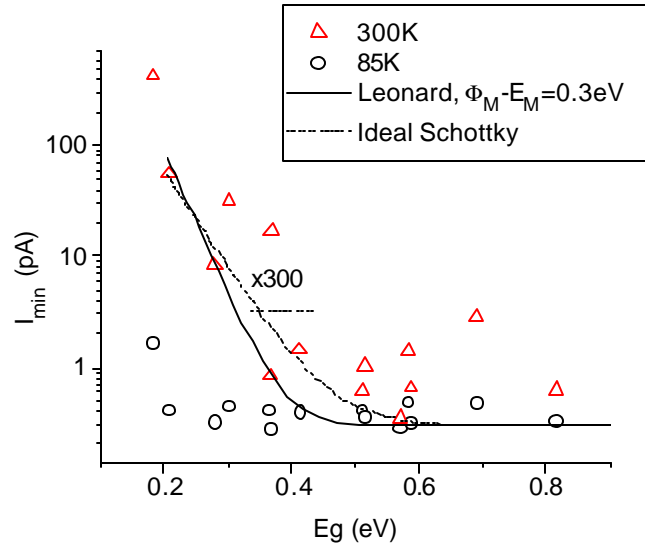
Yet another evidence supporting the side-contact geometry can be deduced by plotting  $I_{min}$  vs  $E_g$ . A simple formula for calculating  $I_{min}$  considering only the contribution from thermionic emission is equation 4.4:

$$I_{min} = AT^2 \exp(-qF_e/kT) + BT^2 \exp(-qF_h/kT), \quad (4.4)$$

The two terms of equation 4.4 are the contributions from electrons and holes. When the current is at the minimum, the contribution from each term should be almost equal. The prefactor  $A$  is a product of the Richardson's constant and the junction area.  $A$  and  $B$  should be the same for electrons and holes because the effective mass is the same. As a result  $I_{min}$  should be well approximated by:

$$I_{min} = 2AT^2 \exp(-qF_h/kT), \quad (4.5)$$



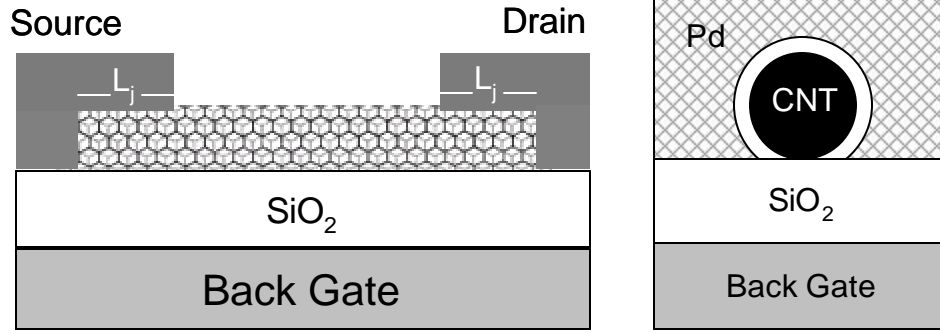


**Figure 4.11**  $I_{min}$  vs band gap  $E_g$ .  $L_j$  =length of the contact.  $L_j=25\text{nm}$  is used to produce a good numerical fit.  $I_{min}$  from the ideal Schottky model (equation 4.2) is some 300x smaller than the data. The effective mass of the nanotube,  $m_h^*=m_e^*=0.1m_0/d(\text{nm})$  [30], is used in calculating Richardson's constant. A constant leakage current of 0.3pA is added to account for the background leakage in the semiconductor analyzer.

For each diameter (bandgap), SBH is calculated from equation 4.3.  $I_{min}$  calculated using these SBH values fits well with data (figure 4.11), if one assumes that the current flows under the contact metal over a length  $L_j$  of 25nm, illustrated in figure 4.12. However, if the SBH is calculated from equation 4.2,  $I_{min}$  is some 300 times smaller than the observed data (figure 4.11), when the same  $L_j=25\text{nm}$  is used. The length  $L_j=25\text{nm}$  agrees with the 25nm predicted by ab-initio simulation of Nemec *et al*[31], and consistent with conclusions from 4-probe measurements[28,29].

The strong temperature dependence of  $I_{min}$  shown in figure 4.11 justifies using equation 4.4 alone for  $I_{min}$ , and one needs not to include contributions from tunneling. Electrostatic calculations by Guo[32] show that the extent of the depletion region is in

the order of the gate oxide thickness, which is 160nm in this case. This distance is much too large for tunneling current to be significant.

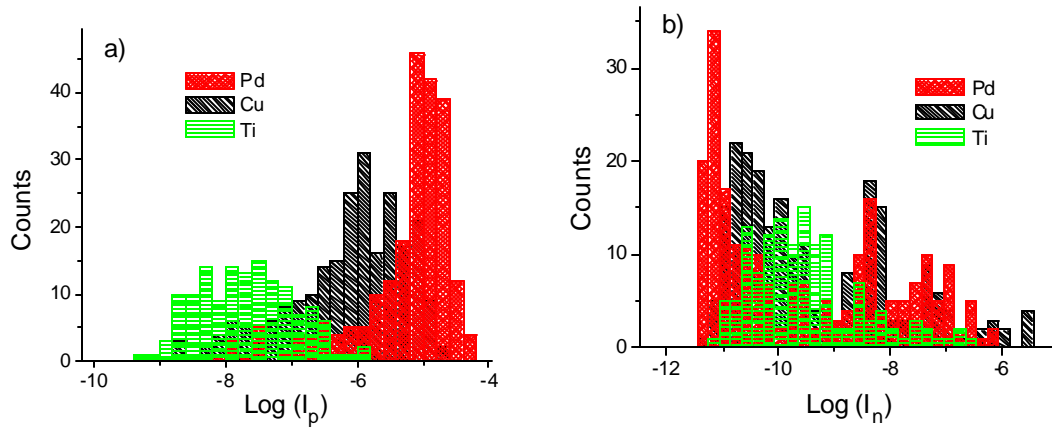


**Figure 4.12** Definition of  $L_j$ . In calculating  $I_{min}$ , current is assumed to flow from the metal contact into the nanotube over the distance  $L_j$ , leading to a contact area of  $2pRL_j$ .

Although we assumed that all nanotubes are single-walled, there is a possibility that the large-diameter nanotubes may be double-walled, or even multi-walled. Assuming that all shells are semiconducting, the leakage current through the outer, larger diameter shells should dominate. If a DWNT has an inner shell of 1.5nm, then the outer shell has a diameter of 2.18nm, using an intershell distance of 0.34nm[33]. Using our simplistic model for leakage current, the outer shell would conduct 28 times more current in the off-state than the inner shell. In addition, the coupling of the metal to the inner shell is generally weaker. The leakage current of the devices in figure 4.11 is also much lower than what would be expected from a metallic nanotube ( $\sim 10\mu A$ ). As such, if the nanotubes in question have multiple walls, they have either no metallic shell, or the contact to these is extremely poor.

## 4.5 Other metals

A further prediction of the unpinned model is that the SBH should depend strongly on the work function of the metal contact. Carbon nanotube transistors can be ambipolar – the current-carrying carrier can be predominantly p-type or n-type, depending on the gate bias. A lower workfunction metal should give a lower  $I_p$  (current at  $V_g = -15V$ ) but higher  $I_n$  ( $V_g = +15V$ ), because of higher  $\phi_h$  but lower  $\phi_e$ . Figure 4.13 shows the distributions of these two quantities and they match the prediction from the unpinned model.

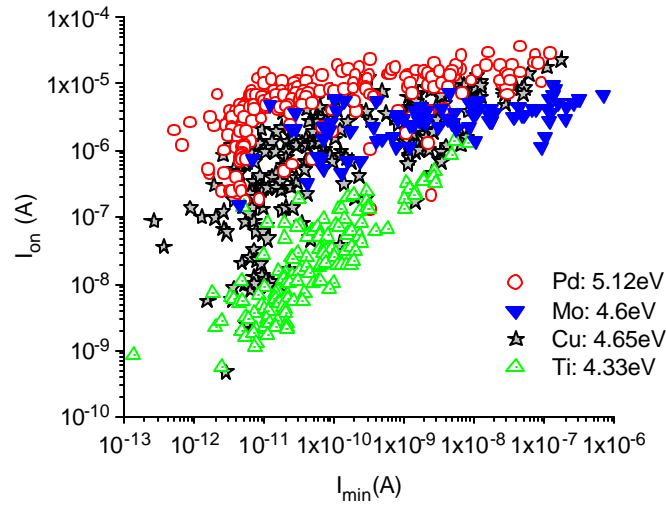


**Figure 4.13** Distribution of the currents at large gate bias. a) current at  $V_g = -15V$ . b) current at  $V_g = +15V$ . At  $V_g = +15V$ , Pd- and Cu-contacted devices with  $I_{min} > 1nA$  are relatively large in diameter ( $> 1.6nm$ ).  $V_d = 2V$  for all devices.

Ti, having the lowest average  $I_p$ , has the highest average  $I_n$ , whereas the reverse is true for Pd, the highest workfunction metal. Although exposure to oxygen can significantly increase the work function of Ti and Cu[34], the distributions in Fig. 4.13 suggest that Ti remains the metal with the lowest work function under the measurement

conditions. As such, Ti-contacted devices have the highest barrier for hole transport, but the lowest for electrons.

Even when these CNT devices are integrated with a CMOS circuit[18], the effect of diameter variation is still noticeable, as seen in figure 4.14. Mo has a workfunction of 4.6eV, similar to that of Cu (4.65eV), and leads to devices with similar on-currents as Cu. There is still a large spread in  $I_{min}$ , due to the spread in CNT diameter.



**Figure 4.14** Comparing the statistics of many isolated CNTFETs with those with Mo contacts and that are integrated with a Si-based CMOS circuit.

## 4.5 Conclusions

We experimentally verified that the junction between metal and semiconductor carbon nanotube is unpinned. The currents in the on- and off- state of a carbon

nanotube transistor depend sensitively on the diameter of the nanotube, as well as the work function of the contact metal, in a way that does not require the consideration of surface states and dipoles. Although the contacts are unpinned, the effect of geometry can complicate the precise relationship between the band gap and the Schottky barrier height. The results of compact modeling and temperature-dependent measurements across devices of different CNT diameters show that a side-contact geometry is a much better description.

For integrated circuit applications, a large-diameter nanotube with an appropriate metal contact is desirable for its low contact resistance, and enhanced mobility[35,36]. However, the off-current  $I_{min}$  associated with such devices will invariably be higher. The results presented here indicate that, for small diameter nanotubes (<1.5nm), a metal with higher work function than Pd will be needed to make barrier-free p-type electrical contacts. Similarly, to make barrier-free n-type contacts, a metal with a very low work function will be required. Low work function metals tend to oxidize rapidly and are difficult to work with. The need for two distinct metal work functions may be circumvented by using an approach involving heavily doped source and drain[37,38]. In addition, this approach seems to have the benefit of increasing on-state conduction while suppressing ambipolar leakage[36].

The statistical method employed in this work can also be extended to other types of study where large variability exists. An example is the optimization of the CVD process to control the nanotube diameter's distribution. By measuring the on- and off-

state currents of a large number of nanotube devices, the diameter distribution can be estimated rapidly. A statistical process optimization method, such as a factorial experiment, can then be used to optimize the growth process to obtain narrowly distributed diameters around a desired mean. The control over CNT diameter will present a step towards the large scale integration of carbon nanotube devices.

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# Chapter 5

## Capacitance Measurement of Metal-Semiconductor Carbon Nanotube Schottky Contacts

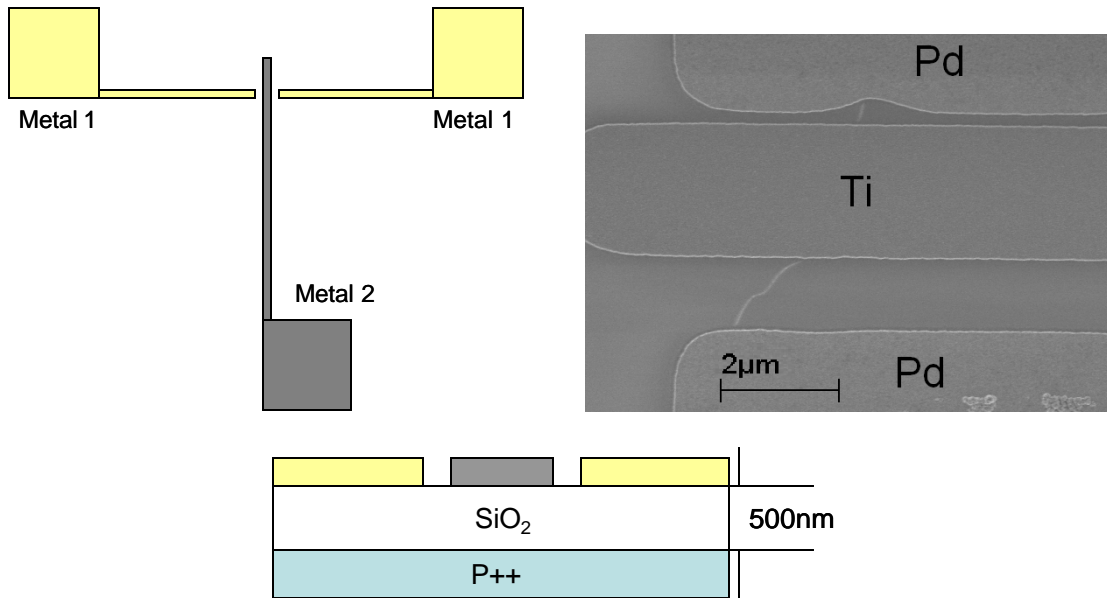
In chapter 4 it was discussed how the Fermi-level at the contact between semiconductor carbon nanotubes and metal is essentially unpinned. The Schottky Barrier Height (SBH), probably the most important parameter of a metal-semiconductor (MS) contact, was deduced using compact modeling. Chen *et al*[1] also extracted SBH using a model based on non-equilibrium Green's function (NEGF). Appenzeller used a simple argument to qualitatively deduce the SBH from the transfer characteristics of a nanotube transistor [2]. Nevertheless, these methods do not directly measure the SBH of the MS contact, but rely instead on the validity of the transport and device models.

Unlike bulk MS contacts, there is no convenient way of measuring this device parameter, due primarily to the smallness of the contact area. As concluded in chapter 4, the area of the contact is in the order of  $10\text{nm}^2$ , much too small for photoemission measurements, a widely accepted way for measuring SBH[3]. My own temperature-dependent transport measurements of a CNT Schottky diode structure reveal that many thermally activated processes are present, possibly due to on-tube defects, making a reliable determination of the SBH difficult. The only obvious alternative is the C-V measurement. Although the standard laboratory apparatus is inadequate to this task, the instrument described in chapter 1, as the results in this chapter show, is capable of measuring this important parameter in a straightforward manner.

## **5.1 The Test Structure for C-V Measurement and Its Fabrication**

The test structure for measuring the capacitance of a metal-CNT Schottky contact is a Schottky diode, similar to what is needed for measuring a Schottky contact in bulk. Two MS contacts are necessary: the Schottky contact to be measured, and a low-resistance ohmic contact to the semiconductor carbon nanotube. For all devices studied in this chapter, the ohmic contact is made using a metal stack of 50nm Pd/1nm Ni, and the Schottky contact is varied between Ti, Nb, and Cr. Although the Pd/Ni contact may be a Schottky contact, its resistance is in general much smaller than any capacitive reactance in parallel and it can be considered ohmic for all practical purposes. This is not the case for the Schottky Ti-CNT contact, where the capacitance can actually be significant as will be shown.

The test structure is illustrated in figure 5.1. The gap between the electrodes is about  $1\mu\text{m}$ . A back gate, separated from the nanotube and the S/D contacts by 500nm of silicon dioxide, can be used to modulate the conductivity of the bulk of the nanotube. The background parasitic capacitance can be measured by turning off the nanotube. The oxide needs to be thick to prevent excessive loss across the Schottky contact via tunneling, as well as to prevent the S/D electrodes from shorting to the back gate during wire bonding. The ultrasonic power used to create a strong mechanical bond between the bonding pad and the wire can damage the material directly under the bond. It was found that oxide at least 200nm thick is needed to prevent shorting the S/D electrodes to the substrate.

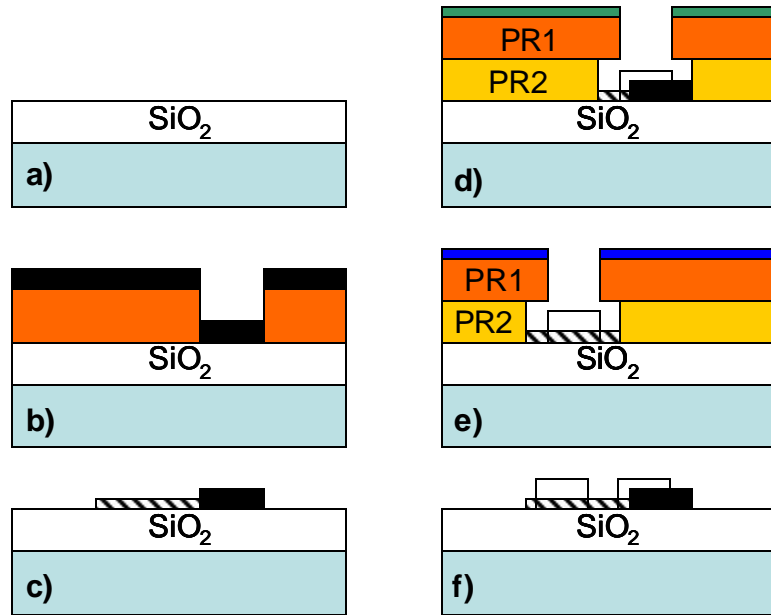


**Figure 5.1** Test structure for C-V measurement. Only one such structure is placed on each 5mmx5mm die to reduce the background parasitic capacitance. The SEM picture shows a nanotube bridging the two dissimilar electrodes. The contact to Ti is Schottky while the contact to Pd is ohmic.

The device can also be damaged by the ultrasonic power if it is too close to the wirebond. To reduce this problem, the bonding pads are purposely placed far away

(200 $\mu\text{m}$ ) from the device, and their area minimized to reduce shunting capacitance to ground as shown in figure 5.1. As described in chapter 1, only two devices are placed on each die to minimize the number of floating electrodes in order to reduce the background parasitic capacitance.

The fabrication procedures of the test structure are illustrated in figure 5.2. Starting from a heavily boron-doped silicon wafer, wet oxidation is used to grow 500nm of silicon dioxide. Followed is the definition of a global alignment mark, etched into the oxide layer using buffered HF. The catalyst for growing CNTs is then deposited and patterned using lift-off, using previously established procedures [3]. Single-walled carbon nanotubes are then grown using CVD methods. Next, the Pd/Ni ohmic contacts are realized by e-beam evaporation followed by lift-off. The Schottky contacts are also realized the same way. The Ni layer is only 1nm thick and helps the Pd metal to stick to the oxide surface. Ni has a large workfunction, and does not degrade the electrical contact to the CNT significantly.



**Figure 5.2** Fabrication procedure of the C-V test structure. a) Thermal oxidation. b) Catalyst deposition and lift-off. c) Nanotube growth. d, e) Patterning of metal 1 (Ni/Pd) and 2 (Ti, Nb or Cr) using a lift-off stack of photoresist (I-line resist on MicroChem LOR3A). f) Completed device.

Because there are only two devices per die, it is necessary to fabricate the test devices on a wafer scale to reduce cost. However, it is impossible to insert the 4" Si wafer, on which steps a-b in figure 5.2 are performed, into the 2.5" wide furnace tube for growing the nanotubes. A work-around is to cut the wafers in half before inserting them in the CNT growth furnace. The two remaining lithography steps that follow are performed using the same GCA 6200 stepper, operated in manual mode. Although the wafer pieces are manually loaded, alignment precision of better than 1 $\mu$ m is still possible. These work-arounds are awkward, but they are necessary because of the small furnace size for growing nanotubes. Post-processing of other bottom-up nanowires and nanotubes on a wafer scale has the same problem, since the chambers for growing these

objects are often too small to accept a full wafer. Significant engineering efforts remain in scaling up these bottom-up processes.

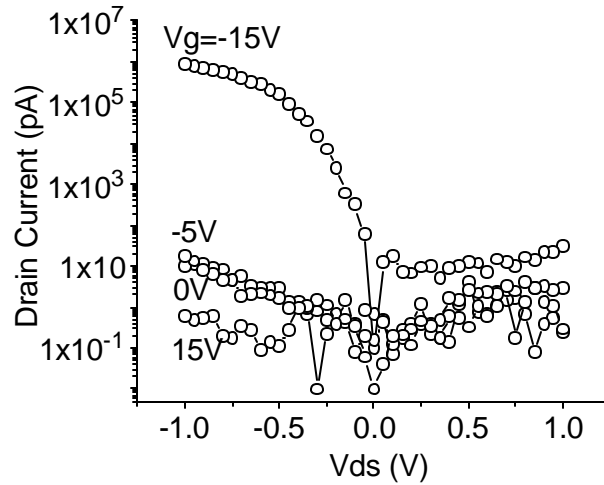
## 5.2 Transport Characteristics of Metal-Semiconductor Schottky Diodes

The transport characteristics of a Schottky diode are shown in figure 5.3. As expected, the device is rectifying. When  $V_{ds}$  more negative than the turn-on voltage  $V_n$  is applied to the titanium electrode, large current starts to flow. Qualitatively, the negative bias applied to the titanium electrode lowers the hole barrier, causing current to flow. The negatively biased back gate electrostatically dopes the tube p-type, allowing conduction of holes in the channel. Reverse leakage starts to develop at large positive  $V_{ds}$ , when the energy bands are sufficiently bent to allow band-to-band tunneling from the valence to the conduction band of the nanotube.

$V_n$  should be directly related to the SBH[4]. Indeed,  $V_n$ , defined here as the x-intercept of the line tangent to the I-V curve at its steepest point, clearly decreases with the nanotube diameter (figure 5.4), when measured in vacuum. When measured in air, the scatter is such that no clear correlation emerges between  $V_n$  and the diameter. The work function of Ti can be strongly affected by exposure to oxygen, and a prior work shows that this exposure can dramatically change the SBH[5].

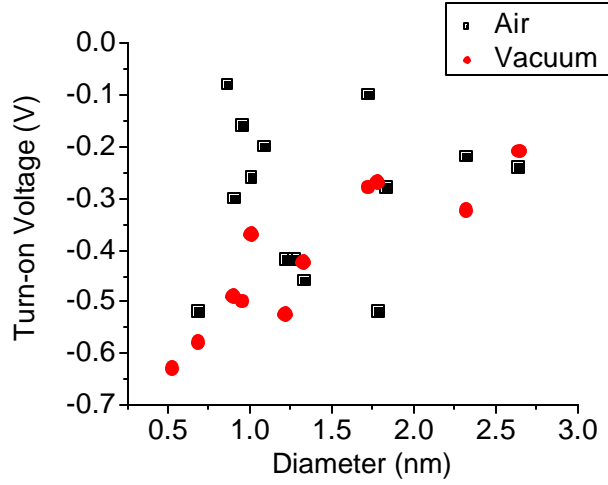
Gas molecules on a metal surface usually do not desorb by simply reducing the ambient pressure to  $3 \times 10^{-5}$  torr, the pressure at which the I-V measurements were

made. One possibility is that Joule heating at the contacts facilitated the desorption of oxygen molecules, as concluded by Dong *et al* [6]. Wind *et al* demonstrated that annealing at 425°C in an inert environment [7] can modify the Ti workfunction sufficiently so the contact changes from p- to n-type. Furthermore, Heinze *et al* [5] demonstrated that electrical conduction through the Ti-CNT contact is extremely sensitive to exposure to oxygen, even at relatively high oxygen partial pressures ( $10^{-1}$  to  $10^{-4}$  torr). Since the contact area to the carbon nanotube is small, only the gas molecules near that region need to desorb to change significantly the SBH. It is not necessary that gas molecules desorb completely from a large area, which would require a much better vacuum environment.



**Figure 5.3** I-V Characteristics of a Pd-CNT-Ti Schottky diode at various back gate voltages  $V_g$ , exhibiting rectifying behavior. It is necessary to apply a large negative bias to the substrate to make conductive the bulk of the nanotube. At large positive back gate biases there is no appreciable current flow.



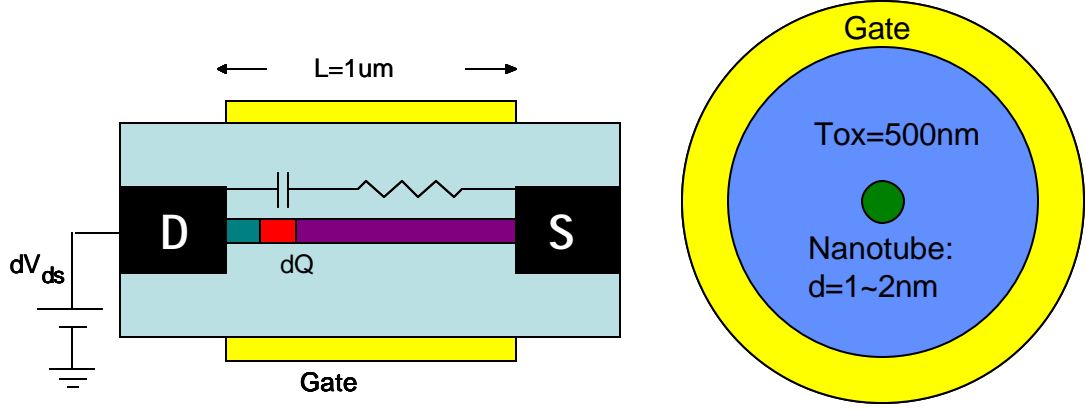


**Figure 5.4** Turn-on voltage  $V_n$  vs diameter for a set of devices measured in ambient conditions and vacuum. The backgate voltage ( $V_g - V_t$ ), is -5V for all devices. The vacuum is about  $3e-5$  torr.

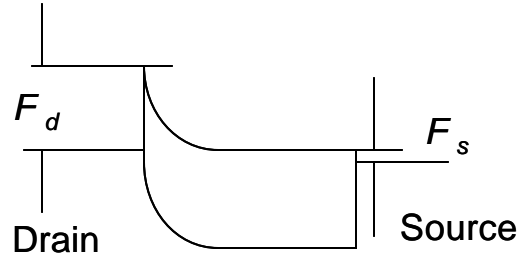
### 5.3 Simulation of the C-V Measurements

We estimate the magnitude of the capacitance using a Poisson-Schroedinger solver for 1-D semiconductors[8]. The simulated structure is shown in figure 5.5. The semiconductor CNT is surrounded by a concentric gate and insulator, and contacted with the source and drain electrode at each end of the nanotube. The SBH of each contact electrode can be specified independently. To model the Ti-CNT Schottky diode, the source work function is aligned to the conduction band, and that of the drain to the middle of the bandgap (figure 5.6). The simulation is done for electrons. Since the conduction and valence bands are symmetrical, trivial modifications lead to the same results for holes. Although the results presented below are those of a concentric geometry, simulation results using a planar geometry largely agree, provided that an effective dielectric constant ( $\epsilon_r=1.77$ ) is used for the gate dielectric. This approximation

is similar to that used for modeling thin striplines in microwave circuits, and the value of  $\epsilon_r$  is consistent with that deduced from chapter 3.



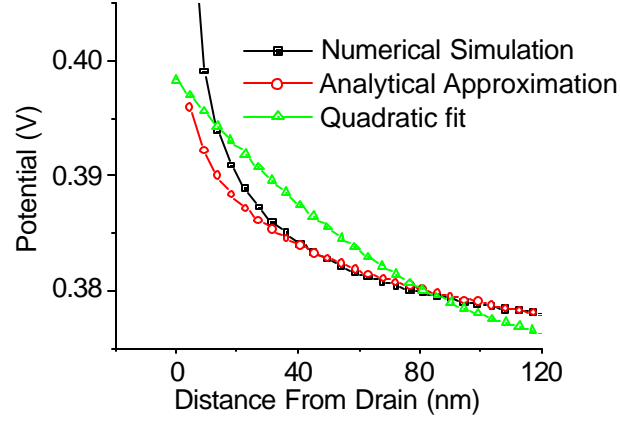
**Figure 5.5** Device structure for simulating the C-V measurement. Left: side view. Right: front view. S: source. D: Drain. The capacitance is estimated by calculating the small change in charge  $dQ$  for a small change  $dV_{ds}$ . The gate surrounding the device serves to turn on the nanotube. The dielectric medium (blue) has a relative permittivity of  $\epsilon_r = 1.77$  to match the results of simulation with a planar geometry.



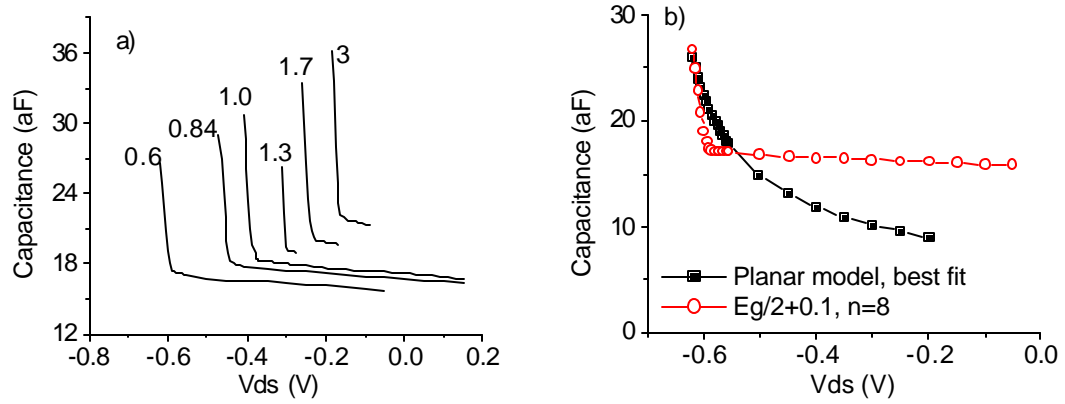
**Figure 5.6** Energy alignment of the simulated device.  $F_s$  = SBH of the source contact.  $F_d$  = SBH of the drain contact. A gate bias is applied to put charges (electrons) on the bulk of the tube.

Two different C-V measurements are simulated. The first is the capacitance across the source and drain versus the voltage  $V_{ds}$  across the same two electrodes, with a fixed and non-zero gate voltage. This simulates the actual experiment where the nanotube is gated on, and  $V_{ds}$  is swept to see any change in the capacitance. This measurement is very similar to what would be done for a bulk Schottky contact, with the exception that an extra gate terminal is needed to make the nanotube conductive.

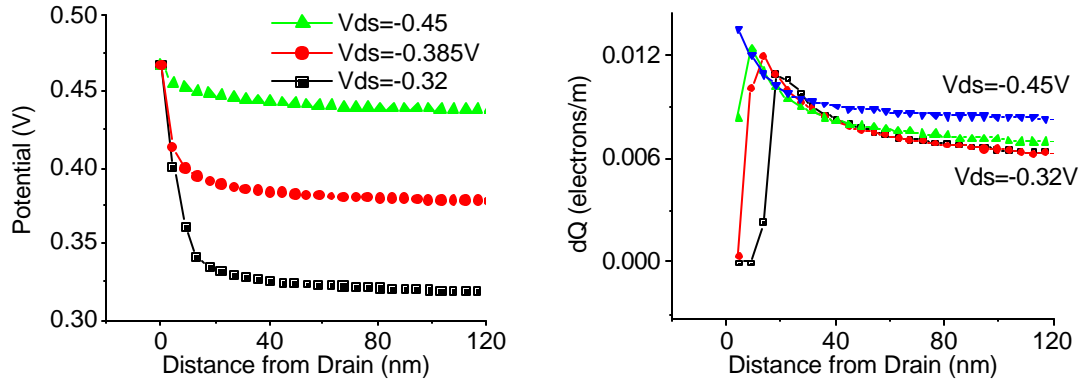
The bias applied at the gate terminal can be thought as a way to electrostatically “dope” the nanotube.



**Figure 5.7** Potential along the length of a nanotube with  $V_{ds}$  applied along its length. The simulated geometry is that shown in figure 5.5.



**Figure 5.8** a) Simulated  $C$ - $V_{ds}$  curves for Schottky Junctions of various CNT diameters (in nm). The SBH is set as  $E_g/2+0.1$  (eV). b) Comparison of the simulated  $C$ - $V_{ds}$  curve to a planar model  $\sim B/(V_{bi}-V_{ds})^{0.5}$ , with fitting parameter  $B$ , and  $V_{bi}=0.67$ V, the SBH in the numerical simulation.



**Figure 5.9** a) Potential profile near the Schottky junction for different applied bias  $V_{ds}$  across it. b) Charge density  $dQ$  modulated by applied bias  $dV_{ds}$  across the source-drain of the Schottky junction.

As predicted from an early work on electrostatic in objects with one-dimensional electronic density of states, potential applied across the long axis of the tube is poorly screened and falls as  $\sim \ln(T_{ox}/x)$  along the nanotube [9], where  $T_{ox}$  is the dielectric thickness between the gate metal and the nanotube. Figure 5.7 shows the comparison between the results of numerical simulation, analytical approximation, and a best quadratic fit, showing the agreement between the former two. This is expected since the junction geometry is far from planar. Figures 5.9a-b show the potential and charge profile as  $V_{ds}$  is varied. As the built-in voltage is reduced and the entire device brought close to flat-band, more charges are accumulated along the entire length of the tube, evidence of the long screening length in the carbon nanotube. In addition, the peak position of charge accumulation moves closer to the drain, analogous to what happens in bulk, where the depletion width is narrowed upon canceling the built-in voltage.

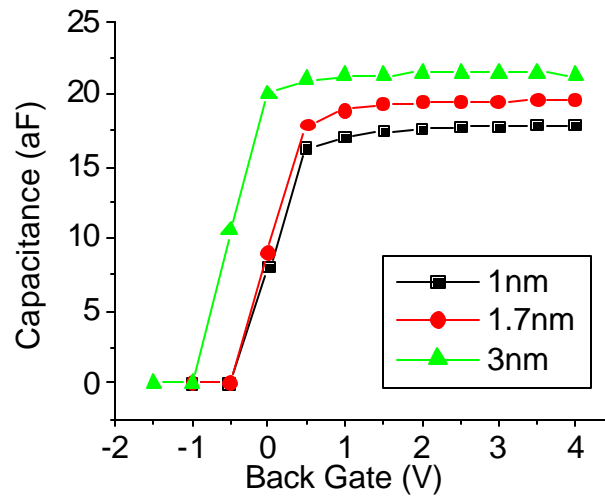
The simulated  $C$ - $V_{ds}$  curves for different nanotube diameters and Schottky barrier height are shown in figure 5.8a. Figure 5.8b shows that the capacitance

obviously does not follow the  $\sim 1/(V_{ds}-V_{bi})^{1/2}$  rule in a planar junction. Rather, it increases very slowly, and increases very steeply just before flatband, when the applied bias just about cancels the SBH. This steep increase reflects the occupation of the 1<sup>st</sup> subband as the potential profile becomes flat, as evidenced in figure 5.8. As the potential profile is biased to flat-band, the quasi-Fermi level moves closer to the band edge, leading to a sudden increase in charge. At this condition, the same modulation  $dV_{ds}$  changes the amount of charge  $dQ$  on the tube more significantly (figure 5.9b), more so than a reverse-biased junction. Thus, in measuring the curve  $C$ - $V_{ds}$ , and finding where it increases very steeply, one can readily extract the SBH of the junction.

A second useful measurement to simulate is the capacitance across the S/D electrodes versus the gate voltage  $V_g$ , at a zero bias across the S/D. This measurement extracts the capacitance of the junction relative to the background parasitic, at zero  $V_{ds}$ . This parameter represents essentially the electrostatic coupling between the drain contact and the channel, very similar to what would describe DIBL in a MOS compact model. To obtain a numerical value of the capacitance  $C$ - $V_g$ , we calculate the change in charge ( $dQ$ ) on the entire tube as a function of a small change in the drain voltage ( $dV_{ds}$ ), and set  $C=dQ/dV_{ds}$ . This is repeated for a range of gate voltages  $V_g$ . Figure 5.10 and 5.11 show the simulation results and the dependence on nanotube diameter. Qualitatively, this parameter is related to  $C_{ox}$  in a very simple way. As a small change  $dV_{ds}$  is applied, the threshold voltage  $V_t$  changes to  $V_t'$  due to DIBL, and the amount of charge on the tube changes as well. An equation that describes this would be:

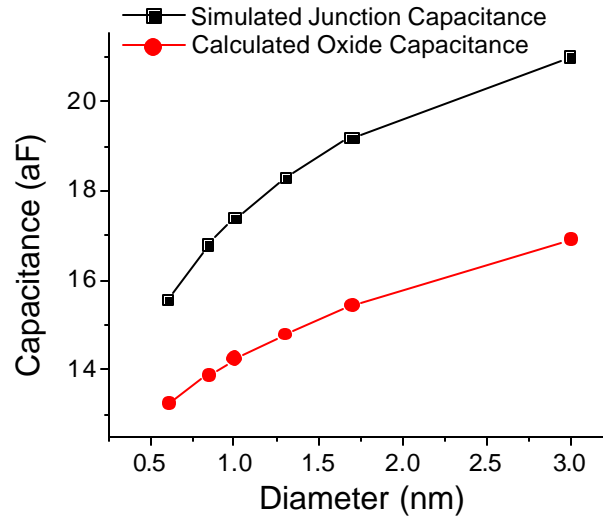
$$dQ = C_{ox} (V_g - V_t) - C_{ox} (V_g - V_{t'}) = C_{ox} (V_{t'} - V_t) \quad (5.1)$$

where  $V_t$ ,  $V_{t'}$  are threshold voltages for charge accumulation on the nanotube for each applied voltage  $V_{ds}$ . Thus, the measurement  $C$ - $V_g$  would give a good measure of the diameter of the nanotube, without having to measure the actual diameter, which can be difficult if the surface is dirty, or intentionally covered with a dielectric layer.



**Figure 5.10** Simulated C-Vg curves for Schottky diodes of three diameters.  $V_{ds}=0$ .

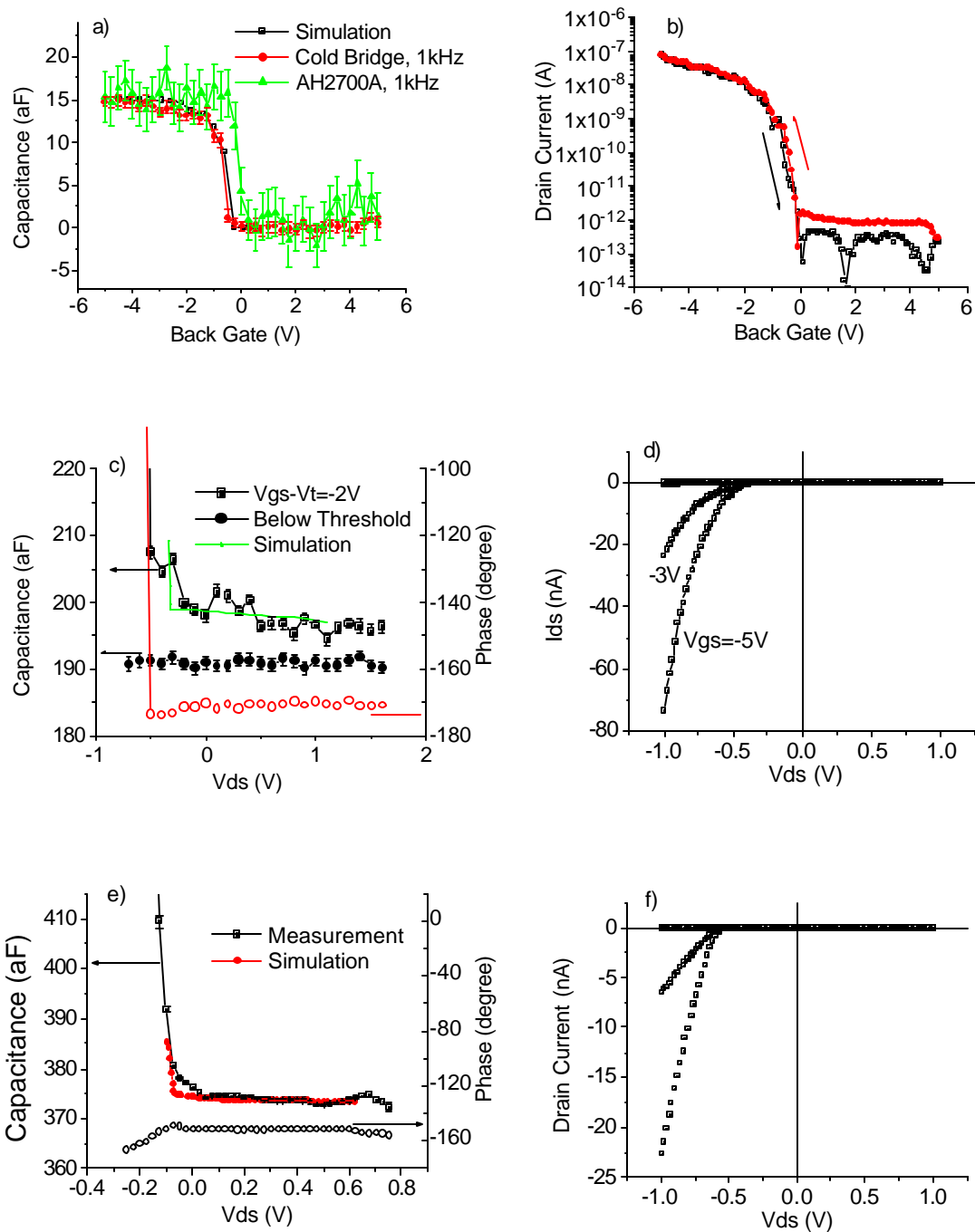
This quantity is previously measured in a CNT transistor using Coulomb Blockade measurement at very low temperatures ( $\sim 30\text{mK}$ ) [10], and showed qualitatively the same behavior as the simulations above, although with a smaller numerical value ( $\sim 3\text{aF}$ ). This may be because the nanotube in [10] was suspended in air, which reduces the effective dielectric constant between the drain and the channel, and because the amount of charges stored on it limited by the nanotube length.



**Figure 5. 11** Simulated  $C$ - $V_g$  as a function of nanotube diameter.

#### 5.4 Measurement results

The measured  $C$ - $V_g$  curve of a CNT Schottky diode is shown in figure 5.12. The measurements are performed with the home-built cold bridge and the AH2700A commercial capacitance bridge. Very little loss is observed using either method. The two curves agree well, except near the threshold  $V_t$ . This is due to the larger AC excitation that is needed for the AH2700A to obtain a signal of useful size. Several control experiments were repeated with the identical electrode layout, but without a nanotube in between. In all these cases, the capacitance is observed to stay constant to less than 1 aF over the full range of applied gate and source/drain biases.

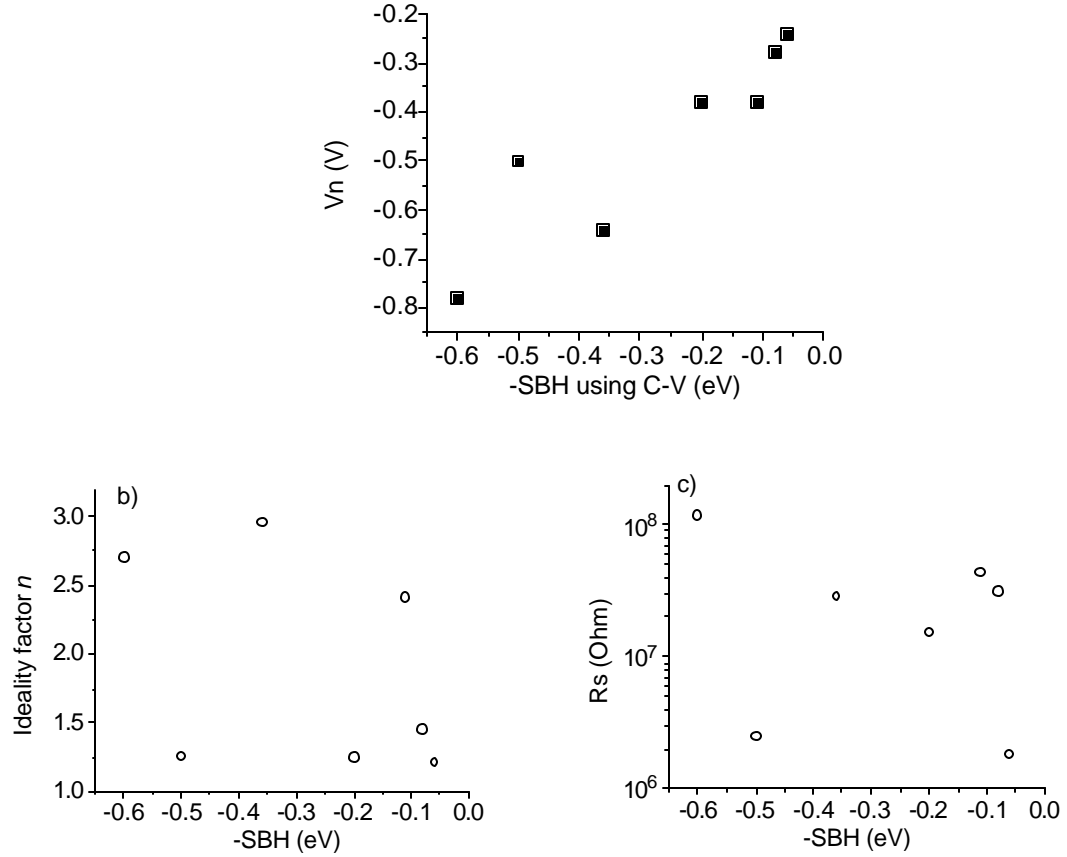


**Figure 5.12** a) Capacitance across a Ti-CNT Schottky junction as a function of back gate bias, measured using both the cold bridge and a commercial bridge. b)  $I_d$ - $V_g$  characteristics of the same device ( $V_{ds}=-1V$ ). c) Capacitance as a function of voltage across the Ti-CNT Schottky junction. d)  $I_d$ - $V_d$  characteristics of the Ti-CNT Schottky diode for several back gate voltages. e)  $C$ - $V_{ds}$  of an Nb-CNT Schottky junction, showing remarkable agreement with simulation. f)  $I_d$ - $V_d$  of the Nb-CNT Schottky diode.



The change in capacitance with applied gate bias shown in figure 5.12a (15aF) matches well with that expected from simulation. Comparison with the  $I_d$ - $V_g$  characteristics shows that the abrupt increase in capacitance is due to the bulk of the nanotube becoming conductive, and the capacitance across the junction is measured in addition to the background. A qualitative agreement between simulation and measurement is also observed for the  $C$ - $V_{ds}$  measurement is shown in figure 5.12c. As  $V_{ds}$  becomes more negative, beyond a certain threshold, the capacitance increases steeply, until significant loss is encountered, as evidenced by the phase of the cold bridge output. The rapid increase in capacitance occurs at a much smaller voltage than that required for the device to conduct. Figure 5.12e shows the  $C$ - $V_{ds}$  curve of another device, with Nb as Schottky contact, and shows a much better agreement between simulation and experiment. The quality of the fit differs from device to device, because many non-idealities, such as surface charges and on-tube defects, are not modeled. The SBH found from the C-V measurements correlate well with the turn-on voltages extracted from IV measurement, as shown in figure 5.13a. Analyzing the room temperature I-V curves of these same diodes, it is revealed that the ideality factor  $n$  ranges from 1.2 to close to 3, with no clear correlation to the SBH (figure 5.13b). Previous report on CNT Schottky diodes made with dissimilar metals[11] also reported ideality factors between one and two. The larger  $n$  in some diodes may come from defects near the Schottky contact. The series resistance  $R_s$  is also extracted (figure 5.13c), and it also has no clear relation to the SBH.  $R_s$  should be determined by the bulk of the tube and the low resistance contact between the Pd metal and nanotube. Although it has no clear relationship to the SBH, it is nevertheless small enough to have

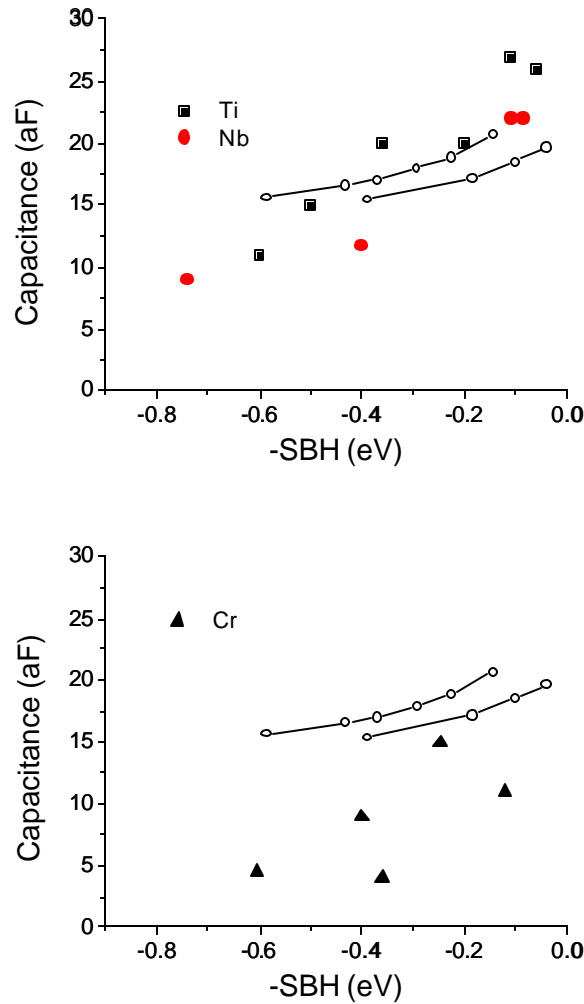
no impact on the capacitance measurement. The small oscillations in the  $C-V_{ds}$  curve are likely due to non-monotonic variation in the charge and potential profile along the tube, caused by neighboring charges on the oxide substrate. Such an undulating potential profile was observed previously[12].



**Figure 5.13** a) Turn-on voltage vs SBH measured using the C-V method. b) Ideality factor vs SBH. c) Series resistance  $R_s$  vs SBH.

The  $C-V_g$  measured on 15 devices varies from 10aF to 25aF. Plotting this change in capacitance versus the SBH extracted by the  $C-V_{ds}$  method in figure 5.14, a clear relationship becomes evident, where devices having larger  $C-V_g$  also has a smaller barrier height. Using our simulator, this relationship is mostly reproduced and is shown

in figure 5.14. Essentially, the magnitude of the capacitance reflects simply the diameter of the nanotube, and its apparent dependence on SBH is the result of the unpinned junction. As evidenced in figure 5.14a-b, there is a lateral shift for the data series of devices with a Cr contact relative to those with Ti, since Cr has a higher workfunction (4.5eV). Devices with an Nb MS contact give very similar results to those with Ti, since these metals have very similar work function (4.3eV for Nb vs 4.33eV for Ti).



**Figure 5.14** Capacitance  $C$ - $V_g$  as a function of measured SBH. The open symbols are the simulated  $C$ - $V_g$  with the Schottky Barrier Height being related to the band gap  $E_g$  as  $E_g/2+0.1$  and  $E_g/2-0.1$ .

The size of the shift in the Cr data series (0.1-0.3eV) is in agreement with the workfunction difference between Ti (Nb) and Cr, confirming once again the unpinned nature of the MS contact. However, the magnitude of the measured C-V<sub>g</sub> for devices with Cr contacts differs considerably from simulation. It is possible that details of the contact geometry are different for Cr, like the case for Pd. Further modeling, perhaps on an ab-initio basis, is warranted to fully understand the discrepancy.

## 5.5 Summary and Future Work

In summary, we have developed a method to measure the capacitance across a nanoscale Schottky contact. In our model system of Ti-CNT Schottky barrier, the experimental results match well with the calculations based on a Poisson-Schroedinger device simulator. We have extracted Ti-CNT Schottky barrier heights that are consistent with the results of I-V measurements. The capacitive measurement of the SBH across MS contacts involving different metals show once again the unpinned nature of the contact. Nb-CNT contacts are similar to Ti, but Cr is rather different. MS contacts with a larger metal workfunction may not fit well to the end-contact picture, as illustrated in chapter 4.

The Pd-CNT contact, or any other low-barrier height contacts, are of particular interest. To measure the barrier height in these systems using the C-V method would be very difficult since these junctions are effectively very lossy capacitors. A possible way to work around this problem would be to measure instead the barrier height of the

electrons, which should be large for Pd-CNT contacts. For this purpose, a reliable n-type MS contact is then necessary, and would require the use of very low work function metals. Sc[13] seems to be a possible solution, although there are no confirmation that these results are reproducible. Al also has a low work function, but is only successfully employed for large diameter nanotubes [14], and leads to Schottky diodes with large leakage and no obvious rectifying behavior.

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- [14] The author has experimented with making Al-CNT-Pd diodes, which fail to conduct at all except for large diameter nanotubes ( $>4\text{nm}$ ). Also from private communication with A. Javey.

# Conclusions

This work demonstrated the application of the standard capacitance-voltage measurement technique to small devices and junctions. Using this non-destructive characterization method, basic information about very small semiconductor junctions were obtained in an unambiguous way. The test structure shown in chapter 1 should be general enough for any variety of nanowires, nanotubes, and gate stack materials. In this work, the following were studied: boron diffusion profile in a single silicon nanowire, the metal-carbon nanotube Schottky contact, as well as the native surface of an InAs nanowire. The information obtained from these studies confirm that 1) the

diffusion of boron in silicon nanowires is dominated by the interstitial-assisted mechanism, 2) the metal-carbon nanotube Schottky contact is unpinned, and 3) electron mobility in small InAs nanowires is limited by surface scattering.

Bottom-up, nanoscale materials hold promise in many applications. Since surface effects often dominate the behavior of these materials, a direct method for characterizing the surface of each individual object is important. The methods and instrumentation described in this work show that this is possible despite of the small area inherent to these materials. Other devices and junctions of interest that can be studied using this technique include but are not limited to the following: abrupt PN junction and heterojunction for tunneling transistors, organic gate dielectric for organic electronics, and very small FinFets. The list is limited only by the imagination of the investigator.

Although the instrument developed here was operated at cryogenic temperatures, this method can conceivably be extended to ambient conditions, where most devices operate. The only significant problem to be solved is the design of a circuitry that has similar noise characteristics at room temperature. It would also be necessary to extend the operating frequencies of this instrument to several MHz. This next progress would expand the reach of this technique to operating conditions typical of solid-state devices, an important point to consider in any work in this field.