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Plasma Slab with Steep Density Gradient

M. J. Gerver and C. K. Birdsall

**Department of Electrical Engineering and Computer Sciences
and Electronics Research Laboratory
University of California, Berkeley, California 94720**

**A. B. Langdon and D. Fuss
Lawrence Livermore Laboratory
University of California, Livermore, California 94550**

The main text of this report (excluding the appendices), with minor changes, has been accepted for publication in Physics of Fluids.

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ABSTRACT

The electrostatic flute-like normal modes were found for a collisionless loss cone plasma in a uniform magnetic field with density varying sinusoidally in one direction in space. A local method, appropriate to $kL \gg 1$, where k is the wave number and L the scale length, and a nonlocal method, appropriate to $kL \leq 1$, were both used; the ion Larmor radius a_i was not assumed to be small. The usual drift cone mode was found when $a_i \ll L$; other instabilities were found for $a_i \gtrsim L$. In principle, the methods could be applied to other configurations of plasma.

Research sponsored by the Energy Research and Development Administration
Contract E(04-3)-34-PA128.

I. Introduction

In analyzing the kinetic instabilities of a non-uniform plasma the assumption is frequently made^{1,2} that the Larmor radius is small compared to the scale length of the plasma, although in many experiments³ the ion Larmor radius a_i is comparable to the scale length L . We have found that it is often possible to find the normal modes, and even to use a local approximation, without assuming $a_i \ll L$. The procedure starts with the integrodifferential Vlasov-Poisson dispersion relation for the electrostatic modes of a non-uniform collisionless plasma. Two different approximate methods can be used to solve this integral equation, reducing it to either a differential equation or a matrix equation. Each method is valid in a different regime, but neither method requires $a_i \ll L$. The two methods have been used to find the properties of the most unstable flute-like mode of a deuterium loss cone plasma with a density varying sinusoidally in space in a direction perpendicular to a uniform magnetic field, for a variety of densities, density gradients, and mirror ratios. (The sinusoidally varying density was used because it simplifies the calculations and because it has been used in computer simulations of the drift cone mode^{4,5}.) The numerical results of the two methods are in good agreement (typically within 10%) in the regime where both are expected to be valid, thus increasing our confidence in them.

In Sec. II the integrodifferential dispersion relation will be derived for an arbitrary configuration of plasma and magnetic field, as well as for the special case of a uniform magnetic field, and we will discuss the reasons for the usual assumption that $a_i \ll L$, and under what circumstances this assumption can be dispensed with. In Sec. III the two methods of solving the integral equation will be described and

applied to a loss cone plasma with sinusoidally varying density. The range of validity of each method will be found. In Sec. IV the numerical results obtained by the two methods will be given, and the numerical techniques used will be briefly described. In Sec. V the physical significance of these results (particularly for $a_i \gtrsim L$) will be discussed, and a summary and conclusions will be presented in Sec. VI.

II. Dispersion Relation

The linearized Vlasov equation for a plasma with an electrostatic perturbation is

$$\frac{df_{1s}}{dt}(x, v, t) = -\frac{q_s}{m_s} \nabla \phi(x, t) \cdot \frac{\partial f_{0s}}{\partial v}(x, v) \quad (1)$$

where f_{1s} is the first-order perturbation in the distribution function, f_{0s} is the zero-order equilibrium distribution function (satisfying $\partial f_{0s}/\partial t = 0$), q_s is the charge and m_s is the mass for species s ; and ϕ is the perturbed potential. Eq. (1) can be integrated over the zero-order particle orbits to obtain

$$f_{1s}(x, v, t) = \frac{q_s}{m_s} \int_{-\infty}^t d\tau \nabla \phi[x'_s(\tau), \tau] \cdot \frac{\partial f_{0s}}{\partial v_s}[x'_s(\tau), v'_s(\tau)] \quad (2)$$

where $x'_s(\tau)$ is the unperturbed orbit of a particle of species s , and $v'_s(\tau) \equiv dx'_s/d\tau$, with $x'_s(t) = x$ and $v'_s(t) = v$.

Eq. (2) is combined with the Poisson equation

$$\sum_s 4\pi q_s \int f_{1s}(x, v, t) dv + \nabla^2 \phi(x, t) = 0$$

to yield the well-known result⁶

$$\sum_s \frac{4\pi q_s^2}{m_s} \int dy \int_{-\infty}^t d\tau \nabla \phi(\underline{x}_s', \tau) \cdot \frac{\partial f_{os}}{\partial \underline{v}'_s} (\underline{x}_s', \underline{v}_x') + \nabla^2 \phi(\underline{x}, t) = 0 \quad (3)$$

Eq. (3) can be Fourier transformed in \underline{x} : (See Appendix A)

$$\int dk \tilde{\phi}(k) \left(\int dk' \exp(i\underline{k}' \cdot \underline{x}) \left\{ \sum_s \frac{4\pi q_s^2}{m_s} \int dy \int_{-\infty}^0 d\tau \right. \right. \\ \left. \left. ik' \cdot \frac{\partial f_s}{\partial \underline{v}'_s} (\underline{k}-\underline{k}', \underline{v}_s') \exp[ik' \cdot (\underline{x}_s' - \underline{x}) - i\omega\tau] \right\} - k^2 \right) = 0 \quad (4)$$

$$\text{where } \tilde{f}_s(k, v) \equiv (2\pi)^{-3} \int dx f_{0s}(x, v) \exp(ik \cdot x)$$

$$\tilde{\phi}(k) \equiv (2\pi)^{-3} \int dx \phi(x, 0) \exp(-ik \cdot x)$$

and $\phi(x, t)$ is assumed to vary in time as $\exp(-i\omega t)$.

Eq. (4) can be written in compact form as

$$\int dk \exp(ik \cdot x) \tilde{\phi}(k) D(x, k, \omega) = 0$$

or

$$D(x, i\nabla, \omega) \phi(x) = 0 \quad (5)$$

where D/k^2 is the usual dielectric function, defined by

$$D(x, k, \omega) \equiv -k^2 + \sum_s D_s(x, k, \omega) \\ D_s(x, k, \omega) \equiv \frac{4\pi q_s^2}{m_s} \exp(-ik \cdot x) \int dk' \exp(ik' \cdot x) \\ \int dy \int_{-\infty}^0 d\tau ik' \cdot \frac{\partial f_s}{\partial \underline{v}'_s} (\underline{k}-\underline{k}', \underline{v}_s') \exp[ik' \cdot (\underline{x}_s' - \underline{x}) - i\omega\tau] \quad (6)$$

If the magnetic field varies over a distance comparable to a Larmor radius, then it is difficult to calculate the zero-order orbits $\tilde{x}_s'(\tau)$, and to find an equilibrium distribution function $f_{0s}(x, v)$. In a low- β plasma, however, it is possible for the scale length of the magnetic field (i.e. $B_0 / |\nabla B_0|$) to be much greater than the scale length of the plasma, so we can assume the magnetic field $B_0(x)$ to be uniform in space, or varying gradually, in calculating the particle orbits and the constants of motion, without assuming that $f_{0s}(x, v)$ varies gradually as a function of x . For uniform B_0 , the constants of motion are v_\perp , v_\parallel , and $\tilde{x}_{gc\perp} \equiv x_\perp + v \times \hat{B}_0 \omega_{cs}^{-1}$ (where \hat{B}_0 is a unit vector parallel to B_0 , and v_\perp and v_\parallel are components of v perpendicular and parallel to B_0), so

$$f_{0s}(x, v) = g_s(v_\perp, v_\parallel, \tilde{x}_{gc\perp})$$

and (see Appendix A)

$$\tilde{f}_s(k, v) = \exp[-ik \cdot (v \times \hat{B}_0) \omega_{cs}^{-1}] \tilde{g}_s(v_\perp, v_\parallel, k) \quad (7)$$

where

$$\tilde{g}_s(v_\perp, v_\parallel, k) \equiv (2\pi)^{-3} \int dx g_s(v_\perp, v_\parallel, x) \exp(ik \cdot x)$$

The particle orbits are

$$\begin{aligned} \tilde{x}_s'(\tau) &= x + \frac{v_\perp}{\omega_{cs}} \sin \omega_{cs} \tau + \frac{v \times \hat{B}_0}{\omega_{cs}} (1 - \cos \omega_{cs} \tau) \\ &\quad + v_\parallel \hat{B}_0 \tau \end{aligned} \quad (8)$$

[For non-uniform $B_0(x)$, the particle drifts would have to be included in Eq. (8) as well, and the constants of motion replaced by adiabatic constants of motion.]

Putting Eqs. (7) and (8) into Eq. (6), and using the Bessel function identity⁷

$$\exp(i a \sin \theta) = \sum_l J_l(a) \exp(il\theta)$$

we can do the integration over τ and over the azimuthal direction of \mathbf{v} to obtain (see Appendix A)

$$D_s(\mathbf{x}, \mathbf{k}, \omega) = \frac{4\pi q_s^2}{m_s} \exp(-i\mathbf{k} \cdot \mathbf{x}) \int d\mathbf{k}' \exp(i\mathbf{k}' \cdot \mathbf{x}) \int_{-\infty}^{\infty} dv_{\parallel} \\ \int_0^{\infty} 2\pi v_{\perp} dv_{\perp} \sum_{\ell} [\hat{\mathbf{k}}_{\perp} \cdot (\hat{\mathbf{k}}'_{\perp} + i\hat{\mathbf{B}}_0 \times \hat{\mathbf{k}}'_{\perp})]^{\ell} J_{\ell}\left(\frac{\mathbf{k}_{\perp} v_{\perp}}{\omega_{cs}}\right) J_{\ell}\left(\frac{\mathbf{k}'_{\perp} v_{\perp}}{\omega_{cs}}\right) \\ (\omega - \ell\omega_{cs} - k_{\parallel} v_{\parallel})^{-1} \left[\frac{-i\mathbf{k} \cdot (\hat{\mathbf{B}}_0 \times \hat{\mathbf{k}}')}{\omega_{cs}} \tilde{g}_s(v_{\perp}, v_{\parallel}, \mathbf{k} - \mathbf{k}') \right. \\ \left. - k_{\parallel} \frac{\partial}{\partial v_{\parallel}} \tilde{g}_s(v_{\perp}, v_{\parallel}, \mathbf{k} - \mathbf{k}') - \frac{\ell\omega_{cs}}{v_{\perp}} \frac{\partial}{\partial v_{\perp}} \tilde{g}_s(v_{\perp}, v_{\parallel}, \mathbf{k} - \mathbf{k}') \right] \quad (9)$$

where $k_{\parallel} \equiv \mathbf{k} \cdot \hat{\mathbf{B}}_0$, $\mathbf{k}_{\perp} \equiv \mathbf{k} - k_{\parallel} \hat{\mathbf{B}}_0$, $\hat{\mathbf{k}}_{\perp} \equiv \mathbf{k}_{\perp}/k_{\perp}$.

If the scale length of the plasma is much greater than a Larmor radius, then only $\mathbf{k}' \approx \mathbf{k}$ will contribute significantly to the integral over \mathbf{k}' in Eq. (9), and $D_s(\mathbf{x}, \mathbf{k}, \omega)$ can be expressed in terms of $g_s(v_{\perp}, v_{\parallel}, \mathbf{x})$, and its gradient at the same point \mathbf{x} in space⁸: (see Appendix B)

$$D_s(\mathbf{x}, \mathbf{k}, \omega) = - \frac{4\pi q_s^2}{m_s} \int dv_{\parallel} \int 2\pi v_{\perp} dv_{\perp} \sum_{\ell} J_{\ell}^2 \left(\frac{\mathbf{k}_{\perp} v_{\perp}}{\omega_{cs}} \right) \\ (\omega - \ell\omega_{cs} - k_{\parallel} v_{\parallel})^{-1} [\mathbf{k} \cdot (\hat{\mathbf{B}}_0 \times \nabla g_s)/\omega_{cs} + k_{\parallel} \partial g_s / \partial v_{\parallel} \\ + (\ell\omega_{cs}/v_{\perp}) \partial g_s / \partial v_{\perp}] \quad (10)$$

If a suitable $g_s(v_{\perp}, v_{\parallel}, \mathbf{x})$ is chosen, however, it may be possible to integrate Eq. (9) over \mathbf{k}' analytically; in this case there is no need to assume that the Larmor radius is small compared to the scale length.

III. Methods of Solution

We will consider only modes with $k_{\parallel} = 0$, so the integration over v_{\parallel} can be done by replacing $g_s(v_{\perp}, v_{\parallel}, \underline{x})$ by

$$g_{s\perp}(v_{\perp}, \underline{x}) \equiv \int dv_{\parallel} g_s(v_{\perp}, v_{\parallel}, \underline{x})$$

[with $\tilde{g}_{s\perp}(v_{\perp}, \underline{k})$ similarly defined] in Eq. (9). We will further assume that $g_{s\perp}$ is Maxwellian and that there are no temperature gradients

$$g_{s\perp}(v_{\perp}, \underline{x}) = (2\pi v_s^2)^{-1} \exp(-v_{\perp}^2/2v_s^2) n_s(\underline{x}).$$

A loss-cone distribution can be constructed by subtracting two Maxwellians⁹

$$\begin{aligned} g_{s\perp}(v_{\perp}, \underline{x}) &= [2\pi v_s^2(1-R^{-1})]^{-1} n_s(\underline{x}) \\ &[\exp(-v_{\perp}^2/2v_s^2) - \exp(-Rv_{\perp}^2/2v_s^2)] \end{aligned} \quad (11)$$

where R is the mirror ratio. The two components can be formally treated as two different species, with thermal velocities v_s and $v_s R^{-1/2}$.

For the rest of this paper, unless otherwise noted, all species will be assumed to have Maxwellian distributions, with the understanding that loss cone species will be formally treated as two different Maxwellian species.

Finally, we assume a slab geometry, with density $n_s(\underline{x})$ depending only on x and B_0 in the z direction. Then Eq. (9) becomes (see Appendix C)

$$\begin{aligned} D_s(\underline{x}, \underline{k}, \omega) &= \frac{4\pi q_s^2}{m_s} \int_{-\infty}^{\infty} dk'' \exp(ik''x) \sum_{\ell} \exp(i\ell\alpha) \\ &\exp[-(k^2 + k'^2) a_s^2/2] I_{\ell} (k^2 a_s^2) (\omega - \ell \omega_{cs})^{-1} \\ &(-ik_y k''/\omega_{cs} + \ell \omega_{cs}/v_s^2) \bar{n}_s(k'') \end{aligned} \quad (12)$$

where $k'' \equiv k'_x - k_x$, $k_y' \equiv k_y$, $\alpha \equiv i \log_e \left(\frac{k'_x + ik_y}{k'} \right)$ $- i \log_e \left(\frac{k'_x - ik_y}{k'} \right)$ is the angle between the vectors \underline{k} and \underline{k}' ,

$$a_s \equiv v_s / \omega_{cs},$$

and $\tilde{n}_s(k'') \equiv (2\pi)^{-1} \int_{-\infty}^{\infty} dx \exp(-ik''x) n_s(x).$

For a sinusoidal density profile,

$$n_s(x) = (1 + \Delta_s \cos k_0 x) n_{s0} \quad (13)$$

we have $\tilde{n}_s(k'') = (2\pi)^{-1} n_{s0} [\delta(k'') + (\Delta_s/2) \delta(k'' + k_0) + (\Delta_s/2) \delta(k'' - k_0)].$

(There is no requirement that Δ_s be small, in fact usually we will use

$\Delta_s \approx 1$; see Fig. 1.)

Then the integral over k'' in Eq. (12) becomes a sum over three terms, $k'' = 0, -k_0, +k_0$. Since we are assuming no equilibrium electric fields, we must have

$$\sum_s q_s \int d\underline{v} f_{0s}(x, \underline{v}) = 0 \text{ for all } x$$

or (see Appendix D)

$$\sum_s q_s n_{s0} \Delta_s \exp(-k_0^2 a_s^2 / 2) = 0 \quad (14a)$$

and

$$\sum_s q_s n_{s0} = 0 \quad (14b)$$

The eigenmodes $\phi(x)$ satisfying Eq. (5) must be of the form

$$\phi(x) = \phi(x) \exp(ik_y y)$$

since $D(x, \underline{k}, \omega)$ has no dependence on y , and we have been assuming $k_{||} = 0$.

We can then write Eq. (5) as

$$\int dk_x \exp(ik_x x) D(x, k_x, \omega) \phi(k_x) = 0$$

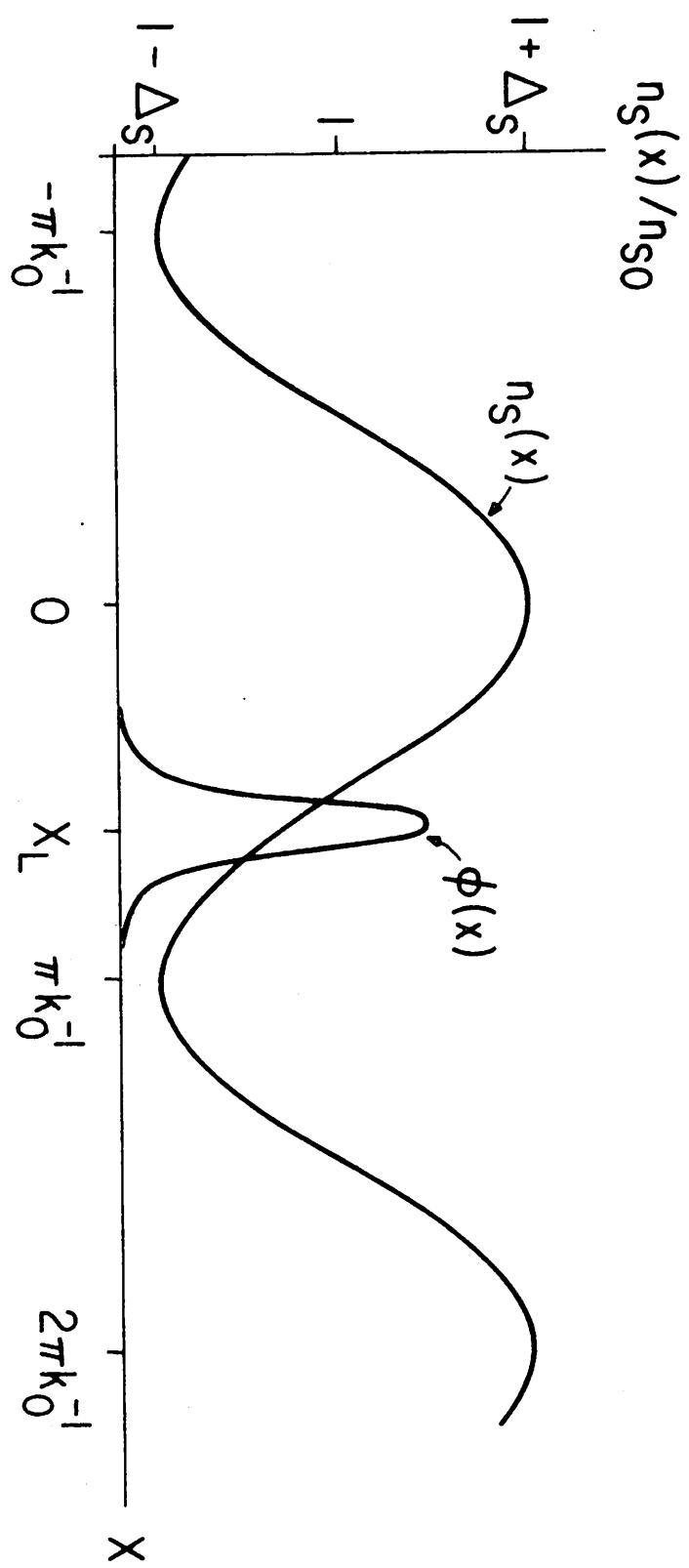


Figure 1. Typical guiding center profile $n_s(x)$ given by Eq.(13), with typical normal mode potential $\phi(x)$

or

$$D(x, -i \frac{\partial}{\partial x}, \omega) \phi(x) = 0 \quad (15)$$

where k_y is understood to be a parameter, and

$$\tilde{\phi}(k_x) \equiv (2\pi)^{-1} \int_{-\infty}^{\infty} dx \phi(x) \exp(-ik_x x)$$

We want to find the normal modes $\phi_n(x)$ and the corresponding frequencies ω_n which satisfy Eq. (15) with appropriate boundary conditions.

A. Local Method

One approach is to expand $D(x, k_x)$ in a power series around some $x = x_L$, $k_x = k_L$, and $\omega = \omega_L$ (all complex, in general) such that

$$D(x_L, k_L, \omega_L) = \frac{\partial D}{\partial x}(x_L, k_L, \omega_L) = \frac{\partial D}{\partial k_x}(x_L, k_L, \omega_L) = 0 \quad (16)$$

(Note that a wave packet localized around x_L , with well-defined wave number k_L , would have a frequency close to ω_L , and would have zero group velocity and acceleration.)

Then

$$\begin{aligned} D(x, k_x, \omega) &= \frac{1}{2} (x - x_L)^2 \frac{\partial^2 D}{\partial x^2} + \frac{1}{2} (k_x - k_L)^2 \frac{\partial^2 D}{\partial k_x^2} \\ &+ (x - x_L) (k_x - k_L) \frac{\partial^2 D}{\partial x \partial k_x} + (\omega - \omega_L) \frac{\partial D}{\partial \omega} + \dots \end{aligned} \quad (17)$$

where the derivatives of D are evaluated at x_L, k_L, ω_L , and Eq. (15) becomes

$$A \frac{d^2 \psi}{dx^2} + Bx \frac{d\psi}{dx} + C x^2 \psi + \lambda \psi = 0 \quad (18)$$

where

$$A \equiv -1/2 \frac{\partial^2 D}{\partial k_x^2}, \quad B \equiv -i \frac{\partial^2 D}{\partial k_x \partial x}, \quad C \equiv 1/2 \frac{\partial^2 D}{\partial x^2},$$

and

$$\lambda \equiv (\omega - \omega_L) \frac{\partial D}{\partial \omega}, \text{ all evaluated at } x_L, k_L, \text{ and } \omega_L;$$

$$\text{and } \psi(x) \equiv \exp(-ik_L x) \phi(x + x_L).$$

This approach is similar to that used by other authors¹⁰⁻¹², who have, however, taken $k_L = 0$ to satisfy Eq. (16), and hence $B = 0$ in Eq. (18). Furthermore, the truncation of Eq. (17) has usually been justified by assuming small Larmor radius compared to scale length, and we wish to emphasize that this assumption is not the only one which will justify Eq. (17).

Taking $\psi(x) \rightarrow 0$ as $x \rightarrow \pm\infty$ as the boundary conditions, Eq. (18) has the solutions (see Appendix E)

$$\psi_n(x) = H_n(\eta^{1/2}x) \exp(-\beta x^2/2) \quad (19a)$$

$$\lambda_n = (2n\eta + \beta)A \quad (19b)$$

where

$$\eta \equiv [(B/2A)^2 - C/A]^{1/2}, \quad \beta \equiv \eta + B/2A,$$

and H_n is the order n Hermite polynomial, $n=0,1,2\dots$. Then

$$\phi_n(x) = H_n[\eta^{1/2}(x-x_L)] \exp(-\beta(x-x_L)^2/2 + ik_L x) \quad (20a)$$

$$\omega_n = \omega_L - (n\eta + \beta/2) \left(\frac{\partial D}{\partial \omega} \right)^{-1} \frac{\partial^2 D}{\partial k_x^2} \quad (20b)$$

A typical normal mode $\phi_n(x)$ for $n=0$ is shown in Fig. 1.

These solutions are valid provided we can neglect the higher derivatives of D in Eq. (17), and provided the Stokes lines of D have the proper

topological behavior in the complex x -plane with respect to the real axis to allow the boundary conditions to be satisfied.¹³ We conjecture that Eq.(20) is a valid solution for the first few modes ($n=0,1,2\dots$) provided (see Appendix F)

$$L(k_L^2 + k_y^2)^{1/2} \gg 1 \quad (21)$$

(where L is the scale length of the plasma) except perhaps for special unusual cases. For instabilities requiring $k_i a_i \gtrsim 1$ (e.g. drift cone¹⁴ or drift cyclotron¹⁵), $a_i \ll L$ is sufficient for inequality (21) to be satisfied, but it is certainly not necessary.

Since ω_n depends linearly on n , the fastest growing mode must be the $n = 0$ mode for some set (x_L, k_L, ω_L) satisfying Eq. (16), or else it cannot be found by the local method at all. [It has turned out in almost every case we have examined for which inequality (21) is satisfied, that the fastest growing mode can in fact be found by the local method using Eqs.(16) and (20), and is thus the $n = 0$ mode, but it is possible to construct models where this will not be true.] The fastest growing mode will then be

$$\phi(x) = \exp[-\beta(x-x_L)^2/2 + ik_L x] \quad (22a)$$

$$\omega = \omega_L - \frac{\beta}{2} \left(\frac{\partial D}{\partial \omega} \right)^{-1} \frac{\partial^2 D}{\partial k_x^2} \approx \omega_L \quad (22b)$$

where we require that x_L, k_L, ω_L satisfy

$$\text{Im} \left[\delta \left(\frac{\partial D}{\partial \omega} \right)^{-1} \frac{\partial^2 D}{\partial k_x^2} \right] > 0$$

as well as Eq. (16).

A large class of solutions (x_L, k_L, ω_L) satisfying Eq. (16) have $k_L = 0$, since this guarantees that $\partial D / \partial k_x = 0$, and it is then only necessary to find x_L and ω_L satisfying $D = 0$ and $\partial D / \partial x = 0$. In this case $\partial^2 D / \partial k_x^2 = 0$, and

$$\delta = \beta = \left(\frac{\partial^2 D}{\partial x^2} / \frac{\partial^2 D}{\partial k_x^2} \right)^{1/2}$$

B. Nonlocal Method

When inequality (21) is not satisfied a different approach is required. We Fourier transform $D(x, k_x, \omega)$

$$D(x, k_x, \omega) = (2\pi)^{-1} \int_{-\infty}^{\infty} dk'' \exp(ik''x) \tilde{D}(k'', k_x, \omega)$$

where

$$\tilde{D}(k'', k_x, \omega) \equiv \int_{-\infty}^{\infty} dx \exp(-ik''x) D(x, k_x, \omega) \quad (23)$$

Putting Eq. (23) into Eq. (15), multiplying by $\exp(-ik'x)$ for arbitrary k' , and integrating over x , we obtain

$$\int dk'' \tilde{D}(k'', k' - k'', \omega) \tilde{\phi}(k' - k'') = 0 \quad (24)$$

for all k' .

For the sinusoidal density profile given by Eq. (13), using Eqs. (6) and (12), Eq. (23) becomes

$$\begin{aligned} \tilde{D}(k'', k_x, \omega) &= G_0(k_x, \omega) \delta(k'') + G_{+1}(k_x, \omega) \delta(k'' - k_0) \\ &\quad + G_{-1}(k_x, \omega) \delta(k'' + k_0) \end{aligned} \quad (25)$$

where

$$G_0 \equiv -k^2 + \sum_s G_{0,s},$$

$$G_{\pm 1} \equiv \sum_s G_{\pm 1,s},$$

$$G_{0,s}(k_x, \omega) \equiv \frac{\omega_{ps}^2}{v_s^2} \exp(-k^2 a_s^2) \sum_\ell I_\ell(k^2 a_s^2) (\omega/\omega_{cs} - \ell)^{-1} \ell$$

$$G_{\pm 1,s}(k_x, \omega) \equiv \frac{\Delta_s \omega_{ps}^2}{2v_s^2} \exp[-(k^2 + k_{\pm 1}^2)a_s^2/2]$$

$$\sum_\ell \exp(i\ell \alpha_{\pm 1}) I_\ell(k^2 a_{\pm 1}^2) (\omega/\omega_{cs} - \ell)^{-1} (\ell \pm ik_y k_0 a_s^2)$$

$$k_{\pm 1}^2 \equiv (k_x \pm k_0)^2 + k_y^2,$$

$a_{\pm 1} \equiv i \log_e \left(\frac{k_x \pm k_0 + ik_y}{k_{\pm 1}} \right) - i \log_e \left(\frac{k_x + ik_y}{k} \right)$ is the angle between k and $k_{\pm 1}$, and

$$\omega_{ps}^2 \equiv 4\pi n_{s0} q_s^2 / m_s.$$

Then the integral in Eq. (24) becomes a discrete sum

$$\begin{aligned} G_0(k', \omega) \tilde{\phi}(k') &+ G_{+1}(k' - k_0, \omega) \tilde{\phi}(k' - k_0) + G_{-1}(k' + k_0, \omega) \\ \tilde{\phi}(k' + k_0) &= 0 \end{aligned} \quad (26)$$

If we require $\phi(x)$ to be periodic with the same periodicity k_0 as the density [appropriate for a simulation with periodic boundary conditions; non-periodic $\phi(x)$ will be considered later], then $\tilde{\phi}(k_x)$ will vanish except at $k_x = pk_0$ for integer p :

$$\tilde{\phi}(k_x) = \sum_{p=-\infty}^{\infty} \phi_p \delta(k_x - pk_0) / 2\pi$$

where

$$\phi_p \equiv (k_0/2\pi) \int_0^{2\pi/k_0} dx \phi(x) \exp(-ipk_0 x)$$

and

$$\phi(x) = \sum_p \phi_p \exp(ipk_0 x) \quad (27)$$

[It should be kept in mind that in general $\phi(x)$ is complex, so there is no relation between ϕ_p and ϕ_{-p} , as there would be if $\phi(x)$ were always real.]

Then, setting $k' = pk_0$, Eq. (26) becomes

$$A_{p,p-1}(\omega)\phi_{p-1} + A_{p,p}(\omega)\phi_p + A_{p,p+1}(\omega)\phi_{p+1} = 0 \quad (28)$$

where

$$A_{p,p'}(\omega) \equiv G_{(p-p')}(p'k_0, \omega).$$

Eq. (28) must be satisfied for all integers p , since Eqs. (24) and (26) are satisfied for arbitrary k' . So, we require

$$\det A_{p,p}(\omega) = 0 \quad (29)$$

If, for the modes we are interested in, ϕ_p is negligibly small for all $p \geq p_{\max}$, and all $p \leq p_{\min}$ for some finite p_{\max} and p_{\min} , then we can truncate the matrix $A_{p,p}$, at $p > p_{\max}$ and $p < p_{\min}$. We can then solve Eq. (29) to find the normal mode frequencies ω (in general there will be $p_{\max} - p_{\min} + 1$ of them for each cyclotron harmonic), use Eq. (28) to find the ϕ_p for each normal mode, and then use Eq. (27) to find $\phi(x)$.

This method is easily generalized to periodic density profiles $n_s(x)$ other than the sinusoidal profile given by Eq. (13). For

$$n_s(x) = \sum_{j=-\infty}^{\infty} n_{s,j} \exp(ijk_0 x) \quad (30)$$

Eq. (25) becomes

$$\tilde{D}(k'', k_x, \omega) = \sum_{j=-\infty}^{\infty} G_j(k_x, \omega) \delta(k'' - jk_0) \quad (31)$$

with G_j defined like $G_{\pm 1}$ in Eq. (25) but with $\Delta_s/2$ replaced by

$n_{s,j}/n_{s0}$, and $\pm k_0$ replaced by $+ jk_0$. Eq. (28) then becomes

$$\sum_{p'} A_{p,p'} \phi_{p'} = 0$$

which again leads to Eq. (29). The advantage in using a sinusoidal density profile is that the matrix $A_{p,p'}$ is tri-diagonal, and Eq. (29) is easier to solve numerically than it would be for an arbitrary matrix. Adding terms with $2k_0$, for example, would result in a penta-diagonal matrix. On the other hand, an isolated slab of plasma with $a_i/L \sim 1$ would be more realistically modelled by a periodic density profile including higher harmonics of k_0 .

It is also not difficult to generalize this method to potentials $\phi(x)$ which are not periodic in x . It can be shown using Floquet's theorem that, except for a measure zero subset of the parameter space, all normal mode potentials must be of the form (see Appendix G)

$$\phi(x) = \exp(iKx) \sum_p \phi_p \exp(ipk_0 x) \quad (32)$$

for some K , $0 < K < k_0$. Then we can still use Eqs. (28) and (29), but we must redefine $A_{p,p'}$, as

$$A_{p,p'}(\omega) \equiv G_{(p-p')}(p'k_0 + K, \omega) \quad (33)$$

The nonlocal method will only be practical if we can use $p_{\max} - p_{\min}$ not too large; otherwise the numerical solution of Eq. (29) will be too difficult. In order to estimate the conditions under which the nonlocal method is practical, we will temporarily assume that inequality

(21) is at least marginally satisfied, so that Eq. (20a) is at least qualitatively correct for the fastest growing mode. Then, using the definition of ϕ_p in Eq. (27), we find

$$\phi_p \propto \exp[-(pk_0 - k_L)^2/2\beta - ik_0 x_L]$$

so we must choose $p_{\max} - p_{\min}$ to be at least a few times $|\beta|^{1/2} k_0^{-1}$. We estimate that β is on the order of $k_0^{1/2} (k_L^2 + k_y^2)$ from the definitions following Eqs. (18) and (19), since the scale length of D in x will be about k_0^{-1} , while the "scale length" of D in k_x will be about $(k_L^2 + k_y^2)^{1/2}$, and we can estimate the relative magnitudes of the various second derivatives of D from these scale lengths. It then follows that

$$p_{\max} - p_{\min} \gtrsim k_0^{-1} (k_L^2 + k_y^2)^{1/2} \quad (34)$$

and we need $p_{\max} - p_{\min} \gg 1$ if inequality (21) is satisfied. So the nonlocal method is not a practical way to find the fastest growing mode in those cases where the local method is valid, whereas it is practical when the local method is marginally valid. We cannot say in general whether the nonlocal method is practical when inequality (21) is not even marginally satisfied. However, in all such cases which we have investigated numerically, $p_{\max} - p_{\min}$ can be chosen small (of order unity). Thus the local and nonlocal methods complement each other; each method works best in the regime where the other method is least efficient or least valid.

IV. Numerical Techniques

To find the normal modes and frequencies using the nonlocal method, the roots of Eq. (29) were found numerically in the region of interest of the complex ω plane, using a standard root-finding routine^{16,17}

(modified by the authors) based on Muller's method.¹⁸ Usually a small value of $k_y a_i$ (typically 0.5) was used initially, since the root-finder was most efficient near the real axis (rarely missing roots with $\text{Im } \omega/\omega_{ci} \lesssim 1$) and at small $k_y a_i$ the roots tended to be near the real axis. Then each root found at the initial $k_y a_i$ was followed out to larger $k_y a_i$; in this way it was possible to find roots far from the real axis at large $k_y a_i$, which the root-finder would very likely miss if $k_y a_i$ were large initially. For each root found, the eigenvector $(\phi_{p\min}, \dots, \phi_{p\max})$ was calculated from Eq. (28), and $\phi(x)$ [from Eq. (27)] was plotted out if desired. In practice p_{\min} was always set equal to $-p_{\max}$, since the matrix elements $A_{p,p'}$ for $p,p' < 0$ could be found using the identity $A_{p,p'} = A_{-p',-p}$ [following from the definitions of $A_{p,p'}$ and $G_0, G_{\pm 1}$ after Eqs. (28) and (25)]; thus little time would be saved by using $|p_{\min}| \neq |p_{\max}|$ if $p_{\min} < 0 < p_{\max}$. (Some time would be saved by using $|p_{\min}| < |p_{\max}|$ to find modes with $\phi_{-p_{\max}} \ll \phi_{p_{\max}}$.)

Since the time required to calculate $\det A_{p,p'}$ is proportional to p_{\max} , and the number of roots is proportional to p_{\max} , the time required to find all the roots in a given range of k_y and ω was roughly proportional to p_{\max}^2 . A typical run for a loss cone deuterium plasma with $\omega_{pe} \approx \omega_{ce}$ and $k_0 a_i \approx 1$, in the range of k_y and ω typical of the drift cone instability ($0.5 \leq k_y a_i \leq 20$, $|\omega|/\omega_{ci} < 2.5$ at $k_y a_i = 0.5$), using $p_{\max} = 3$, took one minute on the CDC 7600 computer. However, for $p_{\max} \gtrsim 5$ the roots were so close together, especially near the cyclotron harmonics, that the root finder could not find many of them. In order to avoid this problem and to reduce the computation time, an approximation was sometimes employed in which the asymptotic form for the Bessel function¹⁹

$$e^{-x} I_\ell(x) \approx (2\pi x)^{-1/2} \exp(-\ell^2/2x), (x \gg \ell \gg 1)$$

was used, and the sum over ℓ replaced by an integral, for the ion terms. Then the definitions after Eq. (25) become, for the ion terms (see Appendix H

$$G_{0,s}(k_x, \omega) = -(\omega_{ps}^2 / v_s^2) [1 + \zeta_0 Z(\zeta_0)]$$

$$G_{\pm 1,s}(k_x, \omega) = -(\omega_{ps}^2 \Delta_s^2 / 2v_s^2) \exp(-k_0^2 a_s^2 / 2) [1 + \zeta_{\pm 1} Z(\zeta_{\pm 1})]$$

(35)

where

$$\zeta_0 \equiv \omega / (\sqrt{2} k v_s)$$

$$\zeta_{\pm 1} \equiv (\omega \pm ik_0 a_s v_s) / (\sqrt{2} k v_s)$$

and $Z(\zeta)$ is the usual plasma dispersion function²⁰

$$Z(\zeta) \equiv \pi^{-1/2} \int dt \exp(-t^2)/(t-\zeta)$$

This approximation is valid when $\text{Im } \omega \gtrsim \omega_{ci}$, $ka_i \gtrsim 1$, and $k_0 \lesssim k$, and is equivalent to using straight line orbits for the ions when integrating the Vlasov equation over the zero-order orbits. When this approximation is used, the modes associated with the ion cyclotron harmonics (Bernstein waves) are eliminated, allowing higher p_{max} to be used without confusing the root-finder (no problems were encountered up to $p_{max} = 9$, as long as the $Z(\zeta)$ routine had high enough precision) and greatly reducing the computation time for a given p_{max} (typically by a factor of 10).

The electron terms were evaluated in the limit of zero Larmor radius, $ka_e \ll 1$:

$$G_{0,e}(k_x, \omega) = -\omega_{pe}^2 k^2 / (\omega_{ce}^2 - \omega^2)$$

$$G_{\pm 1,e}(k_x, \omega) = -(\omega_{pe}^2 \Delta_e / 2) [k k_{\pm 1} / (\omega_{ce}^2 - \omega^2) \pm i k_0 k_y / |\omega_{ce}| \omega] \quad (36)$$

and Δ_e was related to Δ_i (usually set equal to 0.99) by Eq. (14a), so

$$\Delta_e = \Delta_i \sum_{s = \text{ions}} (n_s / n_e) \exp(-k_0^2 a_s^2 / 2) \quad (37)$$

where the sum is over ion species [recall that a loss cone ion distribution, given by Eq. (11), is treated as two Maxwellian ion species].

Numerical solutions were obtained using the local method also. The first two parts of Eq. (16), $D = 0$, and $\partial D / \partial x = 0$, were solved simultaneously for complex ω_L and x_L , using a Newton-Raphson²¹ root finder (k_L was assumed to be zero, so that $\partial D / \partial k_x = 0$ was always satisfied). This root-finder (in contrast to the root-finder used for the nonlocal method) worked well only when the initial values of ω_L and x_L were reasonably close to the correct values. Initial values were taken either from the results of the nonlocal method, or from previous calculations of ω_L and x_L using slightly different parameters. Because the root-finder was very quick, and the equations to be solved were relatively simple, it was possible to cover the parameter space fairly densely, using the local method. In fact the entire parameter space could be covered in less time using the local method than it took to solve a single case using the nonlocal method, and the results were more accurate using the local method when inequality (21) was well-satisfied. On the other hand, the nonlocal method was needed to obtain initial values of ω_L and x_L in a given regime of parameter space, as well as to find modes with $k_L \neq 0$, and modes with inequality (21) not satisfied.

Abridged flow charts and complete listings for the program ROOTS and its subroutines (used for the nonlocal method) and of the program LOCAL and its subroutines (used for the local method) are given in Appendix I.

V. Results

Runs were made for both methods using a mirror ratio $R = 3$, a mass ratio $m_i/m_e = 3700$ (appropriate for a deuterium plasma), a density gradient $k_0 a_i$ ranging from 0.1 to 6.3 [a_i refers to v_i/ω_{ci} where v_i is the thermal velocity of the first Maxwellian component in Eq. (11); the total ion thermal velocity is thus $v_i(1+R^{-1})^{1/2}$], and density $\omega_{pi}^2/\omega_{ci}^2$ ranging from 3 to 10^4 . In each case, for the mode with the highest growth rate, ω and k_y were found and $\phi(x,y)$ was plotted. Sample results using the nonlocal method for one case, $\omega_{pi}^2/\omega_{ci}^2 = 30$, $k_0 a_i = 1.13$, and $p_{max} = 3$, are shown in Fig. 2, a plot of ω vs. k_y , (note that there are $p_{max} - p_{min} + 1 = 7$ branches for each cyclotron harmonic in Fig. 2, as discussed in Sec. II B.) and Fig. 3, a contour plot of $\phi(x,y)$. When inequality (21) was satisfied and when p_{max} was high enough so that $\phi_p \approx 0$ for $|p| \geq p_{max}$, the results using each of the two methods were found to be in excellent agreement, within 1% for ω, k_y , and x_L , and within 10% for the half-width of $\phi(x)$. (see Appendix J)

Figure 4 shows the growth rate of the fastest growing mode as a function of $\omega_{pi}^2/\omega_{ci}^2$ and $k_0 a_i$, using either the local or the nonlocal results, whichever was most accurate for each set of parameters. Figure 5 shows the minimum p_{max} needed in order to use the nonlocal method, as a function of $\omega_{pi}^2/\omega_{ci}^2$ and $k_0 a_i$. Figure 6 shows $|\phi(x)|^2$ and $|\phi_p|^2$ for various values of $k_0 a_i$, for $\omega_{pi}^2/\omega_{ci}^2 = 1000$.

VI. Interpretation

The parameter space is divided into several regimes in each of which the fastest growing mode has qualitatively different characteristics (shown in Fig. 7) and is driven unstable by a different mechanism.

At $k_0 a_i < 1.25$ (region A in Fig. 7), the most unstable mode is a drift cone mode. Its characteristics are in qualitative agreement with

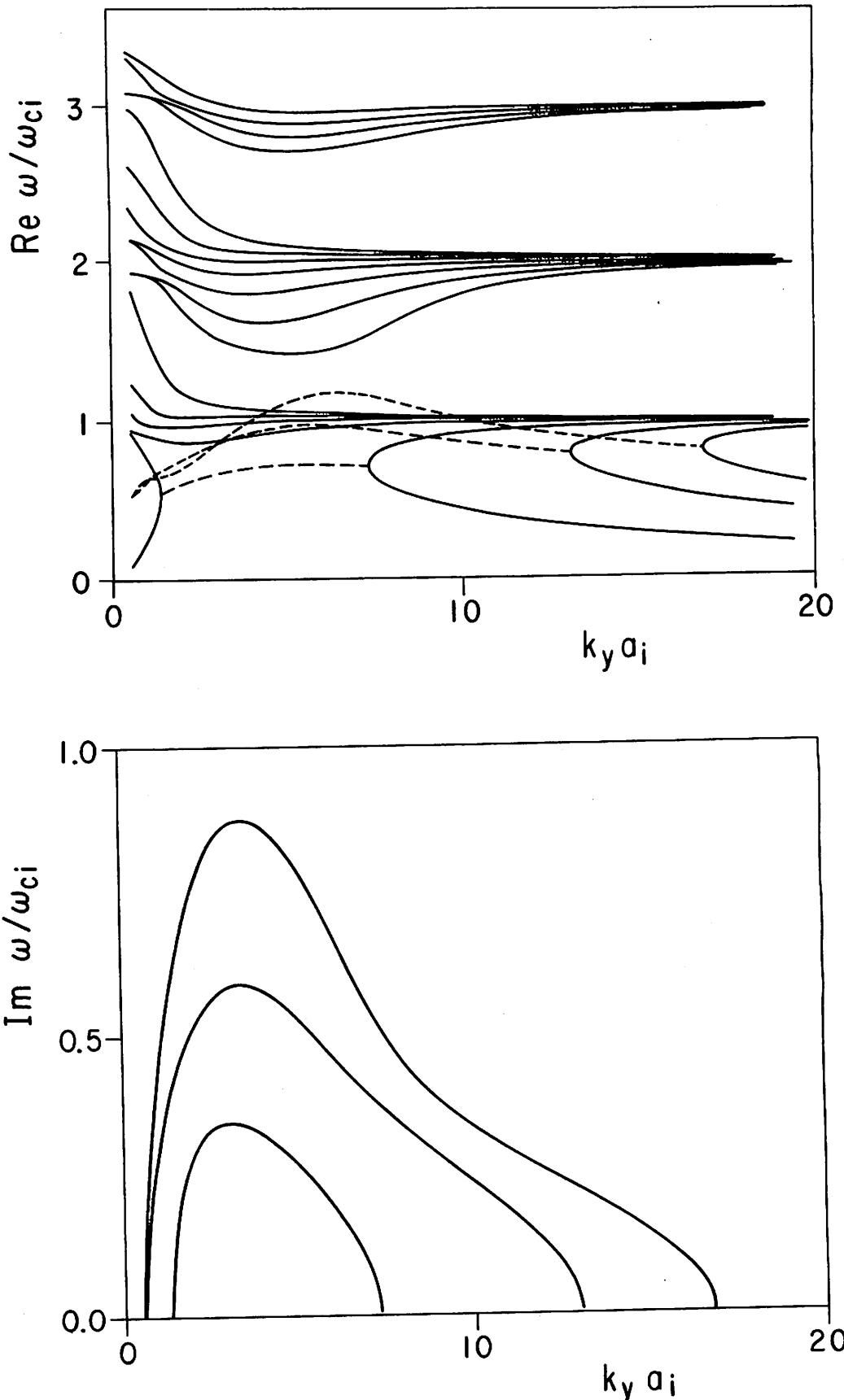


Figure 2. ω vs. k_y plot, using $\omega_{pi}^2/\omega_{ci}^2 = 30$, $m_i/m_e = 3700$, $R = 3$, $k_o a_i = 1.13$, $\Delta_i = 0.99$, $p_{max} = 3$. The real part of ω is shown in the top plot (dashed curves indicate the real parts of complex ω) and the imaginary part of ω (the growth rate) in the bottom plot.

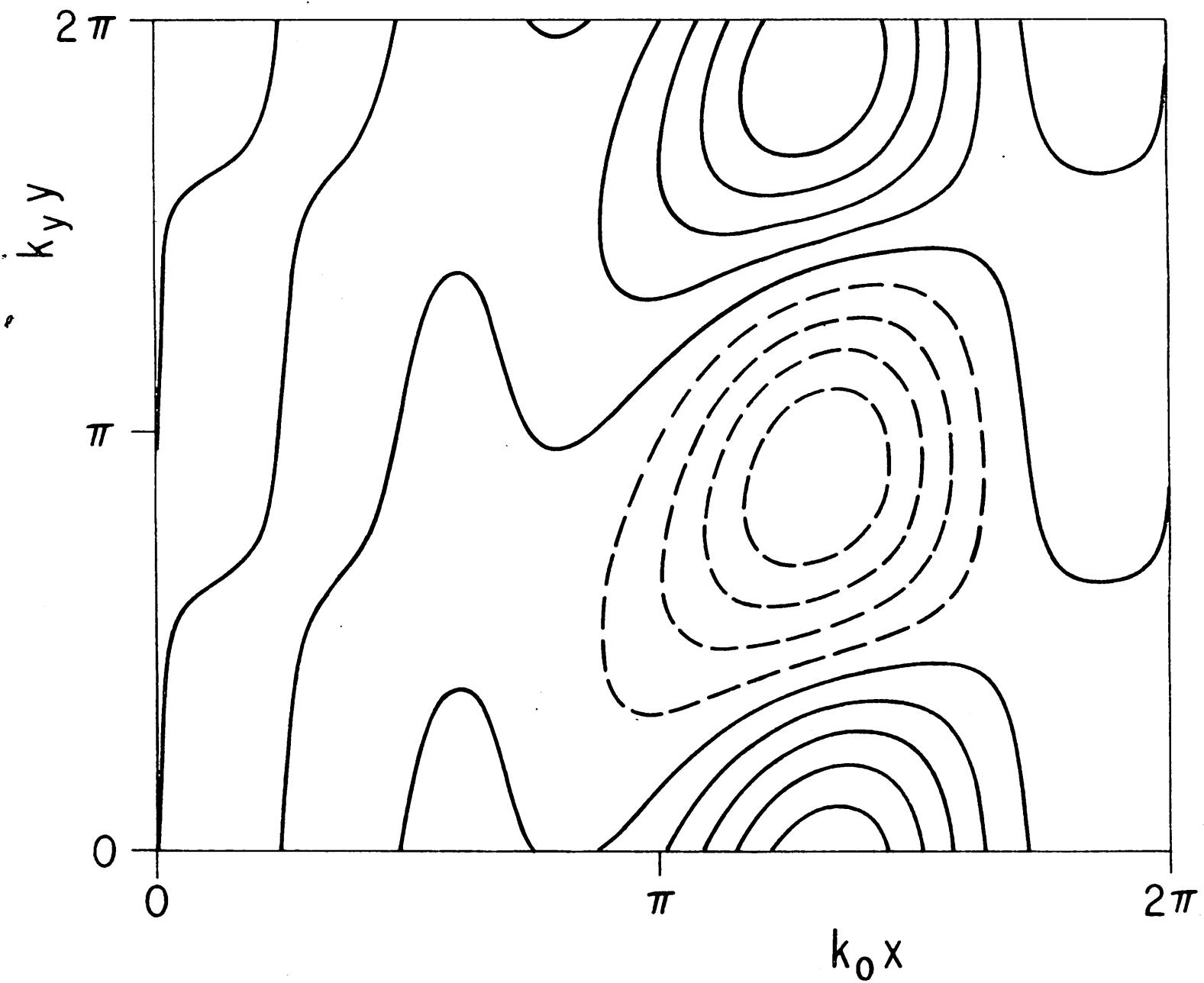


Figure 3. Contour plot of the real part of $\phi(x,y)$ for the fastest growing mode in Fig. 2, at $\omega/\omega_{ci} = 0.953 + 0.873i$, $k_y a_i = 3.55$. The plasma density is at a maximum at $k_0 x = 0$ and 2π , and at a minimum at $k_0 x = \pi$. $\text{Re } \phi(x,y)$ is normalized so that it ranges from -1 to +1. Contours are shown for 0.8, 0.6, 0.4, 0.2, and 0 (solid curves) and for -0.2, -0.4, -0.6, and -0.8. The figure would have to be compressed vertically by a factor of 2.56 to make the vertical and horizontal scales the same.

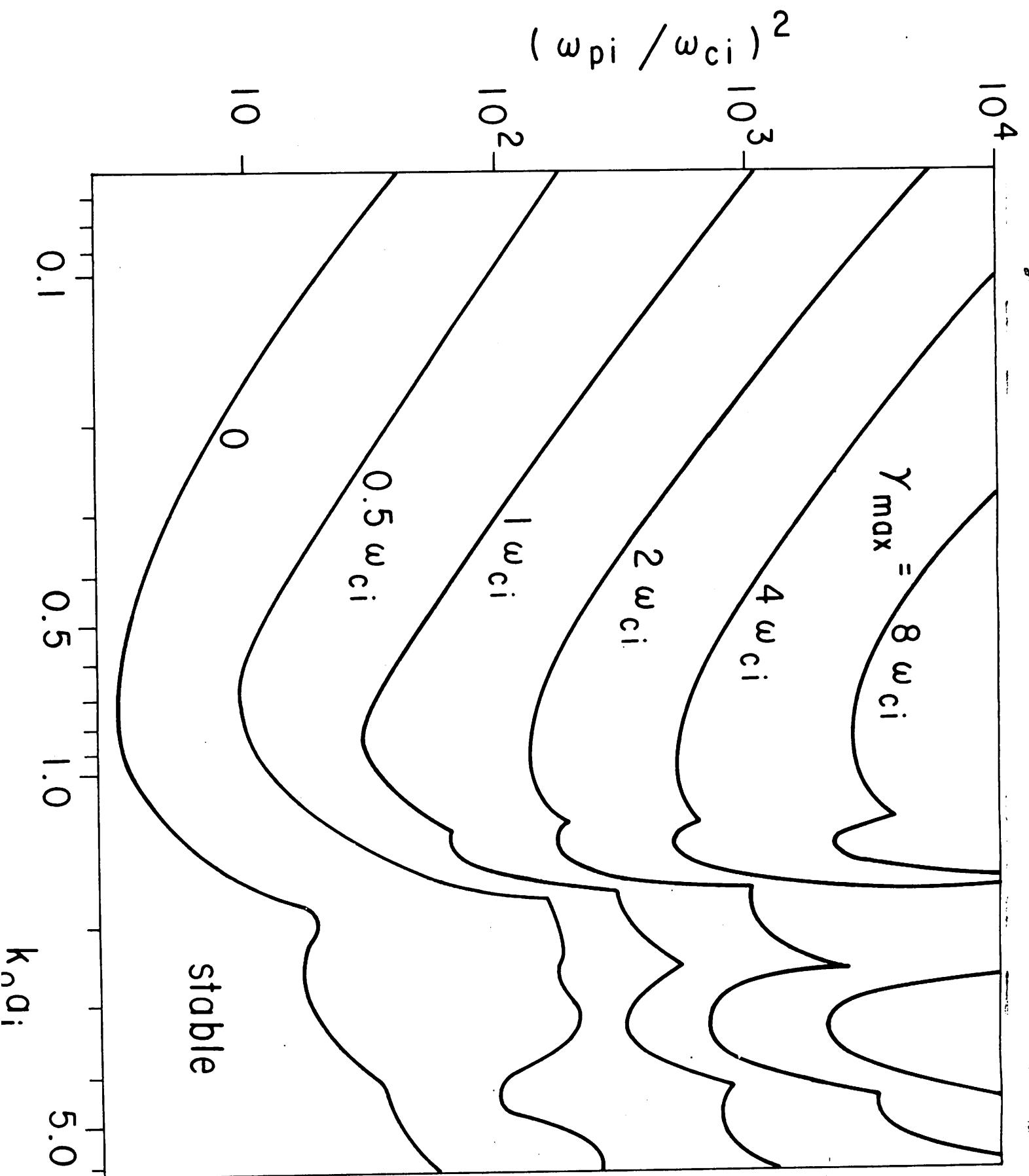


Figure 4. The growth rate γ_{\max} of the fastest growing mode is shown as a function of $(\omega_{pi}/\omega_{ci})^2$ and $k_0 a_i$, for $\Delta_1 = 0.99$, $R = 3$, $m_i/m_e = 3700$.

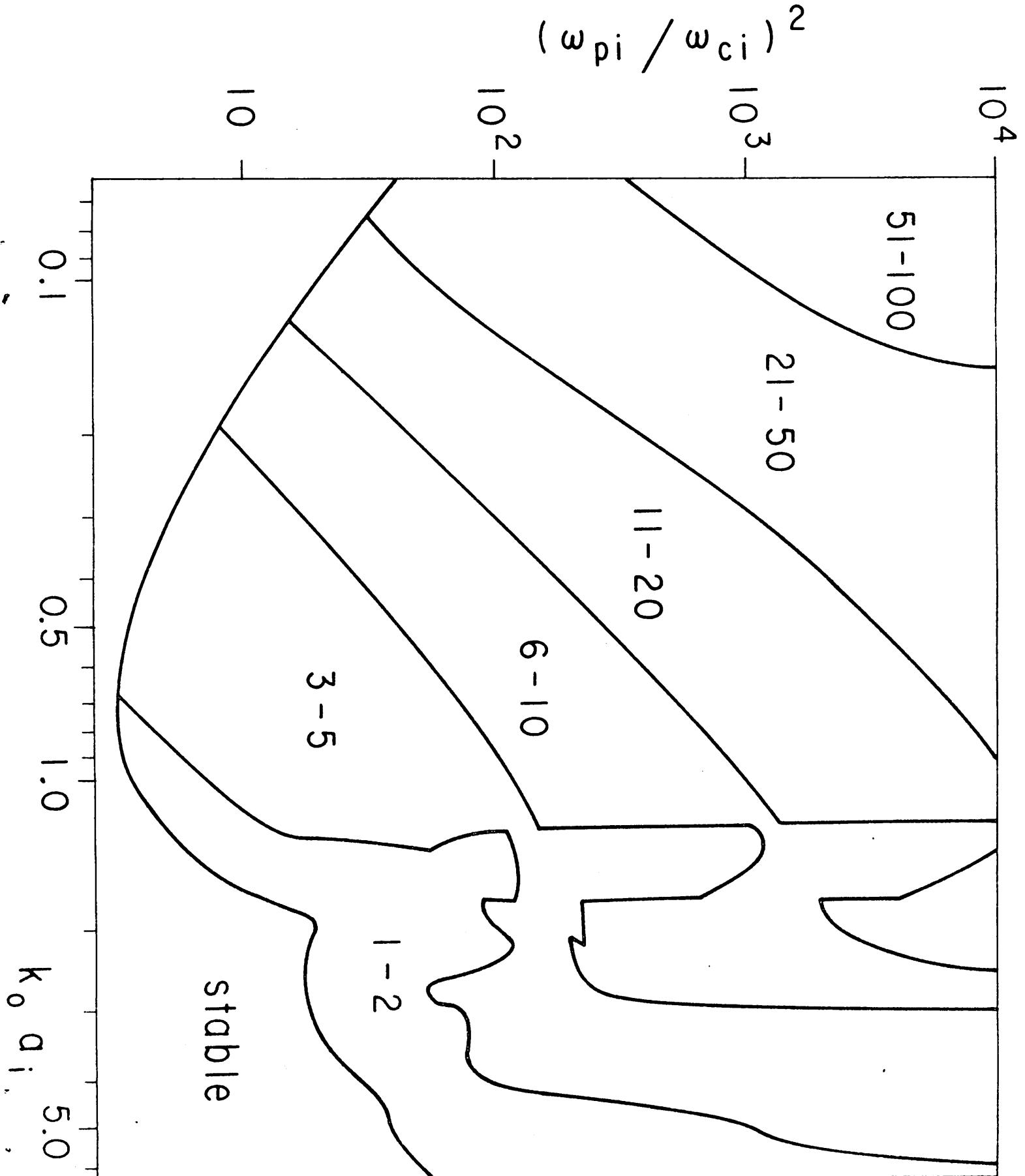


Figure 5. The minimum p_{max} needed to find the fastest growing mode using the nonlocal method is shown as a function of $(\omega_{pi}/\omega_{ci})^2$ and $k_o a_i$, for $\Delta_i = 0.99$, $R = 3$, $m_i/m_e = 3700$.

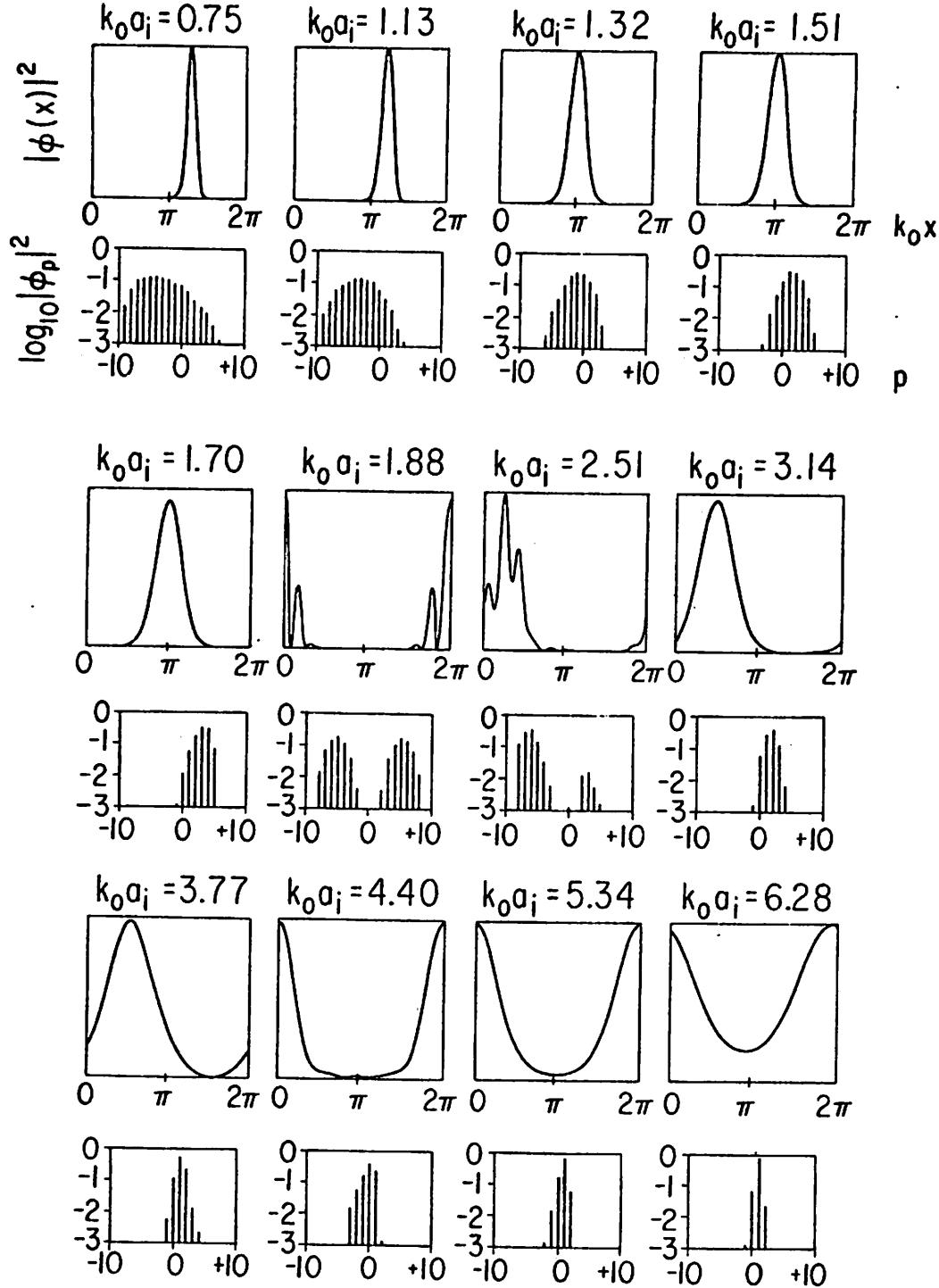


Figure 6. $|\phi(x)|^2$ and $|\phi_p|^2$ are shown for the fastest growing mode for various values of $k_0 a_i$, using $(\omega_{pi}/\omega_{ci})^2 = 1000$, $\Delta_i = 0.99$, $R = 3$, and $m_i/m_e = 3700$. The plasma guiding center density is at a maximum at $k_0 x = 0$ and 2π , and at a minimum at $k_0 x = \pi$. For $k_0 a_i > 1.80$, the plasma density (as opposed to guiding center density) has its maximum at $k_0 x = \pi$, and its minimum at $k_0 x = 0$ and 2π . The twelve cases shown are located respectively in regions A, A, B, B, B, C, D, E, E, F, F, and G of Fig. 7.

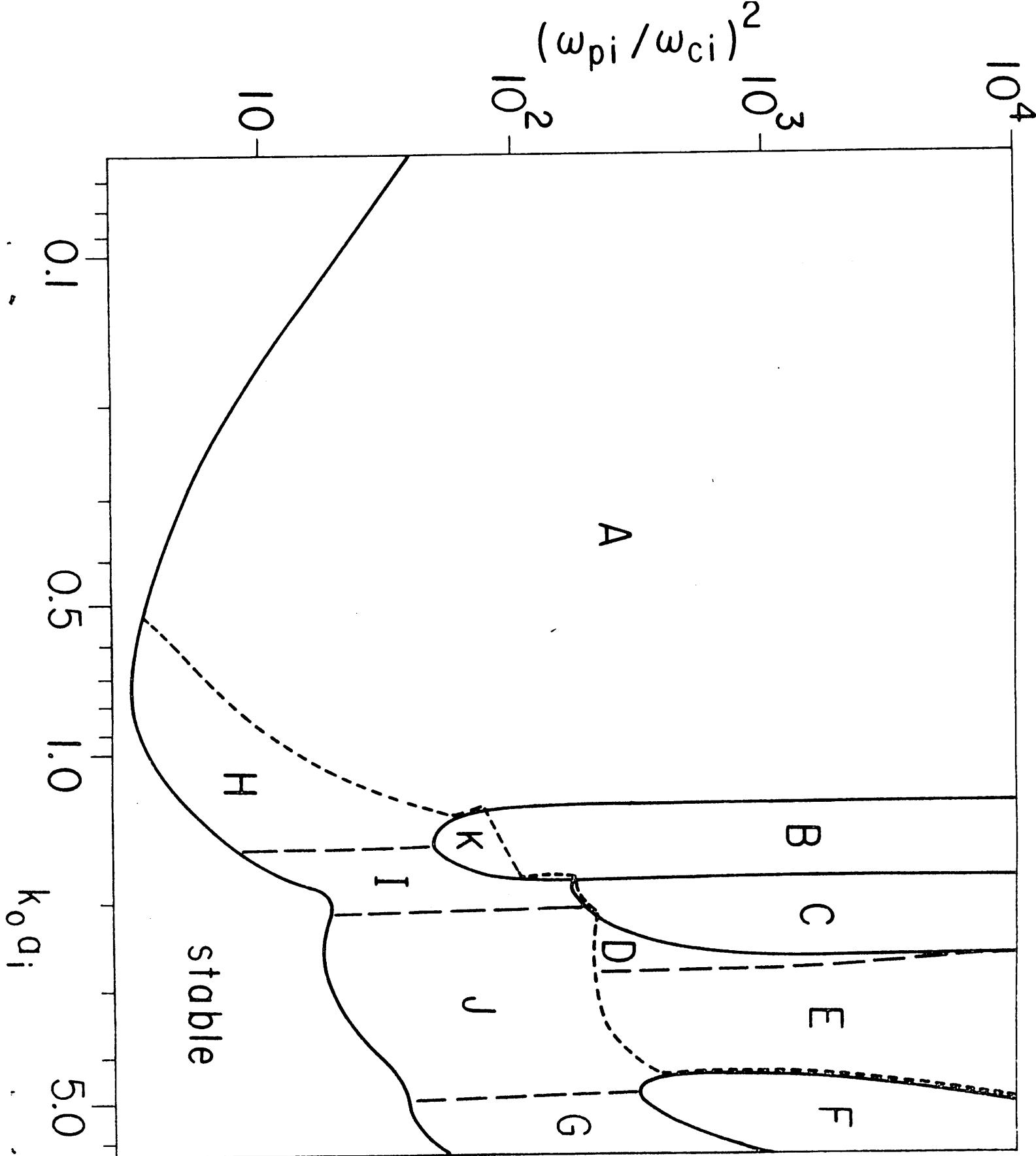


Figure 7. Regions of the parameter space are shown in which the fastest growing mode has different characteristics. The usual drift cone mode occurs in region A; other types of instabilities occur in the other regions, discussed in Sec. VI. $R = 3$, $\Delta_i = 0.99$, $m_i/m_e = 3700$.

the mode described by Post and Rosenbluth¹⁴ for an infinite medium with constant density gradient; it is modified by the fact that $\phi(x)$ is centered near the edge of the plasma (typically $k_0 x_L / 2\pi \approx 0.6$) where the density gradient $(a_i/n)dn/dx$ (a small parameter in Ref. 14) is relatively large. For $k_0 a_i \gtrsim 0.4$, the ion density gradient begins to compete with the loss cone as a source of free energy for the instability, and the mode has some of the characteristics of the Mikhailovskii drift cyclotron instability¹⁵.

At $k_0 a_i > 1.25$ and $\omega_{pi}^2/\omega_{ci}^2 \gtrsim 50$ (region B in Fig. 7), a new mode appears, and quickly becomes more unstable than the drift cone mode. This mode has $\phi(x)$ centered at $k_0 x/2\pi = 0.5$ (the point of minimum ion guiding center density), and has a purely imaginary frequency. It is an ion two-stream instability, driven by the double-humped ion velocity distribution $f_{0i}(x,y)$ at $k_0 x/2\pi = 0.5$ [since $n_i(x)$ is double-humped, and $f_{0i}(x,y) = g_i(v_\perp, v_\parallel) n_i(x_{gc})$]. It is thus an artifact of the periodic guiding center density profile $n_i(x)$, and would not appear in a plasma with a single-humped density profile.

The ion-two-stream instability is most unstable at $k_0 a_i \approx 1.35$, and disappears at $k_0 a_i > 1.80$. The drift cone (or drift cyclotron) instability also disappears at about this value of $k_0 a_i$, since $\Delta_e = 0$ at $k_0 a_i = 1.80$ for $R=3$ [in order to satisfy Eq.(14b)], and the drift cone mode depends on an electron density gradient. But for $\omega_{pi}^2/\omega_{ci}^2 \gtrsim 200$, another instability appears at $k_0 a_i \approx 1.70$, and remains the most unstable mode until $k_0 a_i \approx 2.5$ (region C of Fig. 7). This mode has $\phi(x)$ centered at $k_0 x/2\pi = 0$, the point of maximum ion guiding center density, and is a purely growing ion instability, with $k_L \gtrsim k_y$; the maximum growth rate occurs when $k_y = 0$. The instability arises because the projection of the ion

velocity distribution in the x -direction $\int f_{0i}(x, v) dv_y dv_z$, has its loss cone deepened slightly when $d^2 n_i / dx^2 < 0$ (true at $x = 0$), and this makes the ion distribution unstable by the Penrose criterion²² to modes with wave vector in the x -direction. Eq. (16) can be solved analytically in the limits $k_y = 0$, $\text{Re } \omega_L = 0$, $k_L v_i \gtrsim |\omega_L| \gtrsim \omega_{ci}$, which are applicable in region C when $\omega_{pi} \gg \omega_{ci}$. In these limits, $D(x, k_x, \omega)$ can be written in terms of the plasma dispersion function $Z(\zeta)$, using Eqs. (11), (23), (25), and (35), and $Z(\zeta)$ can be approximated by $i\pi^{1/2}$, since $\zeta = \omega_L / k_L v_i \ll 1$.²⁰ Then Eq. (16) has the solutions (see Appendix K)

$$\begin{aligned}\omega_L &= 0.307 i \omega_{lh} (1-R^{-1})^{-1/2} (e_2 - e_1)^{3/2} [R^{1/2} (e_2 + 1) - (e_1 + 1)]^{-1} \\ k_L &= 0.577 (\omega_{lh} / v_i) (1-R^{-1})^{-1/2} (e_2 - e_1)^{1/2} \\ x_L &= 0\end{aligned}\tag{38}$$

where

$$e_1 \equiv \exp(-k_0^2 a_i^2 / 2), \quad e_2 \equiv \exp(-k_0^2 a_i^2 / 2R),$$

and

$$\omega_{lh} \equiv \omega_{pi} [1 + \omega_{pe}^2 (1 + \Delta_e) / \omega_{ce}^2]^{-1/2}$$

is the lower hybrid frequency at $x = 0$,

and $\Delta_e = (R e_1 - e_2) / (R - 1)$ from Eq. (14a) assuming $\Delta_i = 1$. The growth rate is greatest for a given ω_{lh} when $k_0 a_i = [2R \ln R / (R-1)]^{1/2}$. For $R = 3$, this corresponds to $k_0 a_i = 1.80$, and Eq. (38) gives $\omega_L = 0.06 i \omega_{lh}$ and $k_L / k_0 = 0.27 \omega_{lh} / \omega_{ci}$. Since Eq. (38) is derived using the local method and depends on inequality (21) for validity, we might expect that this mode will no longer exist when $\omega_{pi}^2 / \omega_{ci}^2 \lesssim 200$, since then $k_L / k_0 < 2$. The nonlocal method confirms this expectation and gives results in good agreement with Eq. (38) when $\omega_{pi}^2 / \omega_{ci}^2 > 200$ and $1.80 < k_0 a_i < 2.5$.

Since the mechanism for this instability is the deepening of the loss cone due to $d^2 n/dx^2 < 0$, it does not depend on the periodic nature of the density profile, and we would expect it to occur even in an isolated slab of plasma. However, it would not occur in a plasma column with cylindrical symmetry; this may be seen by applying the Penrose criterion²² at $x = 0$ to a plasma with distribution function $f_{0i}(x, y) = g_i(v_\perp, v_\parallel, x_{gc})$ given by Eq. (11), and $n_i(x) = n_0 \exp(-x^2/L - y^2/L)$. Hence the instability of region C, like that of region B, is an artifact of the model density profile used. (see Appendix L)

When $k_0 a_i > 1.80$, $\Delta_e < 0$ (for $R = 3$), i.e. the electron density gradient is in the opposite direction of the ion guiding center density gradient, and a drift cone or drift cyclotron instability occurs with $\phi(x)$ centered at $0 < k_0 x/2\pi < 0.5$, rather than at $0.5 < k_0 x/2\pi < 1.0$, as occurs when $\Delta_e > 0$. This instability has higher growth rate than any of the purely growing ion instabilities when $2.5 \geq k_0 a_i \geq 4.0$ (regions D and E). At $k_0 a_i \approx 2.5$ (region D) finite $k_L \sim k_y$ must be used in Eq. (16) to describe the fastest growing mode by the local method, but at $k_0 a_i > 2.5$ (region E) $k_L = 0$ may be used. The ion density gradient is more important than the loss cone in driving this instability, but the loss cone is crucial in determining the electron density gradient Δ_e (which would be positive and much smaller in absolute value if there were no loss cone), on which the real part of the frequency (and indirectly the growth rate) depends.

For $k_0 a_i \geq 4.0$, the electron density gradient is unimportant because Δ_e (which decreases exponentially with $k_0 a_i$) is negligibly small. Ion instabilities of the two-stream (or many-stream) type again become important (for $\omega_{pi}^2/\omega_{ci}^2 \geq 50$), driven by the ion density profile [which for $k_0 a_i \gg 1$ results in $f_{0i}(v_y)$ consisting of several

streams], and by the loss cone. These instabilities are purely growing at higher densities and lower $k_0 a_i$ (region F). At lower densities and higher $k_0 a_i$, when ion cyclotron effects (i.e. $\text{Im } \omega \leq \omega_{ci}$) become important, the real frequencies are not zero (region G). Because $f_{0s}(x, y)$ is not very dependent on x when $k_0 a_i \gg 1$, these modes tend to have $\phi(x)$ very spread out in x , with $k_y \approx k_x \approx k_0$. Hence they cannot be described by the local method, only by the nonlocal method.

Fastest-growing modes which cannot be described by the local method also exist at lower $k_0 a_i$, at sufficiently low densities (regions H, I, J, K). For regions H, I, and J, $\text{Re } \omega \neq 0$; in region K, $\text{Re } \omega = 0$. In regions I and K, like regions G and F, the instability is due entirely to the ions, and the electron density gradient (which is very small in these regions) plays no role. In regions H and J, the electron density gradient is important, and both the ions and electrons contribute to the mode. This may be seen by comparing the perturbed ion and electron densities for the fastest-growing mode in the different regions. In regions F, G, I, and K, the perturbed ion density is much greater, while in regions H and J, the perturbed ion and electron densities are comparable.

VII. Summary and Conclusions

Two methods were derived for finding the linear normal modes of electrostatic perturbations in a non-uniform Vlasov plasma. The methods complement each other, since the local method, using Eqs. (16) and (22) is valid only when the wavelength is much smaller than the scale length, while the nonlocal method, using Eqs. (27), (28), and (29), is most efficient when the wavelength is comparable to the scale length. Neither method depends on the Larmor radius being small compared to the scale length. Both methods were employed (each in its own regime of validity)

to find the normal modes for the drift cone and related instabilities in a loss cone plasma with density varying sinusoidally in space in a direction perpendicular to a uniform magnetic field, over a wide range of densities and density gradients.

An immediate application of these results is to computer simulations of the drift cone mode using periodic boundary conditions and a slab geometry, with sinusoidal density profile. Analytic solutions for the linear normal modes and frequencies for this model are useful in order to check the linear behavior of the simulation, before we explore the nonlinear behavior. Such simulations should have $k_0 a_1 < 1.25$; otherwise we will introduce new instabilities that depend on the model, and would not occur in a cylindrical plasma column, for example, as discussed in Sec. VI.

If other models (including more realistic models of experiments) behave in a similar fashion to the model we have considered, then no qualitatively new behavior (not predicted by the small Larmor radius approximation) would occur if $(a_1/n) dn/dx < 1$. The condition is satisfied for the bulk of the plasma in the 2XIIIB experiment.³

More generally, we have shown that it is possible to use a local method to find the normal modes and their growth rates, even when the Larmor radius is comparable to the scale length, provided the wavelength is much less than the scale length [and assuming we can find the equilibrium distribution $f_{0s}(x, y)$]. When the wavelength is comparable to the scale length, it is possible to use a matrix equation (not tri-diagonal in general) truncated at fairly low index p. Although the model we have solved does not resemble any experiment, it should be possible to use these methods to find the normal modes of experimental plasmas with Larmor radius comparable to scale length.

Historical Note

This report is the culmination of many years of work.

In 1969, Birdsall and Fuss (at Lawrence Livermore Lab.) began computer simulation of the drift-cyclotron loss-cone mode, using particles on a two-dimensional periodic mesh, starting with a sinusoidal density profile [Eq.(13) with $\Delta_i \approx 1$, $k_0 a_i / 2\pi \approx 0.1, 0.2$]. The checks between simulation and small-amplitude dispersion results (ω, k), calculated by N. Lindgren (Univ. of Calif., Berkeley) from existing local approximation theory¹⁴, were fair, considering the difference in the model and theory.

Langdon (Univ. of Calif., Berkeley) then provided the exact or nonlocal theory, essentially Eq.(29), from which Birdsall and Fuss obtained a few sample solutions for ω, k (showing the multiple roots, as in Fig. 2) and $\phi(x, y)$ (showing the localization, as in Fig. 3), and these only for a ring distribution of velocities,

$$g_{i\perp}(v_\perp, x) = (2\pi v_0)^{-1} \delta(v_\perp - v_0) n_i(x),$$

rather than the loss cone distribution given by Eq.(11). While these results were presented in talks^{4,5} and progress reports, they were incomplete.

Since 1973, Gerver derived the local method [eqs.(16) and (20)], and used these and the nonlocal dispersion relation, Eq.(29), with loss cone distributions of the form given by Eq.(11), to explore the broad range of parameters displayed in Fig. 4 through 7. This required considerable refinement of the numerical techniques used earlier, including the use of straight-line orbits [Eq.(35)], and extensive modifications of the root-finding routine. The physical identification of the various modes and the interpretations are also Gerver's.

Acknowledgments

We wish to express our appreciation to A.N. Kaufman and W.B. Kunkel for helpful discussions and suggestions, and to Richard Meyers for help in debugging the computer programs.

APPENDIX A

Derivation of Eq. (4):

Starting with Eq. (3) and the identities

$$\begin{aligned}\phi(\underline{x}_s', t) &= \int d\underline{k} \tilde{\phi}(\underline{k}) \exp(i\underline{k} \cdot \underline{x}_s' - i\omega t) \\ f_{0s}(\underline{x}_s', \underline{v}_s') &= \int d\underline{k}'' \tilde{f}_s(\underline{k}'', \underline{v}_s') \exp(-i\underline{k}'' \cdot \underline{x}_s')\end{aligned}$$

we obtain

$$\begin{aligned}&\int d\underline{k}'' \int d\underline{k} \left[\sum_s \frac{4\pi q_s^2}{m_s} \int d\underline{y} \int_{-\infty}^0 d\tau i\underline{k} \cdot \frac{\partial f_s}{\partial \underline{v}_s} (\underline{k}'', \underline{v}_s') \right. \\ &\tilde{\phi}(\underline{k}) \exp(i\underline{k} \cdot \underline{x}_s' - i\underline{k}'' \cdot \underline{x}_s' - i\omega t) - k^2 \tilde{\phi}(\underline{k}) \left. \right] = 0 \\ &\int d\underline{k} \tilde{\phi}(\underline{k}) \left(\int d\underline{k}' \exp(-i\underline{k}'' \cdot \underline{x} + i\underline{k} \cdot \underline{x}) \left\{ \sum_s \frac{4\pi q_s^2}{m_s} \right. \right. \\ &\int d\underline{y} \int_{-\infty}^0 d\tau i\underline{k} \cdot \frac{\partial f_s}{\partial \underline{v}_s} (\underline{k}'', \underline{v}_s') \exp[i(\underline{k}'' - \underline{k}) \cdot (\underline{x} - \underline{x}_s') - i\omega\tau] \left. \right\} \\ &\left. \left. - k^2 \right) = 0\right)\end{aligned}$$

Let $\underline{k}' \equiv \underline{k} - \underline{k}''$, and we obtain Eq. (4).

Derivation of Eq. (7):

Starting with the identity

$$\begin{aligned}\tilde{f}_s(\underline{k}, \underline{v}) &= \int d\underline{x} f_s(\underline{x}, \underline{v}) \exp(i\underline{k} \cdot \underline{x}) \\ &= \int d\underline{x} g_s(v_\perp, v_\parallel, \underline{x}_{gc}) \exp(i\underline{k} \cdot \underline{x}) \\ &= \int d\underline{x}_{gc} g_s(v_\perp, v_\parallel, \underline{x}_{gc}) \exp(i\underline{k} \cdot \underline{x}_{gc}) \\ &\quad \exp[-i\underline{k} \cdot (\hat{\underline{v}} \times \hat{\underline{B}}_0) \omega_{cs}^{-1}]\end{aligned}$$

$$= \exp[-ik \cdot (\hat{v} \times \hat{B}_0) \omega_{cs}^{-1}] \tilde{g}_s(v_\perp, v_\parallel, k)$$

$$\text{using } \hat{x}_{gc} \equiv \hat{x} + \hat{v} \times \hat{B}_0 \omega_{cs}^{-1}$$

Derivation of Eq. (9):

We put Eq. (7) into Eq. (6) to obtain

$$\begin{aligned} D_s(x, k, \omega) &= \frac{4\pi q_s^2}{m_s} \exp(-ik \cdot \hat{x}) \int dk' \exp(ik' \cdot \hat{x}) \\ &\int dv \int_{-\infty}^0 d\tau ik \cdot \frac{\partial}{\partial v_s'} \{ \exp[-i(k - k')] \cdot (\hat{v}_s' \times \hat{B}_0) \omega_{cs}^{-1} \} \\ &\tilde{g}_s(v_\perp, v_\parallel, k - k') \exp(ik' \cdot (\hat{x}_s' - \hat{x}) - i\omega\tau) \end{aligned} \quad (A1)$$

We evaluate $\frac{\partial}{\partial v_s'} \{ \dots \}$

$$\begin{aligned} \frac{\partial}{\partial v_s'} \{ \dots \} &= \exp[-i(k - k') \cdot (\hat{v} \times \hat{B}_0) \omega_{cs}^{-1}] \\ &\{ \frac{\partial \tilde{g}_s}{\partial v_s'} - \frac{i\tilde{g}_s}{\omega_{cs}} \frac{\partial}{\partial v_s'} [(k - k') \cdot (\hat{v}_s' \times \hat{B}_0)] \} \end{aligned} \quad (A2)$$

where the arguments of \tilde{g}_s and its derivatives are always taken to be $(v_\perp, v_\parallel, k - k')$.

$$\frac{\partial \tilde{g}_s}{\partial v_s'} = \hat{v}_\perp s \frac{\partial \tilde{g}_s}{\partial v_\perp} + \hat{B}_0 \frac{\partial \tilde{g}_s}{\partial v_\parallel} \quad (A3)$$

$$\begin{aligned} \frac{\partial}{\partial v_s'} [(k - k') \cdot (\hat{v}_s' \times \hat{B}_0)] &= \frac{\partial}{\partial v_s'} \{ \hat{v}_s' \cdot [\hat{B}_0 \times (k - k')] \} \\ &= \hat{B}_0 \times (k - k') \end{aligned} \quad (A4)$$

where $\hat{v}_{\perp s}' \equiv v_{\perp s}' / |v_{\perp s}'|$, and $v_{\perp s}' \equiv v_{\perp s}' - (v_s' \cdot \hat{B}_0) \hat{B}_0$

Putting Eqs. (A2), (A3) and (A4) into Eq. (A1), we find

$$\begin{aligned}
 D_s(\underline{x}, \underline{k}, \omega) = & \frac{4\pi q_s^2}{m_s} \exp(-ik \cdot \underline{x}) \int d\underline{k}' \exp(ik' \cdot \underline{x}) \\
 & \int_{-\infty}^0 dy \int_{-\infty}^0 d\tau \exp[-i(k - k') \cdot (v_s' \times \hat{B}_0) \omega_{cs}^{-1}] \\
 & \{ik \cdot \hat{v}_{\perp s}' \frac{\partial \tilde{g}_s}{\partial v_{\perp}} + k \cdot [\hat{B}_0 \times (k - k')] \tilde{g}_s \omega_{cs}^{-1} \\
 & + i k_{\parallel} \frac{\partial \tilde{g}_s}{\partial v_{\parallel}}\} \exp[ik' \cdot (x_s' - x) - i\omega\tau] \tag{A5}
 \end{aligned}$$

We can use the fact that $\underline{k} \cdot (\hat{B}_0 \times \underline{k}) = 0$ to replace $\underline{k} \cdot [\hat{B}_0 \times (k - k')]$ by $\underline{k} \cdot (\hat{B}_0 \times \underline{k}')$ in Eq. (A5). We then put in the expression for the particle orbits, Eq. (8), and obtain

$$\begin{aligned}
 D_s(\underline{x}, \underline{k}, \omega) = & \frac{4\pi q_s^2}{m_s} \exp(-ik \cdot \underline{x}) \int d\underline{k}' \exp(ik' \cdot \underline{x}) \\
 & \int dy \exp[i(k' - k) \cdot (y \times \hat{B}_0) \omega_{cs}^{-1}] \int_{-\infty}^0 d\tau \\
 & \exp[ik \cdot v_{\perp} \omega_{cs}^{-1} \sin \omega_{cs}\tau + i k \cdot (y \times \hat{B}_0) \omega_{cs}^{-1} \\
 & (1 - \cos \omega_{cs}\tau) + ik_{\parallel} v_{\parallel} - i\omega\tau] \\
 & \{[i k \cdot \hat{v}_{\perp} \cos \omega_{cs}\tau + i k \cdot (\hat{v}_{\perp} \times \hat{B}_0) \sin \omega_{cs}\tau] \frac{\partial \tilde{g}_s}{\partial v_{\perp}} \\
 & - \underline{k} \cdot (\hat{B}_0 \times \underline{k}') \omega_{cs}^{-1} \tilde{g}_s + ik_{\parallel} \frac{\partial \tilde{g}_s}{\partial v_{\parallel}}\} \\
 = & \frac{4\pi q_s^2}{m_s} \exp(-ik \cdot \underline{x}) \int d\underline{k}' \exp(ik' \cdot \underline{x}) \int dy \\
 & \exp[ik' \cdot (y \times \hat{B}_0) \omega_{cs}^{-1}] \{[\underline{k} \cdot (\underline{k}' \times \hat{B}_0) \omega_{cs}^{-1} \tilde{g}_s \\
 & + ik_{\parallel} \frac{\partial \tilde{g}_s}{\partial v_{\parallel}}] I_1 + i \frac{\partial \tilde{g}_s}{\partial v_{\perp}} I_2\} \tag{A6}
 \end{aligned}$$

$$\text{where } I_1 \equiv \int_{-\infty}^0 d\tau \exp[i\mathbf{k} \cdot \mathbf{v}_\perp \omega_{cs}^{-1} \sin \omega_{cs}\tau - i\mathbf{k} \cdot (\mathbf{v} \times \hat{\mathbf{B}}_0) \omega_{cs}^{-1} \cos \omega_{cs}\tau + ik_\parallel v_\parallel \tau - i\omega\tau]$$

$$I_2 \equiv \int_{-\infty}^0 d\tau \exp[i\mathbf{k} \cdot \mathbf{v}_\perp \omega_{cs}^{-1} \sin \omega_{cs}\tau - i\mathbf{k} \cdot (\mathbf{v} \times \hat{\mathbf{B}}_0) \omega_{cs}^{-1} \cos \omega_{cs}\tau + ik_\parallel v_\parallel \tau - i\omega\tau] [\mathbf{k} \cdot \mathbf{v}_\perp \cos \omega_{cs}\tau + \mathbf{k} \cdot (\hat{\mathbf{v}}_\perp \times \hat{\mathbf{B}}_0) \sin \omega_{cs}\tau]$$

We define an azimuthal angle ϕ by

$$\mathbf{k} \cdot \mathbf{v}_\perp = k_\perp v_\perp \cos \phi$$

$$-\mathbf{k} \cdot (\mathbf{v} \times \hat{\mathbf{B}}_0) = k_\perp v_\perp \sin \phi$$

Then

$$I_1 = \int_{-\infty}^0 d\tau \exp[ik_\perp v_\perp \omega_{cs}^{-1} \sin(\phi + \omega_{cs}\tau) + ik_\parallel v_\parallel \tau - i\omega\tau]$$

$$I_2 = \int_{-\infty}^0 d\tau \exp[ik_\perp v_\perp \omega_{cs}^{-1} \sin(\phi + \omega_{cs}\tau) + ik_\parallel v_\parallel \tau - i\omega\tau]$$

$$k_\perp \cos(\phi + \omega_{cs}\tau)$$

These integrals can be evaluated by using the Bessel function identity

$$\sum_l J_l(x) \exp(il\theta) = \exp(ix \sin\theta) \quad (A7)$$

$$I_1 = \sum_l J_l(k_\perp v_\perp / \omega_{cs}) \int_{-\infty}^0 d\tau \exp(il\phi + il\omega_{cs} \tau - i\omega\tau + ik_\parallel v_\parallel \tau)$$

$$= i \sum_l J_l(k_\perp v_\perp / \omega_{cs}) \exp(il\phi) (\omega - l\omega_{cs} - k_\parallel v_\parallel)^{-1} \quad (A8)$$

$$\begin{aligned}
I_2 &= (k_{\perp}/2) \sum_{\ell} J_{\ell}(k_{\perp}v_{\perp}/\omega_{cs}) \int_{-\infty}^0 d\tau \sum_{\pm} \exp[i(\ell \pm 1)\phi \\
&\quad + i(\ell \pm 1)\omega_{cs}\tau - i\omega\tau + ik_{\parallel}v_{\parallel}\tau] \\
&= (k_{\perp}/2) \sum_{\ell} \sum_{\pm} J_{\ell \pm 1}(k_{\perp}v_{\perp}/\omega_{cs}) \int_{-\infty}^0 d\tau \exp[i\ell\phi \\
&\quad + i\ell\omega_{cs}\tau - i\omega\tau + ik_{\parallel}v_{\parallel}\tau] \\
&= i(k_{\perp}/2) \sum_{\ell} \sum_{\pm} J_{\ell \pm 1}(k_{\perp}v_{\perp}/\omega_{cs}) \exp(i\ell\phi) \\
&\quad (\omega - \ell\omega_{cs} - k_{\parallel}v_{\parallel})^{-1} \\
&= i(\omega_{cs}/v_{\perp}) \sum_{\ell} \ell J_{\ell}(k_{\perp}v_{\perp}/\omega_{cs}) \exp(i\ell\phi) (\omega - \ell\omega_{cs} - k_{\parallel}v_{\parallel})^{-1}
\end{aligned} \tag{A9}$$

where we have used the Bessel function identity

$$(2\ell/x)J_{\ell}(x) = J_{\ell+1}(x) + J_{\ell-1}(x)$$

The dy in Eq. (A6) can be replaced by $v_{\perp}dv_{\perp}d\phi$, and the integration over ϕ performed. We define α as the angle between \hat{k}' and \hat{k}_{\perp}

$$\exp(i\alpha) = \hat{k}_{\perp} \cdot (\hat{k}' + i\hat{B}_0 \times \hat{k}'') \tag{A10}$$

Then

$$-\hat{k}' \cdot (\hat{v} \times \hat{B}_0) = \hat{k}' \cdot \hat{v}_{\perp} \sin(\phi - \alpha)$$

and we can use the identity (A7) to evaluate

$$\begin{aligned}
\exp[i\hat{k}' \cdot (\hat{v} \times \hat{B}_0) \omega_{cs}^{-1}] &= \exp[-ik' \cdot v_{\perp} \omega_{cs}^{-1} \sin(\phi - \alpha)] \\
&= \sum_m J_m(k' \cdot v_{\perp} / \omega_{cs}) \exp[-im(\phi - \alpha)]
\end{aligned} \tag{A11}$$

The ϕ dependence of I_1 and I_2 , given by Eqs. (A8) and (A9), appears only in the factor $\exp(i\ell\phi)$. The only other ϕ dependence of the integrand in Eq. (A6) is in the term evaluated in Eq. (A11). So the integration over ϕ that must be done in Eq. (A6) is

$$\int d\phi \exp[-im(\phi\alpha)] \exp(i\ell\phi) = 2\pi \delta_{\ell m} \exp(i\ell\alpha) \quad (A12)$$

Putting Eqs. (A8) through (A12) into Eq. (A6), we obtain Eq. (9).

APPENDIX B

Derivation of Eq. (10):

In Eq. (9), $\tilde{g}_s(v_\perp, v_\parallel, \mathbf{k} - \mathbf{k}')$ is negligible for $|\mathbf{k} - \mathbf{k}'| \gg L^{-1}$, where L is the scale length, and for $v_\perp \gg v_s$, where v_s is the thermal velocity. If $a_s \ll L$, where $a_s \equiv v_s/\omega_{cs}$ is the Larmor radius, then $\tilde{g}_s(v_\perp, v_\parallel, \mathbf{k} - \mathbf{k}')$ is negligible unless $(\mathbf{k} - \mathbf{k}') \cdot (\mathbf{v} \times \hat{\mathbf{B}}_0) \omega_{cs}^{-1} \approx 1$, so we can make the approximation

$$\exp[-i(\mathbf{k} - \mathbf{k}') \cdot (\mathbf{v} \times \hat{\mathbf{B}}_0) \omega_{cs}^{-1}] \approx 1 \quad (B1)$$

in Eq. (A5) without changing the integral very much. We use the definition of \tilde{g}_s after Eq. (7) to obtain the identities

$$\begin{aligned} & \int d\mathbf{k}' \exp[i(\mathbf{k}' - \mathbf{k}) \cdot \mathbf{x}] \partial \tilde{g}_s(\mathbf{k} - \mathbf{k}') / \partial v_\parallel \\ &= \partial g_s(\mathbf{x}) / \partial v_\parallel \\ & \int d\mathbf{k}' \exp[i(\mathbf{k}' - \mathbf{k}) \cdot \mathbf{x}] \partial \tilde{g}_s(\mathbf{k} - \mathbf{k}') / \partial v_\perp \\ &= \partial g_s(\mathbf{x}) / \partial v_\perp \\ & \int d\mathbf{k}' [\hat{\mathbf{B}}_0 \times i(\mathbf{k}' - \mathbf{k})] \exp[i(\mathbf{k}' - \mathbf{k}) \cdot \mathbf{x}] \tilde{g}_s(\mathbf{k} - \mathbf{k}') = \hat{\mathbf{B}}_0 \times \nabla g_s(\mathbf{x}) \end{aligned}$$

which can be used together with Eq. (B1) to perform the integration over \mathbf{k}' in Eq. (A5), yielding

$$\begin{aligned} D_s(\mathbf{x}, \mathbf{k}, \omega) &= (4\pi q_s^2/m_s) \exp(-ik \cdot \mathbf{x}) \int dv \int_{-\infty}^0 d\tau \\ &\exp[ik \cdot (x'_s - x) - i\omega\tau] [ik \cdot \hat{v}_{\perp s}' (\partial g_s / \partial v_\perp) \\ &+ ik \cdot (\hat{\mathbf{B}}_0 \times \nabla g_s) \omega_{cs}^{-1} + ik_\parallel (\partial g_s / \partial v_\parallel)] \end{aligned} \quad (B2)$$

Eq. (8) can be put into Eq. (B2), and the integration over τ and ϕ performed just as in Appendix A, yielding Eq. (10). The factor $\exp[i\mathbf{k}' \cdot (\mathbf{v} \times \hat{\mathbf{B}}_0) \omega_{cs}^{-1}]$ which appears in Eq. (A6) must be replaced by $\exp[i\mathbf{k} \cdot (\mathbf{v} \times \hat{\mathbf{B}}_0) \omega_{cs}^{-1}]$, which is justified by Eq. (B1); otherwise the derivation is completely analogous.

APPENDIX C

Derivation of Eq. (12):

For a Maxwellian $g_{s\perp}$

$$g_{s\perp}(v_\perp, x) = (2\pi v_s^2)^{-1} \exp(-v_\perp^2/2v_s^2) n_s(x)$$

and a slab $n_s(x)$ independent of y and z , we have

$$\int dv_\parallel \tilde{g}_s(v_\perp, k - k') = (2\pi v_s^2)^{-1} \exp(-v_\perp^2/2v_s^2) \tilde{n}_s(k_x' - k_x)$$

$$\delta(k_y - k_y') \delta(k_z')$$

where $k_z = 0$ by assumption, \tilde{g}_s is defined after Eq. (7) and \tilde{n}_s is defined after Eq. (12). Then Eq. (9) becomes (after integrating over k_y' , k_z' and v_\parallel)

$$D_s(x, k, \omega) = (4\pi q_s^2/m_s) \int_{-\infty}^{\infty} dk_x' \exp[i(k_x' - k_x)x]$$

$$\int_0^\infty 2\pi v_\perp dv_\perp \sum_\ell \exp(i\ell\alpha) J_\ell(k_\perp v_\perp/\omega_{cs}) J_\ell(k_\perp' v_\perp/\omega_{cs})$$

$$(\omega - \ell\omega_{cs})^{-1} (2\pi v_s^2)^{-1} \exp(-v_\perp^2/2v_s^2)$$

$$[ik_y(k_x' - k_x) + \ell\omega_{cs}/v_s^2] \tilde{n}_s(k_x' - k_x)$$

We define $k'' \equiv k_x' - k_x$, change the variable of integration from k_x' to k'' , and use

$$\begin{aligned} & v_s^{-2} \int_0^\infty v_\perp \exp(-v_\perp^2/2v_s^2) J_\ell(kv_\perp/\omega_{cs}) J_\ell(k'v_\perp/\omega_{cs}) dv_\perp \\ &= \exp[-(k^2 + k'^2)v_s^2/2\omega_{cs}^2] I_\ell(k'v_s^2/\omega_{cs}^2) \end{aligned}$$

[from identity 6.633.2 in Gradshteyn and Ryzhik²³] to obtain Eq. (12).

APPENDIX D

Derivation of Eq. (14):

$$\rho_0(\underline{x}) \sum_s q_s \int dv \ f_{0s}(\underline{x}, \underline{v}) = 0 \text{ for all } \underline{x} \quad (D1)$$

for no net equilibrium charge density.

$$f_{0s}(\underline{x}, \underline{v}) = g_s(v_\perp, v_\parallel, \underline{x}_{gc}) \quad (D2)$$

$$\text{where } \underline{x}_{gc} \equiv \underline{x} + \underline{v} \times \hat{\underline{B}}_0 \omega_{cs}^{-1}$$

$$\text{so } \underline{x}_{gc} = \underline{x} + \underline{v}_y / \omega_{cs}$$

$$y_{gc} = y - v_x / \omega_{cs}$$

Using Eq. (D2), the left hand side of Eq. (D1) becomes

$$\begin{aligned} \rho_0(\underline{x}) &= \sum_s q_s \int dv_x dv_y g_{s\perp}(v_\perp, \underline{x}_{gc}) \\ &= \sum_s q_s (2\pi v_s^2)^{-1} \int dv_x dv_y \exp(-v_\perp^2/2v_s^2) n_s(\underline{x}_{gc}) \end{aligned}$$

for Maxwellian $g_{s\perp}$. For a plasma slab, $n_s(\underline{x})$ independent of y and z ,

$$\rho_0(\underline{x}) = \sum_s q_s (2\pi v_s^2)^{-1} \int dv_x dv_y \exp(-v_\perp^2/2v_s^2) n_s(x + v_y / \omega_{cs}) \quad (D3)$$

For a sinusoidal density profile,

$$n_s(x) = n_{0s} (1 + \Delta_s \cos k_0 x)$$

Eq. (D3) becomes

$$\rho_0(x) = \sum_s q_s (2\pi v_s^2)^{-1} \int dv_x dv_y \exp(-v_x^2/2v_s^2)$$

$$\exp(-v_y^2/2v_s^2) n_{0s} [1 + \Delta_s \cos(k_0 x + k_0 v_y / \omega_{cs})]$$

Integrating over v_x

$$\rho_0(x) = \sum_s n_{0s} q_s (2\pi v_s^2)^{-1/2} \int dv_y \exp(-v_y^2/2v_s^2)$$

$$[1 + \Delta_s \cos(k_0 x + k_0 v_y / \omega_{cs})]$$

$$= \sum_s n_{0s} q_s (2\pi v_s^2)^{-1/2} \int dv_y \exp(-v_y^2/2v_s^2)$$

$$[1 + \Delta_s \exp(ik_0 x) \exp(ik_0 v_y / \omega_{cs})/2$$

$$+ \Delta_s \exp(-ik_0 x) \exp(-ik_0 v_y / \omega_{cs})/2]$$

Since $\rho_0(x)$ vanishes for all x ,

$$\int_0^{2\pi/k_0} \rho_0(x) dx = 2\pi k_0^{-1} \sum_s n_{0s} q_s = 0 \text{ or Eq. (14b) and}$$

$$\int_0^{2\pi/k_0} \rho_0(x) \exp(\pm ik_0 x) dx =$$

$$\pi k_0^{-1} \sum_s n_{0s} q_s \Delta_s (2\pi v_s^2)^{-1/2} \int dv_y \exp(-v_y^2/2v_s^2) \exp(\mp ik_0 v_y / \omega_{cs})$$

$$= \pi k_0^{-1} \sum_s n_{0s} q_s \Delta_s \exp(-k_0^2 v_y^2 / 2\omega_{cs}^2) = 0$$

or Eq. (14a).

APPENDIX E

Solution of Eq. (18):

$$A \frac{\partial^2 \psi}{\partial x^2} + Bx \frac{\partial \psi}{\partial x} + Cx^2 \psi + \lambda \psi = 0 \quad (E1)$$

$$\text{Assume } \psi = \left(\sum_{m=0}^n a_m x^m \right) \exp(-\beta x^2/2) \quad (E2)$$

$$\text{Then } \frac{\partial \psi}{\partial x} = \left(\sum_{m=0}^{n-1} (m+1)a_{m+1} x^m \right) \exp(-\beta x^2/2)$$

$$\begin{aligned} & -(\beta \sum_{m=0}^n a_m x^{m+1}) \exp(-\beta x^2/2) \\ & = [\sum_{m=0}^{n-1} (m+1)a_{m+1} x^m - \beta \sum_{m=1}^{n+1} a_{m-1} x^m] \exp(-\beta x^2/2) \\ & = \left\{ \sum_{m=1}^{n+1} [(m+1)a_{m+1} - \beta a_{m-1}] x^m + a_1 \right\} \exp(-\beta x^2/2) \end{aligned} \quad (E3)$$

$$\begin{aligned} \frac{\partial^2 \psi}{\partial x^2} & = \left(\sum_{m=2}^{n+2} \{(m+1)[(m+2)a_{m+2} - \beta a_m] \right. \\ & \quad \left. - \beta(m a_m - \beta a_{m-2})\} x^m \right. \\ & \quad \left. + [2(3a_3 - \beta a_1) - \beta a_1] x + 2a_2 - \beta a_0 \right) \exp(-\beta x^2/2) \\ & = \left\{ \sum_{m=2}^{n+2} [(m^2 + 3m + 2)a_{m+2} - \beta(2m + 1)a_m \right. \\ & \quad \left. + \beta^2 a_{m-2}] x^m + 3(2a_3 - \beta a_1) x + (2a_2 - \beta a_0) \right\} \exp(-\beta x^2/2) \end{aligned} \quad (E4)$$

$$x (\partial \psi / \partial x) = \left[\sum_{m=2}^{n+2} (ma_m - \beta a_{m-2}) x^m + a_1 x \right] \exp(-\beta x^2/2) \quad (E5)$$

$$x^2 \psi = \left(\sum_{m=2}^{n+2} a_{m-2} x^m \right) \exp(-\beta x^2/2) \quad (E6)$$

Putting Eqs. (E4), (E5) and (E6) into Eq. (E1) and dividing through by $\exp(-\beta x^2/2)$ yields

$$\begin{aligned} & \sum_{m=2}^{n+2} x^m \{ A[m^2 + 3m + 2]a_{m+2} - \beta(2m + 1)a_m \\ & + \beta^2 a_{m-2}] + B[m a_m - \beta a_{m-2}] \\ & + C a_{m-2} + \lambda a_m \} \\ & + [3A(2a_3 - \beta a_1) + B a_1 + \lambda a_1] x \\ & + [A(2a_2 - \beta a_0) + \lambda a_0] = 0 \end{aligned} \quad (E7)$$

This can be satisfied for all x only if each term in the polynomial vanishes. So

$$A(2a_2 - \beta a_0) + \lambda a_0 = 0 \quad (E8)$$

$$\begin{aligned} & 3A(2a_3 - \beta a_1) + B a_1 + \lambda a_1 \\ & = 6Aa_3 + (B + \lambda - 3A\beta)a_1 = 0 \end{aligned} \quad (E9)$$

$$\begin{aligned} & A(m^2 + 3m + 2)a_{m+2} + [Bn - \beta A(2m + 1) + \lambda]a_m \\ & + (C - \beta B + \beta^2 A)a_{m-2} = 0 \quad \text{for } n + 2 \geq m \geq 2 \end{aligned} \quad (E10)$$

Setting $m = n + 2$ in Eq. (E10) yields (since $a_m = 0$ for $m > n$)

$$C - \beta B + \beta^2 A = 0 \quad (E11)$$

Then Eq. (E10) becomes

$$A(m+2)(m+1)a_{m+2} + [Bm - \beta A(2m+1) + \lambda]a_m = 0 \quad (E12)$$

$$\text{where } \beta = (B/2A) + [(B/2A)^2 - C/A]^{1/2} \quad (E13)$$

[the + sign is taken in Eq. (E13) so that $\operatorname{Re} \beta > 0$ and $\psi(x) \rightarrow 0$ as $x \rightarrow \pm \infty$].

Taking $m=n$ in Eq. (E12) yields

$$Bn - \beta A(2n + 1) + \lambda = 0$$

or

$$\lambda = \beta A(2n + 1) - Bn \quad (E14)$$

Taking $m = n - 1$ yields $a_{n-1} = 0$, which further implies $a_{n-3} = a_{n-5} = \dots = 0$, so ψ must be either even or odd in x .

For $0 \leq m \leq n - 2$, Eqs. (E12) and (E14) give the recursion relation for the coefficients a_m

$$\begin{aligned} \frac{a_m}{a_{m+2}} &= \frac{A(m+2)(m+1)}{-Bm + \beta A(2m+1) + \lambda} \\ &= \frac{A(m+2)(m+1)}{B(n-m) - 2\beta A(n-m)} \\ &= \frac{(m+2)(m+1)}{(n-m)(B/A - 2\beta)} \\ \frac{a_m}{a_{m+2}} &= \frac{(m+2)(m+1)}{2(m-n)\eta} \end{aligned} \quad (E15)$$

where $\eta = \beta - B/2A$

$$= [(B/2A)^2 - C/A]^{1/2} \quad (E16)$$

Eq. (E15) is the recursion relation for the Hermite polynomial

$$\sum_m a_m x^m = H_n(\eta^{1/2} x) \quad (E17)$$

So the solutions are

$$\psi_n(x) = H_n(\eta^{1/2} x) \exp(-\beta x^2/2) \quad (E18)$$

with β and η defined by Eqs. (E13) and (E16).

Appendix F

Sketch of Proof that Local Method is Valid When Inequality (21) is Satisfied:

We wish to show that inequality (21)

$$L(k_L^2 + k_y^2)^{1/2} \gg 1$$

is the criterion for being able to neglect the terms in Eq.(17) involving higher derivatives of D, so that Eq.(20) is a good approximation to at least some of the solutions of Eq.(15). We will consider a general dispersion function $D(x, k_x, \omega)$, not just the D appropriate to the model considered in Sec.III. However, we will not attempt to make our results as general as possible, but will make various physically reasonable assumptions about $D(x, k_x, \omega)$ when convenient. Sometimes we will make mathematical assumptions about $D(x, k_x, \omega)$ and the physical content of these assumptions will not be obvious; in such cases we cannot prove that the assumptions will be valid for all models of physical interest (or even for the model considered in Sec.III), but we conjecture that the assumptions will be valid for most models of physical interest.

To simplify notation, we will use $\psi(x) \equiv \exp(-ik_L x) \phi(x + x_L)$ and $Q(x, k_x, \omega) \equiv D(x + x_L, k_x + k_L, \omega)$. In this notation, Eq.(15) is

$$Q(x, -i \frac{\partial}{\partial x}, \omega) \psi(x) = 0 \quad (F1)$$

and Eq.(16) is

$$Q(0, 0, \omega_L) = \frac{\partial Q}{\partial x}(0, 0, \omega_L) = \frac{\partial Q}{\partial k_x}(0, 0, \omega_L) = 0$$

Anticipating our result that Eq.(17) is nearly valid without the higher derivatives of D, we expand Q and ψ in perturbation series, and write

$$Q(x, k_x, \omega_n) = Q^{(0)}(x, k_x, \omega_L) + \lambda_n + Q^{(1)}(x, k_x, \omega_n)$$

[The subscript n indicates we are looking at a normal mode whose frequency ω_n is given to lowest order by Eq.(20b)]

$$Q^{(0)}(x, k_x, \omega_L) \equiv -1/2 \frac{\partial^2 Q}{\partial k_x^2}(0, 0, \omega_L) k_x^2 - i \frac{\partial^2 Q}{\partial k_x \partial x}(0, 0, \omega_L) x k_x + 1/2 \frac{\partial^2 Q}{\partial x^2}(0, 0, \omega_L) x^2$$

$$\lambda_n^{(0)} = \lambda_n^{(0)} + \lambda_n^{(1)} + \dots = (\omega_n - \omega_L) \frac{\partial Q^{(0)}}{\partial \omega}(0, 0, \omega_L)$$

$$\lambda_n^{(m)} \equiv \Delta \omega_n^{(m)} \frac{\partial Q^{(0)}}{\partial \omega}(0, 0, \omega_L)$$

$$\omega_n = \omega_L + \Delta \omega_n^{(0)} + \Delta \omega_n^{(1)} + \dots$$

$$\psi_n(x) = \psi_n^{(0)}(x) + \psi_n^{(1)}(x) + \dots$$

Note that $Q^{(1)}$ contains all of the terms neglected in Eq.(17). As a result of these terms, ω_n and ψ_n have small corrections $\Delta \omega_n^{(1)} + \Delta \omega_n^{(2)} + \dots$ and $\psi_n^{(1)} + \psi_n^{(2)} + \dots$. Eq.(F1) may be written

$$(Q^{(0)} + Q^{(1)} + \lambda_n^{(0)} + \lambda_n^{(1)} + \dots)(\psi_n^{(0)} + \psi_n^{(1)} + \dots) = 0 \quad (F2)$$

The zero-order terms of Eq.(F2) give Eq.(18), or in our notation

$$[Q^{(0)}(x, -i \frac{\partial}{\partial x}, \omega_L) + \lambda_n^{(0)}] \psi_n^{(0)}(x) = 0 \quad (F3)$$

where $\psi_n^{(0)}$ and $\lambda_n^{(0)}$ are given by Eq.(19). The first-order terms of Eq.(F2) give

$$(Q^{(0)} + \lambda_n^{(0)}) \psi_n^{(1)} + (Q^{(1)} + \lambda_n^{(1)}) \psi_n^{(0)} = 0 \quad (F4)$$

Following the usual procedure of quantum mechanical perturbation theory, we expand $\psi_n^{(1)}(x)$ in the eigenfunctions $\psi_m^{(0)}(x)$ of $Q^{(0)}$ [given by Eq.(19a)]:

$$\psi_n^{(1)}(x) = \sum_{m=0}^{\infty} c_{mn} \psi_m^{(0)}(x) \quad (F5)$$

$$\text{where } c_{mn} \equiv \int \psi_m^{(0)*}(x) \psi_n^{(1)}(x) dx / \int |\psi_m^{(0)}(x)|^2 dx$$

$$\text{Then, using } Q^{(0)} \psi_m^{(0)} = -\lambda_m^{(0)} \psi_m^{(0)},$$

Eq.(F4) becomes

$$\sum_{m=0}^{\infty} (\lambda_n^{(0)} - \lambda_m^{(0)}) c_{mn} \psi_m^{(0)} + (Q^{(1)} + \lambda_n^{(1)}) \psi_n^{(0)} = 0 \quad (F6)$$

Eq. (F6) can be used to find $\lambda_n^{(1)}$ and c_{mn} for $m \neq n$. If we left-multiply Eq. (F6) by $\psi_n^{(0)*}$ and integrate over x , we obtain

$$\int \psi_n^{(0)*} Q^{(1)} \psi_n^{(0)} dx + \lambda_n^{(1)} \int |\psi_n^{(0)}|^2 dx = 0$$

$$\text{or } \lambda_n^{(1)} = - \int \psi_n^{(0)*} Q^{(1)} \psi_n^{(0)} dx / \int |\psi_n^{(0)}|^2 dx \quad (F7)$$

Left-multiplying Eq. (F6) by $\psi_m^{(0)*}$ for $m \neq n$ and integrating over x yields

$$c_{mn} (\lambda_n^{(0)} - \lambda_m^{(0)}) = - \int \psi_m^{(0)*} Q^{(1)} \psi_n^{(0)} dx / \int |\psi_m^{(0)}|^2 dx \quad (F8)$$

Using Eq. (F7) we will show that (with certain assumptions) inequality (21) implies $\lambda_n^{(1)} \ll \lambda_n^{(0)}$ for small n . Similar arguments (which we will not go through), using Eq. (F8), would show that inequality (21) also implies $c_{mn} \ll 1$ for $m \neq n$, for small n . Thus we will show that if inequality (21) is satisfied, Eqs. (20a) and (20b) are good approximations to the exact normal mode potentials and frequencies, for small n .

We wish to estimate an upper bound for the expression $\int \psi_n^{(0)*} Q^{(1)} \psi_n^{(0)} dx$ appearing in Eq. (F7). We will consider $n = 0$; the same arguments apply for any $n \sim 1$.

From Eq. (19a)

$$\psi_0^{(0)}(x) = \exp(-\beta x^2/2)$$

We note that $\psi_0^{(0)}(x)$ is negligibly small for $x \gg (\text{Re } \beta)^{-1/2}$, and that its Fourier transform is negligibly small for $k_x \gg \beta^{1/2}$. This suggests that $\int \psi_0^{(0)*} Q^{(1)} \psi_0^{(0)} dx$ will depend on $Q^{(1)}(x, k_x, \omega)$ only for $|x| \lesssim (\text{Re } \beta)^{-1/2}$ and $|k_x| \lesssim \beta^{1/2}$, and not for much larger values of x and k_x . Also, if $\lambda_0^{(1)} \ll \lambda_0^{(0)}$, then $\Delta\omega_0^{(1)} \ll \Delta\omega_0^{(0)}$, and we need only consider values of

ω satisfying $|\omega - \omega_L| \leq \Delta\omega_0^{(0)}$. Then we expect

$$\int \psi_0^{(0)*} Q^{(1)} \psi_0^{(0)} dx \lesssim Q_{\max}^{(1)} \int \psi_0^{(0)*} \psi_0^{(0)} dx \quad (F9)$$

where $Q_{\max}^{(1)}$ is the maximum absolute value attained by $Q^{(1)}(x, k_x, \omega)$ for any $|x| \leq (\text{Re } \beta)^{-1/2}$, $|k_x| \leq \beta^{1/2}$ and $|\omega - \omega_L| \leq \Delta\omega_0^{(0)}$. It is possible to imagine operators $Q^{(1)}$ for which Eq.(F9) would not be satisfied, e.g. $Q^{(1)}$ could be exponentially large at $|x| \gg (\text{Re } \beta)^{-1/2}$ for $|k_x| \gg \beta^{1/2}$. However, we conjecture that Eq.(F9) is true for any physically reasonable choice of $Q^{(1)}$.

Then Eqs.(F7) and (F9) imply $\lambda_0^{(1)} \leq Q_{\max}^{(1)}$. Using the definition following Eq.(F2),

$$Q^{(1)}(x, k_x, \omega) = \sum_{\substack{p, q, r \geq 0 \\ p+q+2r \geq 3}} \frac{\frac{\partial^{p+q+r} Q(0, 0, \omega_L)}{\partial x^p \partial k_x^q \partial \omega^r} x^p k_x^q (\omega - \omega_L)^r}{p! q! r!}$$

Thus

$$\lambda_0^{(1)} \leq Q_{\max}^{(1)} \leq \sum_{\substack{p, q, r \geq 0 \\ p+q+2r \geq 3}} \left| \frac{\frac{\partial^{p+q+r} Q(0, 0, \omega_L)}{\partial x^p \partial k_x^q \partial \omega^r}}{p! q! r!} \right| \frac{|\text{Re } \beta|^{-p/2} |\beta|^{q/2} |\Delta\omega_0^{(0)}|^r}{p! q! r!} \quad (F10)$$

We need an upper bound on

$\left| \frac{\partial^{p+q+r} Q(0, 0, \omega_L)}{\partial x^p \partial k_x^q \partial \omega^r} \right|$. We can estimate this by noting that Q is the sum of several terms

$$Q = \sum_j Q_j$$

where each term Q_j is due to a different physical effect, e.g. the vacuum term, the electron convection term, the ion Landau damping term, etc. Each Q_j is assumed to be nearly independent of x for $|x| \leq L_j$; thus L_j is an effective scale length for the plasma properties associated with Q_j (e.g.

density or density gradient of one species). $Q(0,0,\omega_L) = 0$ because all of the Q_j cancel out at $x = 0$, $k_x = 0$, $\omega = \omega_L$. In the vicinity of this point, at least two of the Q_j must be much greater than Q . Similarly, for the dominant terms Q_j , $\partial Q_j / \partial x$ and $\partial Q_j / \partial k_x$ will be much greater than $\partial Q / \partial x$ and $\partial Q / \partial k_x$. We will assume, however, that $\partial Q_j / \partial \omega \sim \partial Q / \partial \omega$, $\partial^2 Q_j / \partial k_x^2 \sim \partial^2 Q / \partial k_x^2$ and $\partial^2 Q_j / \partial x^2 \sim \partial^2 Q / \partial x^2$ for at least some of the dominant terms Q_j .

As may be seen from Eq.(12), k_x appears in D only as part of the expression $(k_x^2 + k_y^2)^{1/2}$, hence k_x appears in Q only as part of $[(k_x + k_L)^2 + k_y^2]^{1/2}$. So we expect each term Q_j to be nearly independent of k_x for $k_x \ll k \equiv (k_L^2 + k_y^2)^{1/2}$. Finally, we assume that all dominant terms Q_j are nearly independent of ω for $|\omega - \omega_L| \lesssim \Omega$, and that $\partial Q / \partial \omega \sim Q_j / \Omega$.

[If, on the contrary, $\partial Q / \partial \omega \ll Q_j / \Omega$, we can still use the local method if we re-define $\lambda_n^{(0)}$ as $\Delta\omega^{(0)} \partial Q^{(0)} / \partial \omega + (1/2) (\Delta\omega_n^{(0)})^2 \partial^2 Q^{(0)} / \partial \omega^2$, and $\lambda_n^{(1)}$ as $\Delta\omega_n^{(1)} \partial Q^{(0)} / \partial \omega + \Delta\omega_n^{(1)} \Delta\omega_n^{(0)} \partial^2 Q^{(0)} / \partial \omega^2$. Then Eqs.(19a), (19b) and (20a) will still be valid if $\lambda_n^{(1)} \ll \lambda_n^{(0)}$, but Eq.(20b) must be replaced by

$$\omega_n = \omega_L - (\partial D / \partial \omega) (\partial^2 D / \partial \omega^2)^{-1} \pm [(\partial D / \partial \omega)^2 (\partial^2 D / \partial \omega^2)^{-2} - (2n\pi + \beta) (\partial^2 D / \partial k_x^2) (\partial^2 D / \partial \omega^2)^{-1}]^{1/2} \quad (F11)$$

In other words, for each integer n there will be two normal modes, with nearly identical potentials given by Eq.(20a), and with frequencies given by the + and - choices of Eq.(F11). This situation occurs near the values of k_y and ω where two modes interact, e.g. a drift wave and a Bernstein wave.]

If $Q_j(x, k_x, \omega)$ is analytic in the range $|x| \ll L_j$, $k_x \ll k$, $|\omega - \omega_L| \ll \Omega$, we can write

$$Q_j(x, k_x, \omega) - Q_j(0,0, \omega_L) = \sum_{\substack{p,q,r \geq 0 \\ p+q+r \geq 1}} \frac{\partial^{p+q+r} Q_j(0,0, \omega_L)}{\partial x^p \partial k_x^q \partial \omega^r} \frac{x^p k_x^q (\omega - \omega_L)^r}{p! q! r!} \quad (F12)$$

Since

$$|Q_j(x, k_x, \omega) - Q_j(0, 0, \omega_L)| \leq Q_j(0, 0, \omega_L)$$

for all $|x| \leq L_j$, $|k_x| \leq k$, $|\omega - \omega_L| \leq \Omega$, it follows from Eq.(F12) that

$$\left| \frac{\partial^{p+q+r} Q_j(0, 0, \omega_L)}{\partial x^p \partial k_x^q \partial \omega^r} \right| \leq p! q! r! L_j^{-p} k^{-q} \Omega^{-r} |Q_j(0, 0, \omega_L)|$$

If there are only a few dominant terms Q_j ,

$$\left| \frac{\partial^{p+q+r} Q(0, 0, \omega_L)}{\partial x^p \partial k_x^q \partial \omega^r} \right| \leq \left| \frac{\partial^{p+q+r} Q_j(0, 0, \omega_L)}{\partial x^p \partial k_x^q \partial \omega^r} \right|$$

it follows that

$$\left| \frac{\partial^{p+q+r} Q(0, 0, \omega_L)}{\partial x^p \partial k_x^q \partial \omega^r} \right| \leq p! q! r! L^{-p} k^{-q} \Omega^{-r} |Q_j(0, 0, \omega_L)| \quad (\text{F13})$$

where L is the smallest L_j for any of the dominant terms Q_j , and Q_j is a typical dominant term. Putting Eq.(F13) into Eq.(F10) yields

$$\lambda_0^{(1)} \leq \sum_{\substack{p, q, r > 0 \\ p+q+2r \geq 3}} (L |\operatorname{Re}\beta|^{-1/2})^{-p} (k |\beta|^{-1/2})^{-q} (\Omega |\Delta\omega_0^{(0)}|^{-1})^{-r} |Q_j(0, 0, \omega_L)|$$

We want to compare $\lambda_0^{(1)}$ to $\lambda_0^{(0)}$ where

$$\lambda_0^{(0)} = \Delta\omega_0^{(0)} \partial Q / \partial \omega \sim \Delta\omega_0^{(0)} Q_j \Omega^{-1}$$

So $\lambda_0^{(1)} \ll \lambda_0^{(0)}$ if

$$L \ll |\operatorname{Re}\beta|^{-1/2} \quad (\text{F14})$$

and

$$k \ll |\beta|^{1/2} \quad (\text{F15})$$

and

$$\Delta\omega_0^{(0)} \ll \Omega \quad (\text{F16})$$

We will assume $\text{Re } \beta \sim \beta$ (this may not be true for plasmas in which magnetic shear is important) so Eq.(F14) becomes

$$L \ll |\beta|^{-1/2} \quad (\text{F17})$$

If $B^2 - 4AC \sim -4AC$ in Eq.(18) (This is certainly true for all of the modes found in Sec. V) then, from the definition of β after Eq.(19),

$$\begin{aligned} \beta &\sim \left(\frac{\partial^2 Q}{\partial x^2} / \frac{\partial^2 Q}{\partial k_x^2} \right)^{1/2} \\ &\sim \left(\frac{2Q_j}{L^2} / \frac{2Q_j}{k^2} \right)^{1/2} \sim kL^{-1} \end{aligned} \quad (\text{F18})$$

From Eq.(20b),

$$\begin{aligned} \Delta\omega_0^{(0)} &= -(\beta/2)(\partial Q/\partial \omega)^{-1}(\partial^2 Q/\partial k_x^2) \\ &\sim (k/2L)(Q_j/\Omega)^{-1}(2Q_j/k^2) \\ &= \Omega(kL)^{-1} \end{aligned} \quad (\text{F19})$$

Using Eq.(F18) and F(18), Eq.(F15), (F16), and (F17) all reduce to

$$Lk \gg 1$$

$$\text{i.e. } L(k_L^2 + k_y^2)^{1/2} \gg 1 \quad (\text{F20})$$

which is inequality (21).

Appendix G

Sketch of Proof that Normal Modes are in the Form of Eq. (32):

Floquet's theorem²⁴ tells us that a differential equation of order m

$$D(x, -i\frac{\partial}{\partial x}, \omega) \phi(x) = 0 \quad (G1)$$

where

$$D(x, k_x, \omega) = P_m(x, \omega) k_x^m + P_{m-1}(x, \omega) k_x^{m-1} + \dots + P_0(x, \omega) \quad (G2)$$

with coefficients $P_i(x, \omega)$ periodic in x with period $2\pi k_o^{-1}$

$$P_i(x, \omega) = P_i(x + 2\pi k_o^{-1}, \omega) \text{ for } i = 1, 2, \dots, m$$

has m independent solutions $\phi_j(x)$ which may be chosen so that

$$\phi_j(x + 2\pi k_o^{-1}) = \exp[2\pi i K_j(\omega) k_o^{-1}] \phi_j(x) \\ \text{for } j = 1, 2, \dots, m \quad (G3)$$

where each $K_j(\omega)$ depends on the functions $P_0(x, \omega), P_1(x, \omega), \dots, P_m(x, \omega)$.

Then the most general solution to Eq. (G1) is

$$\phi(x) = \sum_{j=1}^m A_j \phi_j(x) = \sum_{j=1}^m A_j \exp(iK_j x) \sum_{p=-\infty}^{\infty} \phi_{p,j} \exp(ipk_o x)$$

$$\text{where } \sum_p |\phi_{p,j}|^2 = 1$$

If we take as boundary conditions the requirement that $\phi(x)$ remain finite as $x \rightarrow \pm\infty$, then

$$A_j = 0 \quad \text{or} \quad \text{Im}K_j(\omega) = 0$$

for every j , $1 \leq j \leq m$. If $\text{Im}K_j(\omega) = 0$ for only one value of j , then the only $\phi(x)$ which satisfies the boundary conditions is

$$\phi(x) = \exp(iK_j x) \sum_{p=-\infty}^{\infty} \phi_{p,j} \exp(ipk_o x) \quad (G4)$$

If $\text{Im}K_j(\omega) = 0$ for more than one value of j , then there is a degeneracy at this value of ω , but we are still free to choose the normal modes to be of the form given by Eq.(G4).

In fact $D(x, k_x, \omega)$ is not a polynomial function of k_x , as in Eq.(G2), but is a more complicated analytic function of k_x , given by Eq.(12), so Eq.(G1) is an integral equation rather than a differential equation. Is it possible that there is a normal mode solution $\phi(x)$ of Eq.(G1) [with $D(x, k_x, \omega)$ an arbitrary analytic function of k_x , still periodic in x] which could not be written in the form of Eq.(G4)? Suppose that such a mode $\phi(x)$ does exist. If $\phi(x)$ is differentiable, then there is some wave number k such that $\phi(k_x)$ is negligibly small for $|k_x| \geq k$. There is also some integer m such that $D(x, k_x, \omega)$ can be approximated very well by Eq.(G2) for $|k_x| \leq k$. Then $\phi(x)$ would be very close to a normal mode of Eq.(G1) with $D(x, k_x, \omega)$ given by Eq.(G2), which would contradict our supposition that $\phi(x)$ cannot be written in the form of Eq.(G4).

APPENDIX H

Derivation of Eq. (35):

We start with the definitions of $G_{0,s}$ and $G_{\pm 1,s}$ after Eq. (25), and use

$$\exp(-k^2 a_s^2) I_\ell(k^2 a_s^2) \approx (2\pi)^{-1/2} (ka_s)^{-1} \exp(-\ell^2/2k^2 a_s^2) \quad (H1)$$

(valid when $k^2 a_s^2 \gg \ell \gg 1$)¹⁹ and replace the sum over ℓ by an integral [valid when $\text{Im } \omega/\omega_{ci} \geq 1$ so that $(\omega/\omega_{cs} - \ell)^{-1}$ varies slowly with ℓ , and $k_0 \lesssim k$ so that $\exp(i\ell\alpha_{\pm 1})$ varies slowly with ℓ ; these conditions also ensure that $\ell \gg 1$ for most terms that contribute significantly, since typically $|\ell| \approx |\omega|/\omega_{cs}$].

We first consider $G_{0,s}$. With the above approximations,

$$G_{0,s}(k_x, \omega) = (2\pi)^{-1/2} (\omega_{ps}^2/v_s^2) (ka_s)^{-1} \int_{-\infty}^{\infty} d\ell \ell \exp(-\ell^2/2k^2 a_s^2) (\omega/\omega_{cs} - \ell)^{-1} \quad (H2)$$

We do the integration in Eq. (H2):

$$\begin{aligned} & \int_{-\infty}^{\infty} d\ell \ell \exp(-\ell^2/2k^2 a_s^2) (\omega/\omega_{cs} - \ell)^{-1} = \\ & \int_{-\infty}^{\infty} d\ell (\ell - \omega/\omega_{cs}) \exp(-\ell^2/2k^2 a_s^2) (\omega/\omega_{cs} - \ell)^{-1} \\ & + (\omega/\omega_{cs}) \int_{-\infty}^{\infty} d\ell \exp(-\ell^2/2k^2 a_s^2) (\omega/\omega_{cs} - \ell)^{-1} \\ & = -(2\pi)^{1/2} ka_s - (\omega/\omega_{cs}) \pi^{1/2} Z(\omega/\sqrt{2k} v_s) \end{aligned} \quad (H3)$$

Eqs. (H2) and (H3) yield the first part of Eq. (35):

$$G_{0,s}(k_s, \omega) = -(\omega_{ps}^2/v_s^2)[1 + \zeta_0^2(\zeta_0)] \quad (H4)$$

where $\zeta_0 \equiv \omega/\sqrt{2} k v_s$

To calculate $G_{\pm 1,s}$, we note that

$$\begin{aligned} \exp[-(k^2 + k_{\pm 1}^2)a_s^2/2] &= \exp[-(k - k_{\pm 1})^2 a_s^2/2] \\ \exp(-k k_{\pm 1} a_s^2) \end{aligned} \quad (H5)$$

$$(k - k_{\pm 1})^2 \approx k_x^2 k_0^2/k k_{\pm 1} + \theta(k_0^3/k) \quad (H6)$$

$$\alpha_{\pm 1} \approx \mp k_y k_0/k k_{\pm 1} + \theta(k_0^3/k^3) \quad (H7)$$

where Eqs. (H6) and (H7) are valid when $k_0 \ll k$, and may be derived from the definitions of $k_{\pm 1}$ and $\alpha_{\pm 1}$ after Eq. (25). Starting with the definition of $G_{\pm 1,s}$ after Eq. (25), and using Eqs. (H1), (H5), (H6) and (H7), we obtain

$$\begin{aligned} G_{\pm 1,s}(k_x, \omega) &= (\omega_{ps}^2 \Delta_s^2 / 2v_s^2) (2\pi k k_{\pm 1} a_s^2)^{-1/2} \\ &\int_{-\infty}^{\infty} d\ell \exp(\mp i\ell k_y k_0/k k_{\pm 1}) \exp(-k_x^2 k_0^2 a_s^2 / 2k k_{\pm 1}) \\ &\exp(-\ell^2 / 2k k_{\pm 1} a_s^2) (\ell \pm ik_y k_0 a_s^2) (\omega/\omega_{cs} - \ell)^{-1} \end{aligned} \quad (H8)$$

Rearranging terms, Eq. (H8) becomes

$$\begin{aligned} G_{\pm 1,s} &= (\omega_{ps}^2 \Delta_s^2 / 2v_s^2) (2\pi k k_{\pm 1} a_s^2)^{-1/2} \exp(-k_0^2 a_s^2 k / 2k k_{\pm 1}) \\ &\int_{-\infty}^{\infty} d\ell \exp(-\ell^2 / 2k k_{\pm 1} a_s^2 \mp i\ell k_y k_0 / k k_{\pm 1} + k_0^2 k_y^2 a_s^2 / 2k k_{\pm 1}) \\ &(\ell \pm ik_y k_0 a_s^2) (\omega/\omega_{cs} - \ell)^{-1} \end{aligned} \quad (H9)$$

Changing the variable of integration from ℓ to $\ell' \equiv \ell \pm ik_y k_0 a_s^2$,

the integral in Eq. (H9) becomes

$$\int_{-\infty}^{\infty} d\ell' \exp(-\ell'^2/2k k_{\pm 1} a_s^2) \ell' (\omega/\omega_{cs} - \ell' \pm ik_y k_0 a_s^2)^{-1}$$

This integral is of the same form as the integral in Eq. (H2), but with ω/ω_{cs} in Eq. (H2) replaced by $\omega/\omega_{cs} \pm ik_y k_0 a_s^2$, and it can be solved in the same way. To obtain the second part of Eq. (35), we must further replace $k_{\pm 1}$ everywhere by k , which is justified if $k_0 \ll k$. Note that we could not have replaced $k_{\pm 1}$ by k before writing down Eq. (H8), or we would have lost the factor $\exp(-k_x^2 k_0^2 a_s^2 / 2k k_{\pm 1})$ appearing in Eq. (H8).

It might be argued that it was not justified to neglect the higher order terms in Eqs. (H6) and (H7), since these terms, although small compared to the leading terms, may not be small compared to unity when they appear in the exponentials in Eq. (H8); hence they might significantly change Eq. (H8). However, a careful analysis including these higher order terms shows that they are only important when $G_{\pm 1, s}$ is exponentially small, in which case $G_{\pm 1, s}$ would not be important in the dispersion relation anyway.

APPENDIX I

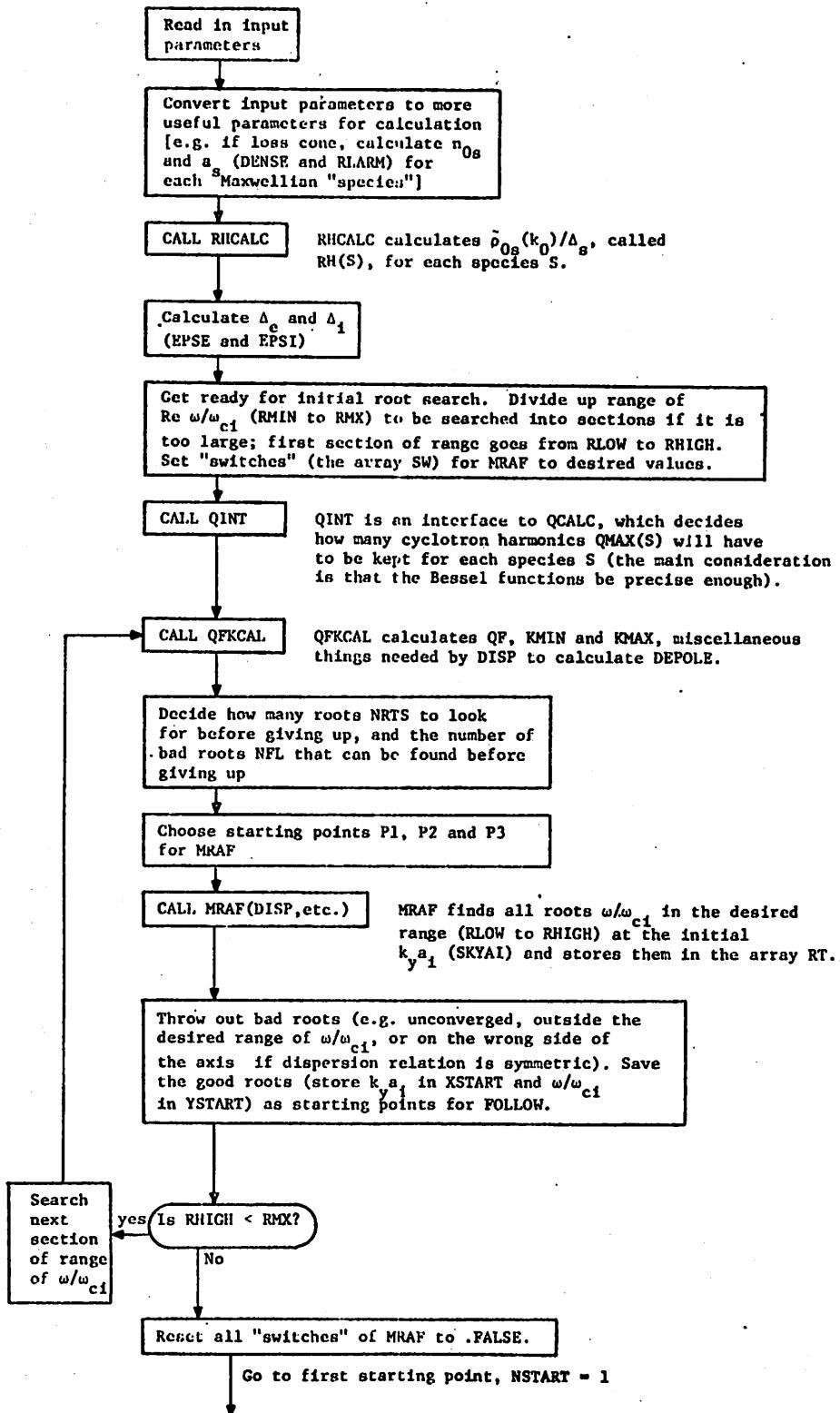
Outlines of the main program ROOTS [which finds the normal modes $\phi(x)$ and frequencies ω , using the nonlocal method described in Sec. IIIB] and of the three large subroutines FOLLOW [which follows a given branch of $\omega(k_y)$ out from small k_y to large k_y], DISP (which calculates the dispersion function $\det A_{p,p}$, for a given ω and k_y) and MRAF [which finds the zeroes of $\det A_{p,p}(\omega)$ for a given k_y] are shown in the flow charts. These charts are intended only as rough guides to the programs. Details of the I/O and details of how various decisions are made (e.g. how FOLLOW decides when two roots are a complex pair or a fork; how FOLLOW decides when to increase or decrease the increment in k_y ; how MRAF decides when $\phi_0 \approx 0$) are not shown. Also not shown are certain modes of operation which were not found to be very useful, e.g. a mode of operation where the frequency, rate of spreading and acceleration were found for wave packets localized at different values of x . For such details the listing may be consulted.

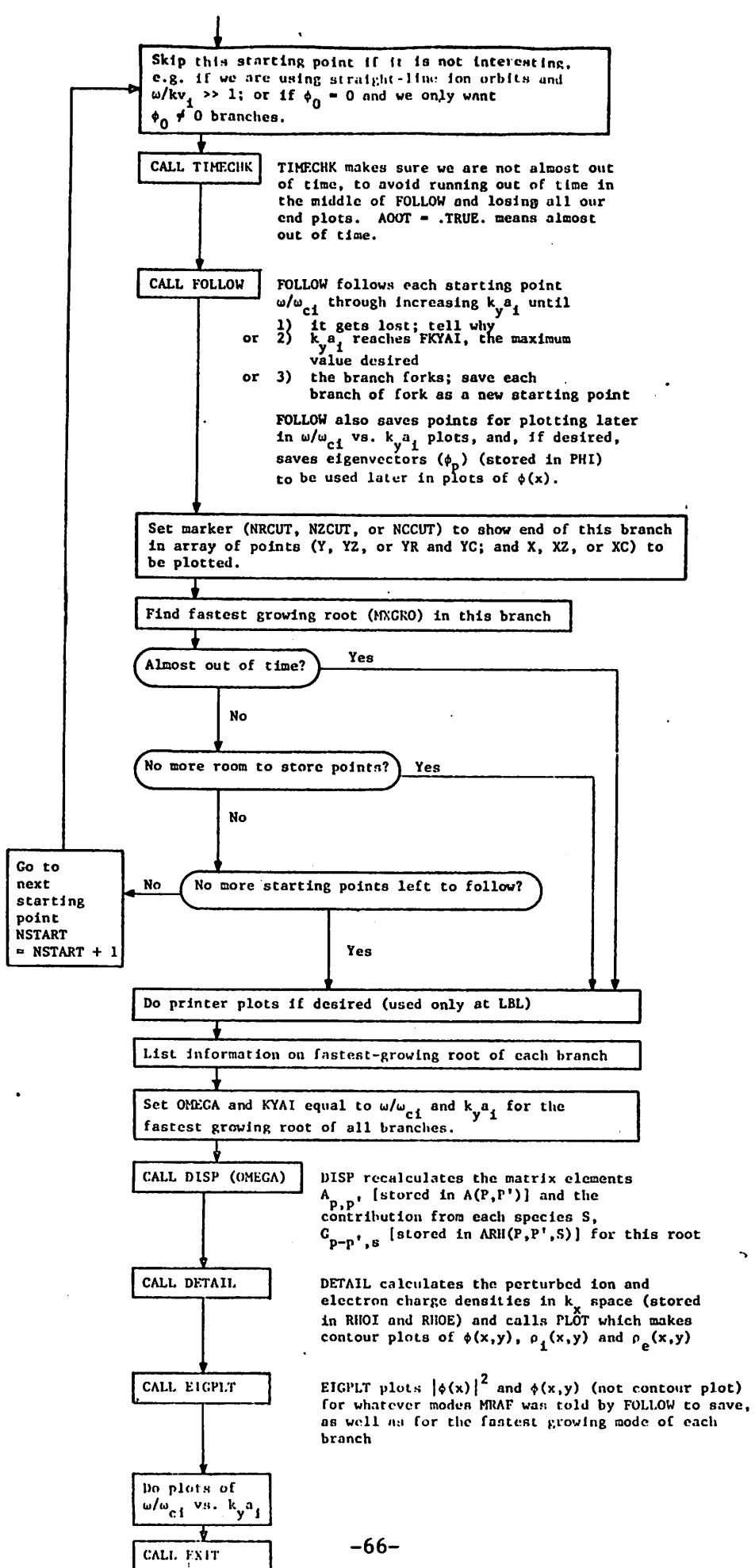
The subroutine MRAF evolved from a root-finding routine published by Rodman¹⁶ and revised by Whitley¹⁷, using a method developed by Muller and Traub¹⁸, a second order iterative method analogous to the secant method. The published version was further revised by one of us (A.B.L.) and used as a subroutine in the first version of ROOTS (written by C.K.B., D.F., and A.B.L.). Several additions and changes to ROOTS and its subroutines were made by M.J.G., including:

- 1) Extension of the dispersion function routine DISP and its subroutines to include Maxwellian and loss cone distributions [only ring distributions, $g_s(v_\perp, v_\parallel, x) \propto \delta(v_\perp - v_0)$, were used in the first version], and to include many species (e.g. deuterium ring and tritium Maxwellian).
- 2) Use of possible symmetry of dispersion function around imaginary axis [i.e. $\det A_{p,p'}(\omega) = \det A_{p,p'}(-\omega^*)$] in finding roots (symmetry around real axis was used in published version of MRAF¹⁶).
- 4) Optional boundary to region of complex plane in which MRAF can search for roots. When the root-search goes beyond this boundary, the search ends (say at point x_i) and the function is divided by $(x-x_i)$. Eventually the boundary is surrounded by poles, and the root-search tends to stay away from the boundary and find all the roots inside.
- 5) Dividing up of complex plane into several regions, each searched separately by MRAF. This greatly reduces the number of roots missed by MRAF, if a large area of the complex plane, with a large number of roots, is to be searched.
- 6) Modifications in criteria for convergence (i.e. for having found a root) in MRAF, necessary when there are many roots close together.
- 7) Use of eigenfunctions (ϕ_p) as a criterion for convergence in MRAF.

- 8) Option for using straight line ion orbits in calculating the dispersion function.
- 9) Implementation of subroutine FOLLOW to follow each branch $\omega(k_y)$ through increasing k_y . Use of eigenfunctions (ϕ_p) to sort out different branches.
- 10) Option which allowed ROOTS to find $\omega(k_y)$ for an infinite medium with constant $(1/n) dn/dx$, using the local approximation [i.e., $D(x=0, \omega, k_x=0) = 0$] rather than finding normal modes.

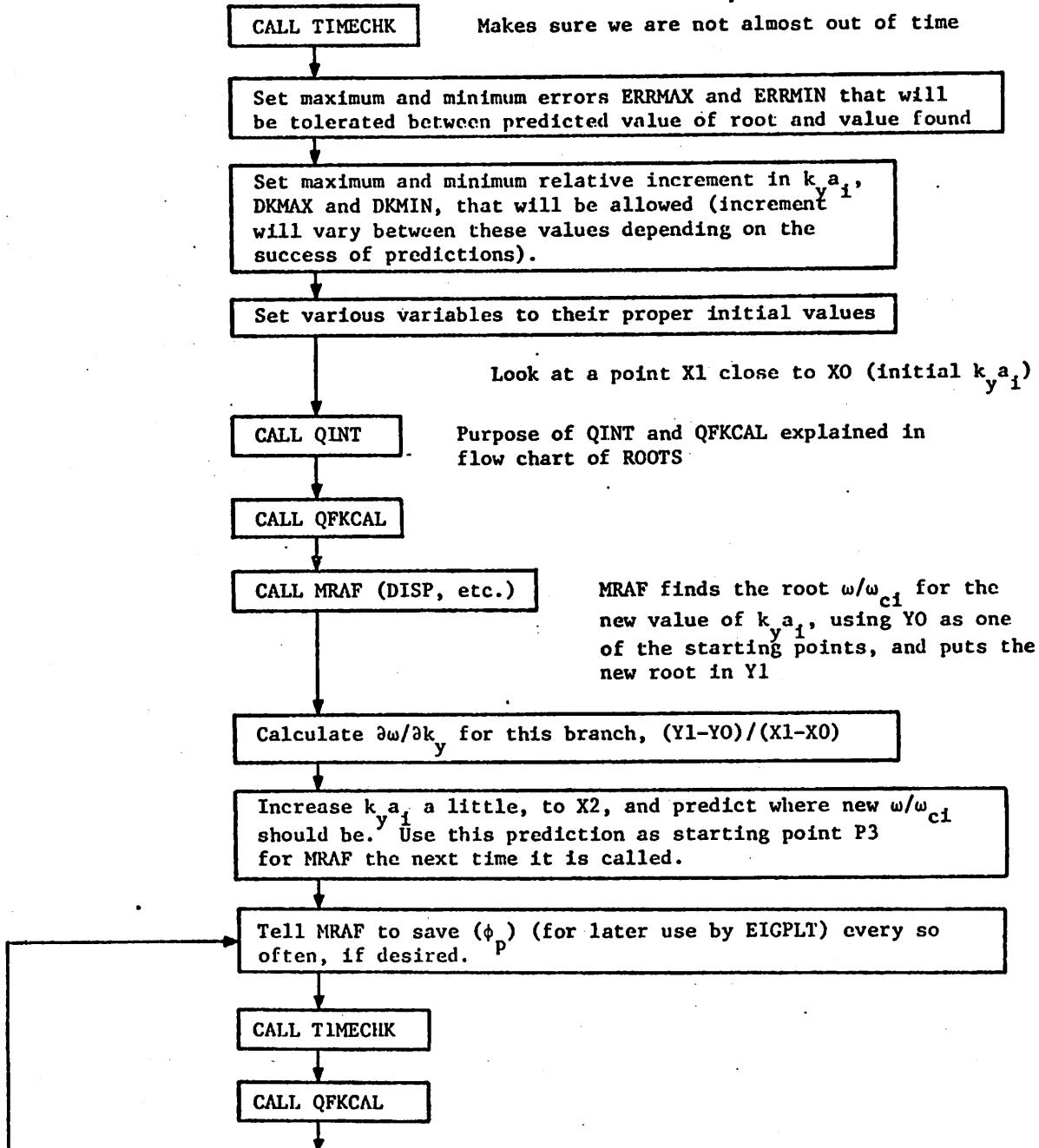
FLOW CHART OF ROOTS





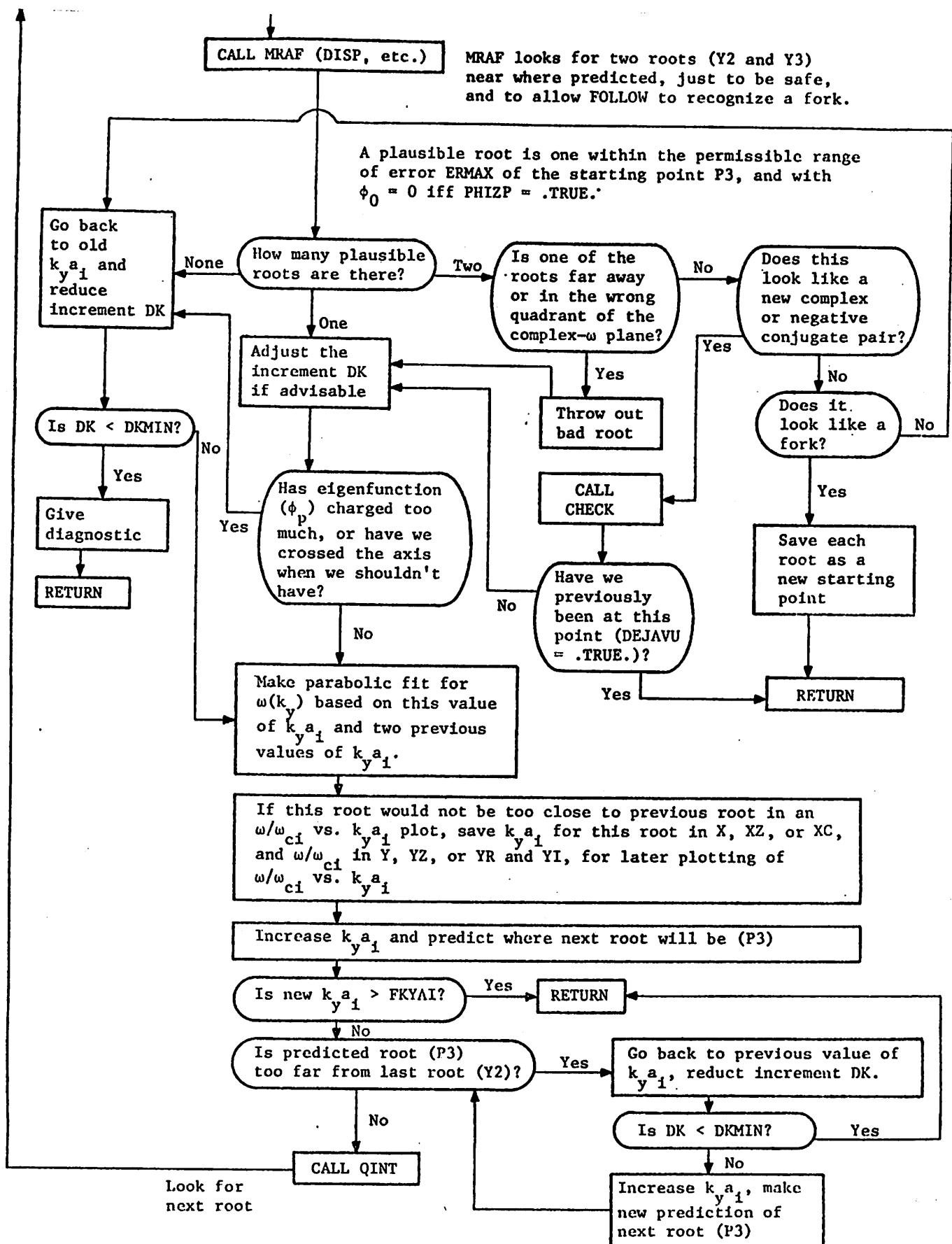
FLOW CHART OF FOLLOW (X0, Y0, PHIZP)

X0 is the k_{y_i} of the starting point
 Y0 is the ω/ω_{ci} of the starting point
 PHIZP = .TRUE. iff $\phi_0 = 0$ for this branch (useful, since
 this is a property which does not change for a given branch
 as k_{y_i} changes)

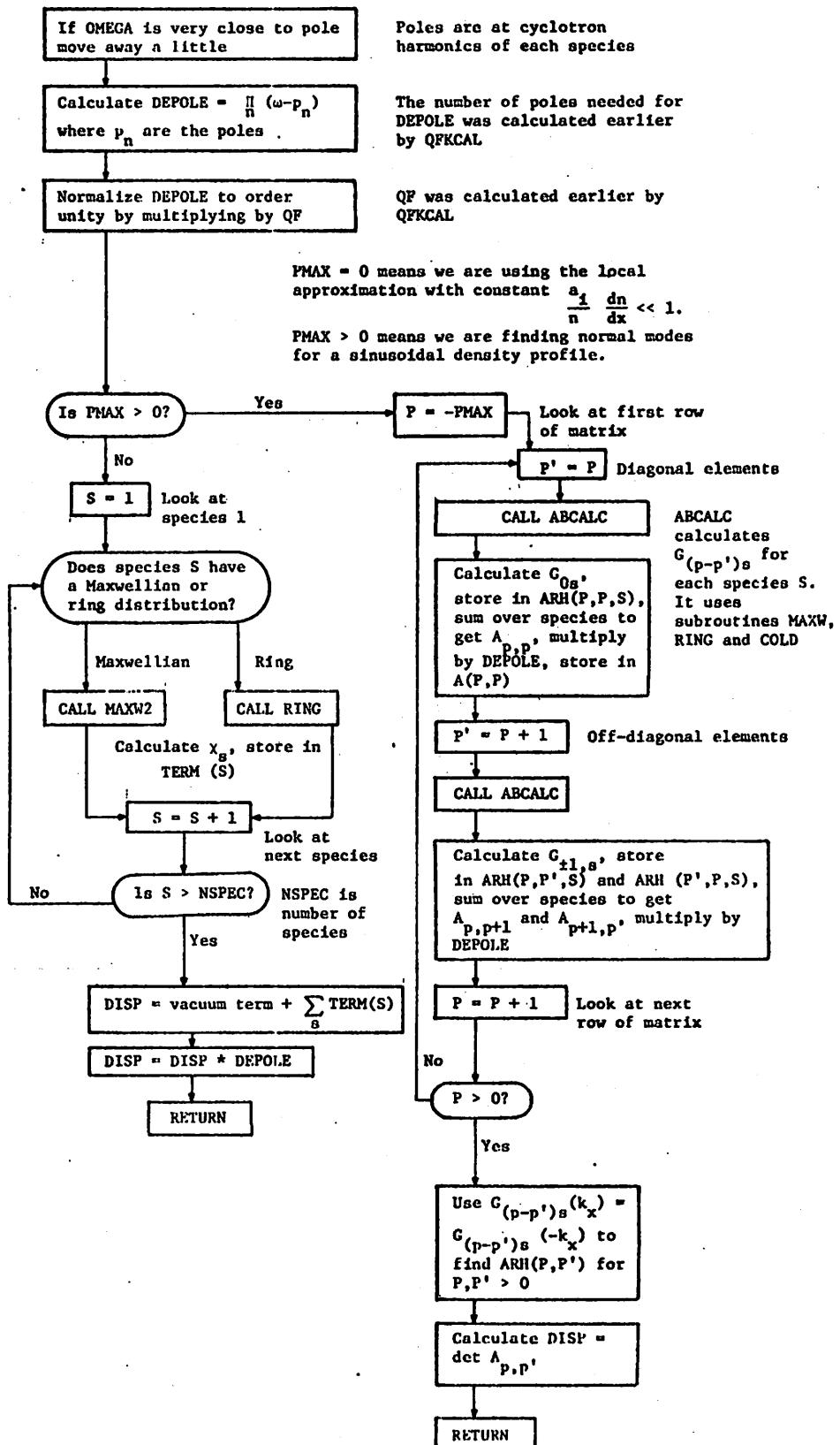


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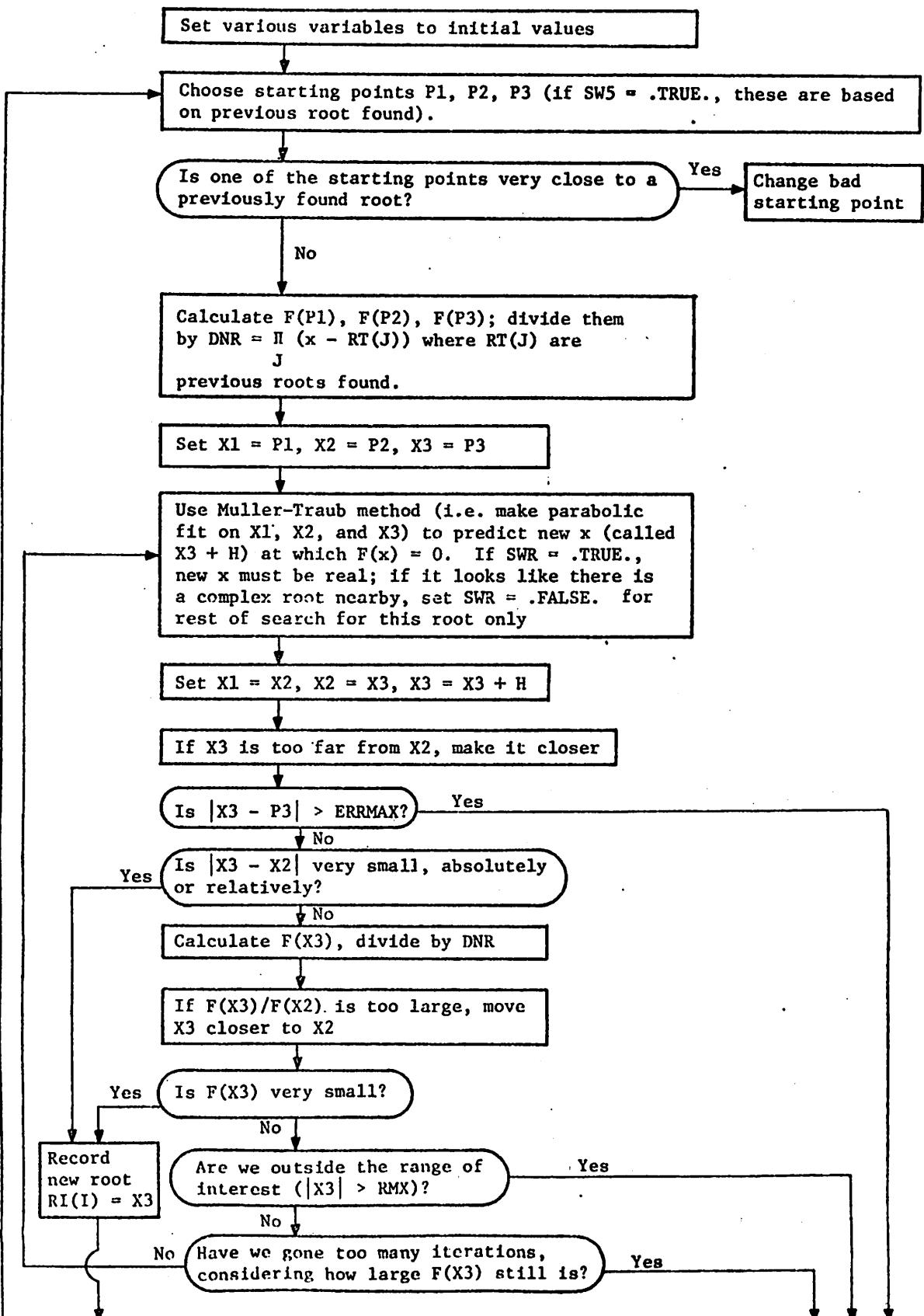


FLOW CHART OF DISP (OMEGA)



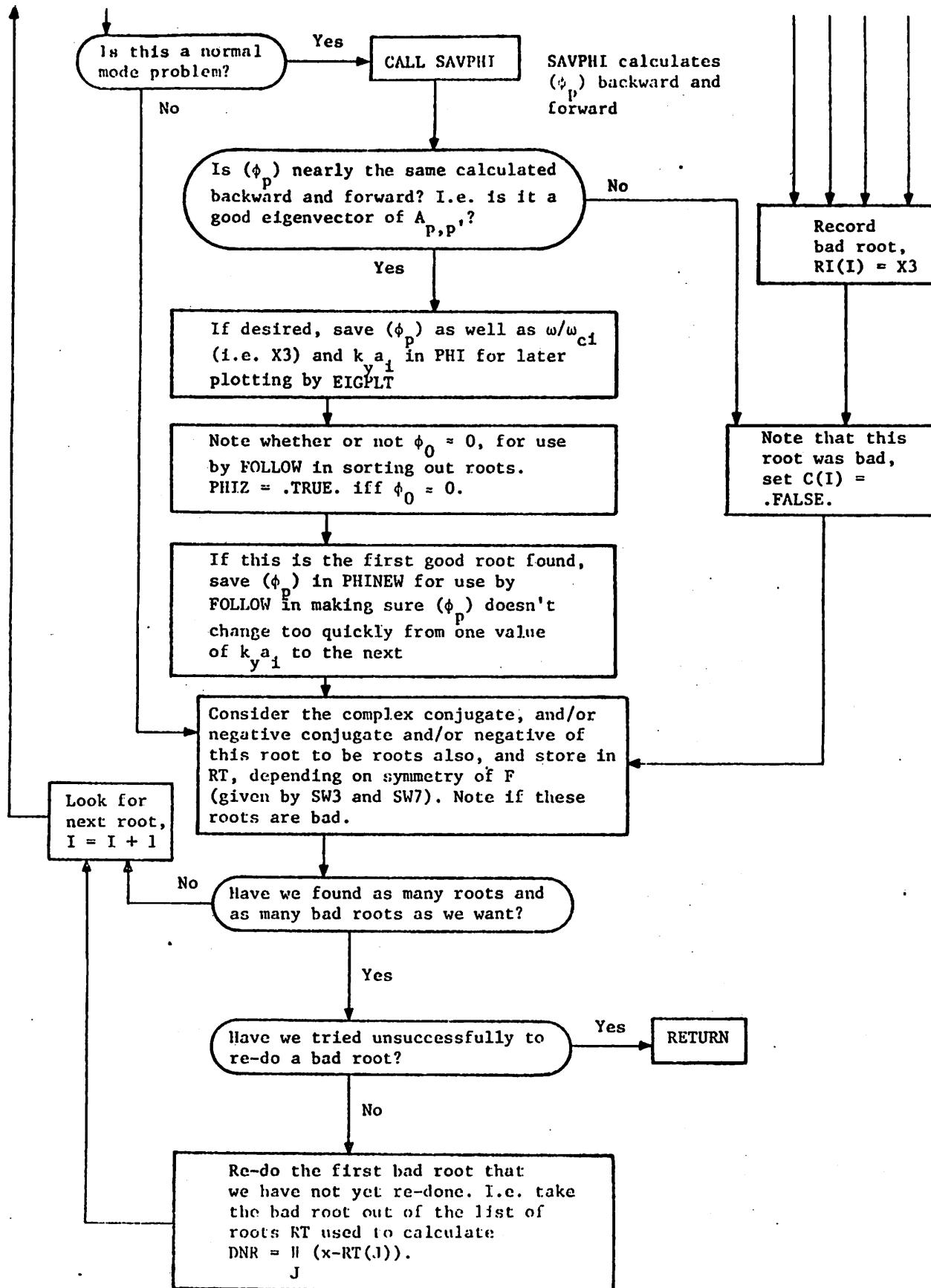
FLOW CHART OF MRAF (F, etc.)

F is the function which MRAF is finding the zeroes of



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Listing of ROOTS and Subroutines

The version of ROOTS listed here runs on the A-machine (a CDC 7600) of the National Magnetic Fusion Energy Computer Center at Lawrence Livermore Laboratory, using the NEW1 compiler (which differs from the better known CHATR compiler in that it does complex division correctly), and the libraries ORDERLIB, CF76LIB, and TV80LIB. Features differing from standard Fortran include I/O (especially graphics routines), tests to see if the time limit has nearly been reached (OOTIM) and treatment of logical variables.

Although the code originated at Livermore, it spent a number of its formative years at Lawrence Berkeley Laboratory (growing from 600 to nearly 3000 cards) and it still contains a number of archaic features from its Berkeley days (e. g. the routines SGNL and WARN).

It is hoped that this code, which should be useful for a wide range of problems, will be made available to the users of the A-machine in the not too distant future, after it has been cleaned up and documented.

C-170A BOX B05 13.28.56 06/17A 1976
 000001 PROGRAM ROOTS(INPUT,HSP,OUTPUT,TAPE10=OUTPUT)
 C THE FOLLOWING CHANGES SHOULD BE MADE IN *ROOTS* AND THE SUBROUTINES
 000002 EVENTUALLY, BUT I HAVE NOT HAD TIME TO MAKE THEM YET, AND PROBABLY WILL NOT
 000003 FOR QUITE A WHILE -MJG.
 000004 1) *RING2*, THE SUBROUTINE USED FOR RING DISTRIBUTIONS WITH THE
 000005 LOCAL APPROXIMATION IS NOT WORKING CORRECTLY AND SHOULD BE CORRECTED
 000006 2) DIFFUSION HAS NOT YET BEEN IMPLEMENTED WITH THE NON-LOCAL (PMAX=0) DISPERSION RELATIONS
 000007 3) THE UNMAGNETIZED PARTICLES OPTION (UNMAG=.TRUE.) HAS NOT YET BEEN
 000008 IMPLEMENTED FOR RING DISTRIBUTIONS, ONLY FOR MAXWELLIAN AND LOSS CONE
 000009 DISTRIBUTIONS.
 000010 4) SO FAR *MRAF* HAS WORKED QUITE WELL IN FINDING THE STARTING POINTS
 000011 BUT IT MIGHT NOT BE SO EFFICIENT (I.E. IT MIGHT MISS ROOTS) IN
 000012 FARTHER REACHES OF PARAMETER SPACE. IN THIS CASE IT MIGHT BE
 000013 NECESSARY TO USE A NYQUIST TECHNIQUE SUCH AS CALLEN USED IN HIS
 000014 THESIS TO DETERMINE HOW MANY ROOTS THERE ARE AND THEIR APPROXIMATE
 000015 LOCATIONS, RATHER THAN THE BLIND HUNTING OF *MRAF*.
 000016 *MRAF* IS PRESENTLY NOT VERY GOOD AT FINDING ROOTS FAR FROM
 000017 THE REAL AXIS, HENCE SKYAI MUST BE SET LOW, TO BE SURE OF NOT
 000018 MISSING ANY ROOTS. IF *MRAF* WERE IMPROVED BY THE METHOD SUGGESTED
 000019 ABOVE, SKYAI COULD BE SET HIGHER, AND CONSIDERABLE TIME SAVED
 000020 (LIKE 75 PERCENT) SINCE MOST TIME IS NOW SPENT AT LOW VALUES OF KYAI.
 000021 5) *MRAF* SOMETIMES BLOWS UP WHEN NRTS IS SET TOO HIGH. THIS HAS BEEN
 000022 PREVENTED BY ARBITRARILY NOT LETTING NRTS BE MORE THAN 100, BUT
 000023 THE UNDERLYING PROBLEMS SHOULD BE FOUND AND CORRECTED.
 000024 6) MAKE *ZEE* MORE EFFICIENT AND MORE ACCURATE. RIGHT NOW IT IS NEITHER
 000025 FOR ABS(X) BETWEEN 5.0 AND 5.7, AND ROOTS OCCASIONALLY GET LOST
 000026 7) AESTHETIC IMPROVEMENTS, E.G. MAKE *MRAF* AND *FOLLOW* A GENERAL
 000027 ROOT-FINDER AND ROOT-FOLLOWER, NOT LIMITED TO THIS PARTICULAR
 000028 PROGRAM AND PROBLEM. SORT OUT THE COMMON BLOCKS SO EACH SUBROUTINE
 000029 ONLY HAS ACCESS TO WHAT IT NEEDS. DON T PUT VARIABLES IN COMMON
 000030 WHEN THEY REALLY SHOULD BE ARGUMENTS OF SUBROUTINES, AND VICE VERSA.
 000031
 000032
 000033
 000034
 000035 EXTERNAL DISP
 000036 LOGICAL C(200)
 000037 LOGICAL PHIZ(200), ZEH(100)
 000038 LOGICAL WARN, A00T
 000039 LOGICAL SW(6), SW7, SW71, SW31, OPT(10)
 000040 LOGICAL UNMAG, SINGLX, G00D, PRDAMP, SNGLX
 000041 COMPLEX QMAX, DISP, ZERO, ZERO, A(20,20), PHI(18,22)
 000042 COMPLEX RT(200), YSTART, Y2
 000043 COMPLEX P1, P2, P3
 000044 COMPLEX H, ROOT, FUNC, FR00T
 000045 COMPLEX DF0W, D2FDK2, DF0X, D2WDK2, DWDX
 000046 INTEGER RTC
 000047 INTEGER P, PMAX, QMAX, EIGV, RMAX, RMAX1
 000048 REAL MASS, KOAI, KOSQ, KYAI, KYSQ, MASQ, IQ, KOAE, KXSQ
 000049 DIMENSION X(2000), Y(2000), XC(1000), YR(1000), YI(1000), XZ(4000),
 . YZ(4000), XPL0T(501), YPL0T(501)
 000050 DIMENSION NRCUT(100), NCUT(100), NZCUT(100), MXGR0(100), SIDE(100)
 000051 DIMENSION RH(4), XLR(100), XLC(100)
 000052 DIMENSION ABSPHI(20), ANGPHI(20)
 000053 COMMON/C10/ICR, IHSP, IGRAPH
 000054 COMMON/CMRAF/SW, RTC, ITC, EP3, FRMAX, XRMAX, H, ROOT, FUNC, FR00T, EIGV,
 000055 SW7, START, RHIGH, NFL, CYA1
 000056 COMMON/CMRAF2/ ERRMAX, NRTSU, SW31, SW71
 000057 COMMON/CRBESJ/ QMAX(4), NMAX(4)
 000058 COMMON/PMX/NPP
 000059 COMMON/CNSP/ NSP, NSP1
 000060 COMMON/DIS/QF, KYSQ, KOSQ, EPSF(4), MASS, KYAI, KOAI, MASQ, PMAX, OMPSQ
 000061 . AEA1, KMAX(4), AMASQ(4), EPS(4), KMIN(4)
 000062 COMMON/CPARAM/ RMAX, AIL, EPS1, EPSE, NSPEC, DFUI, DFUE, EP, SINGLX, XL(10
 .) , NXL
 000063 COMMON/CRGAM/R, GAM, RE, GAME, R1, RE1, AEA11
 000064 COMMON/CFAST/ DK, FKYAI, NPTC, YI, YR, XC, KYD, YM
 000065 . YZ, XZ, Y, X, NPT, NPTZ, ZEH, IGV, A00T, NF0L, FKYAI2, RMIN, YM
 000066 COMMON/CF0L/YSTART(100), XSTART(100), NSTART, YEND(100), XEND(100),
 000067 NSTRT1
 000068 COMMON/CCHECK/XCRIT(100), YCRIT(100), NCRT, DEJAVU, Y2, NN, PZCRIT(100)
 000069 COMMON/CQN/MIN
 000070 COMMON/CSPEC/ RLARM(4), AMASS(4), CHARG(4), JAY(4), DENSE(4), NSPEC
 000071 COMMON/CDFU/ DFU(4), DR0L(4)
 000072 COMMON/PHIC/ A, NRTSV, PHI
 000073 COMMON/F0LE1G/ G00D(18), IBRANCH(18)
 000074 COMMON/CTVY/ TVY
 000075 COMMON/TVP00L/XMIN, XMAX, YMIN, YMAX, TVXMIN, TVXMAX, TVYMIN, TVYMAX
 000076 COMMON/TVTUNE/LPENON, LPENOFF, ITALICS, IWINK, INTENSE, IRIGHT, IUP
 000077 COMMON/TVGUIDE/ TVMODE, TEXTURE, ITV
 000078 COMMON/CPHZ/PHIZ
 000079 COMMON/CXK/XKO
 000080 COMMON/CMAG/UNMAG
 000081 COMMON/CKXSQ/ KXSQ
 000082 COMMON/CBETA/ BETA
 000083 COMMON/CSNGLX/ SINGLX
 000084 DATA ICR, IHSP, IGRAPH/2, 10, 100/
 000085 DATA RLARM/1., 3*0., AMASS/4*1., CHARG/2*1., 2*(-1.), JAY/4*0/,
 000086 DENSE/1., 0., 1., 0./
 000087 DATA AMASQ/4*1./
 000088 DATA NR, NC, NZ/3*1/
 000089 DATA KM1N/4*1/
 000090
 000091

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000092 DATA DFU/4*0./
000093 DATA TEXTURE/0./
000094 DATA PRDAMP/. TRUE./
000095 CALL DROPPFILE
000096 ELAPSED = 0
000097 CALL TIMECHK(A00T,0.,ELAPSED)
000098 CALL KEEPS0(10HR00TP0TA0)
000099 KXSQ = 0,
000100 CALL FRAME(1)
000101 NRCUT(1) = 0
000102 NZCUT(1) = 0
000103 NCCUT(1) = 0
000104 PI = 3.14159265359
000105 C IF WE WISH TO USE THE LOCAL APPROX. AT A SINGLE VALUE OF X/L, THEN
000106 C WE SET PMAX = 0 AND SINGLX = .TRUE. THEN THE DENSITY GRADIENT IS
000107 C GIVEN BY EPS(1) OR EP. WHILE AIL, EPSI, NXL, AND UNMAG ARE IGNORED.
000108 C IF SINGLX = .FALSE. AND PMAX = 0, THEN WE USE A LOCAL DISPERSION RELATION
000109 C AT NXL (UP TO 10) DIFFERENT VALUES OF X/L, GIVEN BY XL, WHILE EPS(1)
000110 C EP ARE IGNORED. IF UNMAG = .FALSE., THE USUAL LOCAL APPROX. DISP. REL. IS
000111 C USED, VALID FOR SMALL AIL. IF UNMAG = .TRUE., WE USE A DISP. REL. VALID
000112 C FOR ALL AIL, BUT ONLY FOR GROWTH RATE GREATER THAN ION CYCLOTRON FREQUENCY
000113 C (I.E. ALL WARM PARTICLES ARE UNMAGNETIZED, NOT YET IMPLEMENTED FOR
000114 C RING DISTRIBUTIONS.)
000115 C IF PMAX.GT.0, WE USE THE NON-LOCAL DISP.REL. (DEVELOPED BY LANGDON)
000116 C A SINUSOIDAL DENSITY PROFILE, AND SINGLX, NXL, XL, AND EP ARE
000117 C IGNORED.
000118 C OPT(1), OPT(2), ETC. ARE VARIOUS OPTIONS WHICH MAY BE TRUE(1) OR FALSE(0).
000119 C OPT(1) MEANS THAT ROOTS WITH PHI(0) = 0. WILL NOT BE FOLLOWED.
000120 C OPT(2) MEANS THAT, IF UNMAGNETIZED IONS ARE USED, ONLY ROOTS WITH
000121 C PHASE VELOCITY LESS THAN ION THERMAL VELOCITY WILL BE FOLLOWED.
000122 C READ(ICR,121)SINGLX,UNMAG,NXL,(OPT(I),I=1,10)
000123 121 FORMAT(2A1,I2,10I1)
000124 IF(SINGLX,EQ.1HT) SINGLX = .TRUE.
000125 IF(UNMAG,EQ.1HT) UNMAG = .TRUE.
000126 IF(UNMAG,EQ.1HF) UNMAG = .FALSE.
000127 IF(SINGLX,EQ.1HF) SINGLX = .FALSE.
000128 IF(.NOT.SINGLX) READ(ICR,122) (XL(I),I=1,NXL)
000129 122 FORMAT(10F5.5)
000130 SINGLX = SINGLX
000131 IF(SINGLX) NXL = 1
000132 C RMAX IS NUMBER OF CYCLOTRON HARMONICS WANTED, PMAX*K0 IS ESSENTIALLY
000133 C A CUTOFF IN KX, SEE MRAF FOR DEF. OF EIGV (BUT EVEN IF EIGV = 2, PHI(X)
000134 C IS PLOTTED FOR FASTEST-GROWING ROOT OF EACH BRANCH). SKYAI AND FKYAI ARE
000135 C LIMITS OF KYAI, DK IS INCREMENT OF KYAI. AIL IS RATIO OF LARMOR RADIUS TO
000136 C LENGTH OF PLASMA, AEAI IS RATIO OF ELECTRON TO ION LARMOR RADIUS,
000137 C OMPSQ IS (PLASMA FREQ./GYROFREQ.)**2, MASS IS ION TO ELECTRON MASS RATIO
000138 C DFUI AND DFUE ARE ION AND ELECTRON DIFFUSION COEFFICIENTS, EP IS THE
000139 C DENSITY GRADIENT IF WE ARE USING THE LOCAL APPROXIMATION WITH THE SAME
000140 C GRADIENT FOR ALL SPECIES.
000141 C IF NSW1.NE.0, INFORMATION ON EACH ROOT IS PRINTED OUT, FOR KYAI = SKYAI
000142 C IF NPRNT.NE.0, A PRINTER PLOT IS MADE (IN ADDITION TO CRT PLOT).
000143 C IF NOCRT.NE.0, NO CRT PLOTS ARE MADE.
000144 C IF THERE IS ONLY ONE SPECIES OF IONS, RING, MAXWELLIAN, OR LOSS CONE
000145 C THEN SET NSPEC = 0. IF THERE IS MORE THAN ONE SPECIES, OR A MORE
000146 C COMPLICATED DISTRIBUTION, THEN NSPEC IS THE NUMBER OF MAXWELLIAN
000147 C COMPONENTS OR RING COMPONENTS, INCLUDING THOSE OF ELECTRONS. (E.G. LOSS
000148 C CONE IONS AND MAXW, ELECTRONS WOULD REQUIRE NSPEC = 2 + 1 = 3)
000149 C IF NSPEC.GT.0, THEN MASS, R, GAM, RE, GAME, AEAI, EP, DFUE, AND DFUI ARE
000150 C IGNORED, BUT DUMMY VALUES MUST BE READ IN.
000151 C ELECTRONS MUST BE READ IN LAST, MUST HAVE LESS THAN ONE TENTH THE MASS
000152 C OF SPECIES 1, AND MUST HAVE CHARGE -1
000153 C IRMIN IS THE LOWEST FREQUENCY LOOKED AT (IN TERMS OF THE CYCLOTRON FREQ.)
000154 C READ(ICR,2) RMAX,PMAX,EIGV,SKYAI,DK,FKYAI,NSW1,NPRNT,NOCRT,NSPEC,!
000155 C .RMIN
000156 2 FORMAT(3I5,3F5.3,5I5)
000157 C NPP = 2*PMAX + 1
000158 C IF WE ARE EXECUTING SEVERAL RUNS ON ONE JOB, WE MAY BE OUT OF TIME
000159 C AT THE BEGINNING OF THIS RUN, SO CHECK TO SEE IF THIS IS THE CASE.
000160 C CALL TIMECHK(A00T,0.,ELAPSED)
000161 C IF(A00T) CALL EXIT
000162 C NSPEC = NSPEC
000163 C READ(ICR,5) AIL,AEAI,OMPSQ,EPSI,MASS,EP,DFUI,DFUE,BETA
000164 5 FORMAT(9F5.0)
000165 C RE AND GAME REFER TO ELECTRONS. SEE RH CALC.
000166 C READ(ICR,12) R,GAM,RE,GAME
000167 12 FORMAT(4F5.3)
000168 C IF WE ARE USING MANY SPECIES OF PARTICLES (NSPEC.GT.0), READ IN THE
000169 C LARMOR RADIUS, MASS, CHARGE, PARTICLE DENSITY AND PARAMETER J FOR EACH
000170 C SPECIES, WHERE F(VPERP) = CONST.*.(VPERP**J)*MAXWELLIAN
000171 C ALSO, THE DENSITY GRADIENT EPS, AND DIFFUSION COEFFICIENT DFU.
000172 C FOR NONLOCAL (PMAX.GT.0) CASE, EPS IS THE DENSITY VARIATION FOR EACH ION
000173 C SPECIES. IF EPS IS LEFT BLANK, IT IS SET EQUAL TO EPSI.
000174 C IF(NSPEC.LE.0) GO TO 82
000175 C IF(NSPEC.GT.4) NSPEC = 4
000176 C DO 83 I = 1, NSPEC
000177 C READ(ICR,84) RLARM(I),AMASS(I),CHARG(I),DENSE(I),JAY(I),EPS(I),DFU
000178 C .(I)
000179 C 84 FORMAT(4F10.5,15,2F10.5)
000180 C AMASQ(I) = AMASS(I)**2
000181 C IF(EPS(I).EQ.0..AND.PMAX.GT.0) EPS(I) = EPSI
000182 C NSP IS THE NUMBER OF ION SPECIES, USED IN CALCULATING EPSE. IF SPECIES
000183 C I IS ELECTRONS, THEN NSP = I - 1
000184 C IF(AMASS(I).LT..1*AMASS(I).AND.CHARG(I).EQ.-1.) NSP = I - 1
000185 C 83 CONTINUE
000186 C GO TO 89

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000187      82 NSPEC = 4
000188      NSP = 2
000189      DFU(1) = DFUI
000190      DFU(2) = DFUI
000191      DFU(3) = DFUE
000192      DFU(4) = DFUE
000193      D0 108 I = 1,4
000194      IF(PMAX.GT.0.AND.I.LE.NSP) EPS(I) = EPSI
000195      108 IF(PMAX.EQ.0) EPS(I) = EP
000196      AMASS(3) = 1./MASS
000197      AMASQ(3) = AMASS(3)**2
000198      IF(R.LE.0.) GO TO 98
000199      DENSE(1) = R/(R - GAM)
000200      DENSE(2) = -GAM/(R - GAM)
000201      RLARM(2) = 1./SQRT(R)
000202      GO TO 90
000203      98 JAY(1) = -1
000204      90 IF(AEAI.EQ.0.) GO TO 89
000205      RLARM(3) = AEA1
000206      IF(RE.LE.0.) GO TO 99
000207      DENSE(3) = RE/(RE - GAME)
000208      DENSE(4) = -GAME/(RE - GAME)
000209      RLARM(4) = AEA1/SQRT(RE)
000210      AMASS(4) = AMASS(3)
000211      AMASQ(4) = AMASQ(3)
000212      GO TO 89
000213      99 JAY(3) = -1
000214      89 FKYAI2 = FKYAI
000215      IF (PMAX.EQ.0) EIGV = 0
000216      IF(EIGV.LT.2) EIGV = 0
000217      IGV = EIGV
000218      AEA11 = AEA1
000219      IF(R.GT.0.) R1 = 1./SQRT(R)
000220      IF(RE.GT.0.) RE1 = 1./SQRT(RE)
000221      KOAI = 2.0*PI*AIL
000222      KOSQ=KOAI*KOAI
000223      NSP1 = NSP + 1
000224      C CALCULATE THE ELECTRON GUIDING CENTER DENSITY GRADIENT EPSE NEEDED TO
000225      C NEUTRALIZE IONS WITH GUIDING CENTER DENSITY GRADIENT EPSI.
000226      C FIRST FIND RATIO OF OSCILLATING PART OF PARTICLE DENSITY TO OSCILLATING
000227      C PART OF GUIDING CENTER DENSITY FOR EACH SPECIES.
000228      101 D0 93 I = 1, NSPEC
000229      KOAE = KOAI*RLARM(I)
000230      RM = 1.
000231      IF(JAY(I).LT.0) RM = 0.
000232      93 CALL RHCALC(RM,0,KOAE,RH(I))
000233      C THEN FIND THIS RATIO (TIMES TOTAL ION CHARGE DENSITY) FOR IONS AS A WHOLE
000234      RHEI = 0.
000235      D0 94 I = 1, NSP
000236      94 RHEI = RHEI + DENSE(I)*CHARG(I)*RH(I)*EPS(I)
000237      C THEN FIND FOR ELECTRONS AS A WHOLE.
000238      RHEE = 0.
000239      D0 95 I = NSP1, NSPEC
000240      95 RHEE = RHEE - DENSE(I)*CHARG(I)*RH(I)
000241      EPSE = RHEI/RHEE
000242      D0 96 I = 1, NSP
000243      96 EPSF(I) = .5*EPS(1)*OMPSQ*CHARG(I)**2*DENSE(I)/AMASS(I)
000244      D0 97 I = NSP1, NSPEC
000245      97 EPSF(I) = .5*EPSE*OMPSQ*CHARG(I)**2*DENSE(I)/AMASS(I)
000246      C PRINT OUT PARAMETERS
000247      103 CALL PARAM(99)
000248      PRINT 7,IRMIN,RMAX
000249      7 FORMAT(40H ROOTS FOUND BETWEEN CYCLOTRON HARMONICS,13,4H AND,13)
000250      MASQ = MASS*MASS
000251      NPT = 0
000252      NPTC = 0
000253      NPTZ = 0
000254      NFOL = 0
000255      YMX = FLOAT(RMAX) + .5
000256      D0 114 IXL = 1, NXL
000257      ERRMAX = 1.E+20
000258      RMX = FLOAT(RMAX) + .5
000259      RHIGH = RMX
000260      RMIN = IRMIN
000261      IF(NSW1.NE.0) SW(1) = .TRUE.
000262      C.....COMPLEX CONJUGATES ARE ALSO ROOTS, IF THERE IS NO DIFFUSION
000263      SW(3) = .TRUE.
000264      D0 107 I = 1, NSPEC
000265      107 IF(DFU(I).GT.0) SW(3) = .FALSE.
000266      IF(UNMAG) SW(3) = .FALSE.
000267      SW(4)=.TRUE.
000268      SW(5) = .TRUE.
000269      IF(UNMAG) SW(5) = .FALSE.
000270      C PMAX = 0 MEANS WE ARE USING A LOCAL APPROXIMATION, IF NOT USING A
000271      C LOCAL APPROX., THEN A ROOT AT OMEGA IMPLIES A ROOT AT -OMEGA*.
000272      IF(PMAX.GT.0) SW7 = .TRUE.
000273      KYAI = SKYAI
000274      KYSQ=KYAI*KYAI
000275      CYAI = KYAI
000276      CHI = KYSQ + PMAX*PMAX*KOSQ
000277      MINQ = 2*RMAX
000278      CALL QINT(CHI)
000279      C IF THE RANGE OF FREQ. WE ARE INTERESTED IN (RMX - RMIN) IS TOO LARGE
000280      C FOR *MRAF* TO HANDLE, WE BREAK IT INTO REGIONS OF CH CYCLOTRON HARMONICS
000281      C AND LOOK AT ONE REGION AT A TIME.
000282      CH = 5.
000283      RLW = RMIN
000284      105 RHIGH = RMX

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000285      IF(RHIGH - RLOW.GT.CH+.5) RHIGH = RLOW + CH + .5
000286      C CALCULATE QF, KMAX, AND KMIN (USED IN *DISP*)
000287      C CALL QFKCAL(QF,KMAX,KMIN,RHIGH,RLOW)
000288      C HOW MANY POLES ARE THERE.
000289      NPOLES = 0
000290      DO 92 I = 1, NSPEC
000291      92 NPOLES = NPOLES + KMAX(I) - KMIN(I) + 1
000292      C IF THE NUMBER OF ROOTS (CONVERGED OR NOT) EXCEEDS NRTS, OR THE NUMBER
000293      C OF UNCONVERGED ROOTS (NOT COUNTING NEGATIVES AND CONJUGATES) EXCEEDS NFL,
000294      C IT IS NOT WORTHWHILE TO LOOK FOR MORE ROOTS (DETERMINED EMPIRICALLY)
000295      NRTS = 2*NPP*(NPOLES + 3*NSPEC - 3)
000296      NFL = NPP*NPOLES + NPOLES
000297      IF(UNMAG) NRTS = 10*NPP
000298      IF(UNMAG) NFL = 10*NPP
000299      IF(NRTS.GT.200) NRTS = 200
000300      IF(NRTS.GT.100) NRTS = 100
000301      IF(PMAX.GT.0) GO TO 117
000302      IF(SINGLX) GO TO 116
000303      C DREL(I) IS THE RELATIVE DENSITY, N(X)/NO FOR SPECIES I
000304      C EPS(I) IS THE LOCAL DENSITY GRADIENT OF SPECIES I
000305      CALL XLSET(XL(ILX),XKO,EPSI,EPSE,NSP,NSP1,NSPEC,EPS,DREL,RH,KOAI)
000306      GO TO 117
000307      116 DO 118 I = 1, NSPEC
000308      118 DREL(I) = 1.
000309      117 CONTINUE
000310      C STARTING VALUES FOR ROOT SEARCH. IF THESE ARE TOO CLOSE TOGETHER,
000311      C IT TAKES TOO LONG TO CONVERGE TO A ROOT.
000312      START = 0.
000313      IF(UNMAG) GO TO 112
000314      P1 = -1.952 + RLOW
000315      P2 = -0.951 + RLOW
000316      P3 = 0.051 + RLOW
000317      GO TO 113
000318      112 P1 = .001
000319      P2 = EPSI*RH(1)*KOAI*KYAI + .0019
000320      P3 = SQRT(EPSI*RH(1)*KOAI)*KYAI + .0027
000321      113 SW(6) = SW(3)
000322      14 CALL MRAF(DISP,RT,C,NRTS,P1,P2,P3,1.E-06,1.E-12,25)
000323      IF(SW(1)) PRINT 10, (C(I),I=1,NRTS)
000324      10 FORMAT(1X,20I5)
000325      IF(SKYAI.GE.FKYAI) GO TO 114
000326      IF(SW(1)) CALL PAGE
000327      DO 21 I = 1, RTC
000328      IF (.NOT. C(I)) GO TO 21
000329      IF(REAL(RT(I)).LT.-1.E-06,AND.SW7) GO TO 21
000330      IF(REAL(RT(I)).LT.0.,AND.SW7) RT(I) = CMPLX(0.,AIMAG(RT(I)))
000331      IF(AIMAG(RT(I)).LT.-1.E-06,AND.SW(3)) GO TO 21
000332      IF(CABS(RT(I)).LT.RLOW - 1.) GO TO 21
000333      IF(RHIGH.LT.RMX.AND.CABS(RT(I)).GT.RHIGH - 1.5) GO TO 21
000334      IF(CABS(RT(I)).GT.RMX) GO TO 21
000335      NSTART = NSTART + 1
000336      C USE THE GOOD ROOTS AS STARTING POINTS FOR *FOLLOW*.
000337      XSTART(NSTART) = KYAI
000338      YSTART(NSTART) = RT(I)
000339      ZEH(NSTART) = PHIZ(I)
000340      IF(NSTART.GE.100) GO TO 106
000341      21 CONTINUE
000342      RLOW = RLOW + CH
000343      IF(RHIGH.LT.RMX) GO TO 105
000344      NSTRT1 = NSTART
000345      C WE HAVE FOUND ALL THE STARTING POINTS. NOW PREPARE TO FOLLOW EACH ROOT.
000346      106 RHIGH = 1.E+06
000347      SW31 = SW(3)
000348      SW71 = SW7
000349      SW(3) = .FALSE.
000350      SW(4) = .FALSE.
000351      SW(5) = .FALSE.
000352      SW(6) = .FALSE.
000353      SW7 = .FALSE.
000354      56 NFOL = NFOL + 1
000355      SW(1) = .FALSE.
000356      SW(2) = .FALSE.
000357      C IF WE HAVE RUN OUT OF SPACE TO STORE ROOTS, OR HAVE FOLLOWED ALL THE
000358      C ROOTS, DO END PROCEDURES.
000359      IF(NFOL.GT.100) GO TO 55
000360      C IF WE ONLY WANT TO FOLLOW SOME OF THE ROOTS, STICK IN EXTRA CARDS HERE
000361      IF(ZEH(NFOL).AND.PMAX.GT.0.AND.OPT(1)) GO TO 56
000362      IF(REAL(YSTART(NFOL)).GT.SKYAI.AND.XSTART(NFOL).EQ.SKYAI.AND.UNMAG
000363      .AND.OPT(2)) GO TO 56
000364      IF(REAL(YSTART(NFOL)).LT.IRMIN) GO TO 56
000365      IF(.NOT.SW71.AND.UNMAG) GO TO 128
000366      IF(REAL(YSTART(NFOL)).LT.IRMIN) GO TO 56
000367      C FOLLOW THE PHI(0)=0 ROOTS BEFORE FOLLOWING THE PHI(0)=0 ROOTS, SINCE
000368      C THE FASTEST-GROWING ROOT IS MORE LIKELY TO HAVE PHI(0).NE.0.
000369      IF(.NOT.ZEH(NFOL).OR.NSTART.GE.100) GO TO 128
000370      DO 138 I = NFOL, NSTART
000371      IF(.NOT.ZEH(I)) GO TO 139
000372      138 CONTINUE
000373      GO TO 128
000374      139 NSTART = NSTART + 1
000375      XSTART(NSTART) = XSTART(NFOL)
000376      YSTART(NSTART) = YSTART(NFOL)
000377      ZEH(NSTART) = ZEH(NFOL)
000378      GO TO 56
000379      128 CALL TIMECHK(AOOT,O.,ELAPSED)

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000381 PRINT 57, NFOL, YSTART(NFOL), XSTART(NFOL), ELAPSED
000382 57 FORMAT(5H ROOT,14.19H STARTS AT OMEGA = ,2E22.13,8H KYAI = ,E22.1
000383 .3,5X,8H TIME IS,F8.3)
000384 IF(CABS2(YSTART(NFOL)).GT.1.E-12) GO TO 58
000385 PRINT 59, NFOL
000386 59 FORMAT(16H OMEGA = 0, ROOT, 14,25H NOT FOLLOWED EXPLICITLY. )
000387 GO TO 56
000388 58 CALL FOLLOW(XSTART(NFOL), YSTART(NFOL), ZEH(NFOL))
000389 PRINT 76, NFOL, Y2, KYAI
000390 76 FORMAT(5H ROOT,14,17H ENDS AT OMEGA = 2E22.13,8H KYAI = E22.13)
000391 C CLASSIFY THE ROOTS ACCORDING TO WHETHER IT IS REAL OR COMPLEX, AND AC-
000392 C CORDING TO WHETHER PHI(0) = 0 (PHIZ = .TRUE.) OR NOT. PHI(0) = 0
000393 C FOR ABOUT HALF THE ROOTS, AND THIS IS A CONVENIENT WAY OF CLASSIFYING
000394 C THEM SO AS NOT TO CONFUSE ONE ROOT WITH ANOTHER NEARBY.
000395 IF(ZEH(NFOL)) GO TO 61
000396 IF(NPT.EQ.NRCUT(NR)) GO TO 60
000397 NR = NR + 1
000398 C NRCUT, NZCUT, AND NCCUT TELL THE CRT PLOTTING ROUTINES WHEN IN THE LIST OF
000399 C POINTS ONE BRANCH ENDS AND ANOTHER BEGINS, SO CONSECUTIVE POINTS FROM
000400 C DIFFERENT BRANCHES WILL NOT BE JOINED.
000401 C NR, NRCUT, NPT FOR REAL ROOTS, PHIZ = .FALSE.
000402 C NZ, NZCUT, NPTZ FOR REAL ROOTS, PHIZ = .TRUE.
000403 C NC, NCCUT, NPTC FOR COMPLEX ROOTS
000404 NRCUT(NR) = NPT
000405 GO TO 60
000406 61 IF(NPTZ.EQ.NZCUT(NZ)) GO TO 60
000407 NZ = NZ + 1
000408 NZCUT(NZ) = NPTZ
000409 IF(PMAX.EQ.0.AND..NOT.SINGLX) XLR(NZ) = XL(IXL)
000410 60 IF(NPTC.EQ.NCCUT(NC)) GO TO 63
000411 NC = NC + 1
000412 NCCUT(NC) = NPTC
000413 IF(PMAX.EQ.0.AND..NOT.SINGLX) XLC(NC) = XL(IXL)
000414 C FIND THE FASTEST-GROWING ROOT IN THIS BRANCH
000415 INIT = NCCUT(NC-1) + 1
000416 MAXGR0 = INIT
000417 DO 130 I = INIT, NPTC
000418 IF(YI(I).GT.YI(MAXGR0)) MAXGR0 = I
000419 SIDE(NC-1) = SIGN(1.,YR(MAXGR0))
000420 MXGR0(NC-1) = MAXGR0
000421 63 IF(NCRIT.GT.100.OR.NPT.GE.2000) GO TO 550
000422 IF(NPTZ.GE.4000.OR.NPTC.GE.1000) GO TO 550
000423 C AOOT MEANS ALMOST OUT OF TIME
000424 IF(WARN(0).OR.AOOT) GO TO 109
000425 GO TO 56
000426 109 PRINT 110
000427 110 FORMAT(19H ALMOST OUT OF TIME)
000428 GO TO 55
000429 550 PRINT 104
000430 104 FORMAT(28H NO MORE ROOM TO STORE ROOTS)
000431 125 IF(PMAX.GT.0) GO TO 55
000432 NFOL = NFOL - 1
000433 IF(NXL.GT.1) PRINT 129, XL(IXL+1)
000434 129 FORMAT(6H X/L =,F5.2)
000435 114 CONTINUE
000436 55 RMX = YMX
000437 EIGV = IGV
000438 CALL TIMECHK(AOOT,0.,ELAPSED)
000439 PRINT 78, ELAPSED
000440 78 FORMAT(5X,8H TIME IS,F8.3)
000441 C FIND THE FASTEST-GROWING ROOT
000442 IF(NPTC.EQ.0) GO TO 43
000443 MAXGR0 = MXGR0(1)
000444 NC1 = NC - 1
000445 DO 42 I = 1, NC1
000446 MXGR0(I) = MXGR0(1)
000447 42 IF(YI(MXGR0(I)).GT.YI(MAXGR0)) MAXGR0 = MXGR0(I)
000448 C FIND THE MAXIMUM GAMMA/KYSQ
000449 MGAMK2 = 1
000450 GAMK2 = YI(1)/XC(1)**2
000451 DO 157 I = 2, NPTC
000452 IF(YI(I)/XC(I)**2.GT.GAMK2) MGAMK2 = I
000453 157 IF(MGAMK2.EQ.I) GAMK2 = YI(I)/XC(I)**2
000454 IF(SW(1)) CALL PAGE
000455 DO 123 I = 2, NC
000456 123 IF(NCCUT(I).GE.MAXGR0) GO TO 124
000457 124 XLGMX = XLC(I)
000458 PRINT 44, YR(MAXGR0), YI(MAXGR0), XC(MAXGR0), XLGMX
000459 44 FORMAT(29H FASTEST-GROWING ROOT, OMEGA=,2E10.3,6H KYAI=,
000460 .E10.4,7H X/L =,F6.3)
000461 PRINT 158, GAMK2, XC(MGAMK2)
000462 158 FORMAT("MAXIMUM GAMMA/KYSQ =",E12.4,"AT KYAI =",E12.4)
000463 IF(SW71.OR..NOT.UNMAG) GO TO 43
000464 IF(.NOT.PRDAMP) GO TO 160
000465 IF(NPTZ.EQ.0) GO TO 43
000466 DO 156 I = 1, NPTZ
000467 156 IF(YZ(I).GT.RMX) RMX = YZ(I)
000468 GO TO 43
000469 160 IF(SINGLX) GO TO 43
000470 IF(YR(MAXGR0).LT.0.) XLGMX = -XLGMX
000471 RMX = RMAX + .5
000472 DO 127 I = 1, NPTC
000473 IF(YR(I).LT.0) YR(I) = -YR(I)
000474 127 IF(YR(I).GT.RMX) RMX = YR(I)
000475 C DO THE PRINTER PLOTS, IF DESIRED.
000476 43 IF(NPRNT.EQ.0) GO TO 137

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000477 YINC = (RMX - RMIN)/50.
000478 XMIN = IFIX(SKYAI)
000479 RANGE = SKYAI - XMIN
000480 X RANGE = 500.
000481 IF(RANGE.LE.250.) X RANGE = 250.
000482 IF(RANGE.LE.100.) X RANGE = 100.
000483 IF(RANGE.LE.75.) X RANGE = 75.
000484 IF(RANGE.LE.50.) X RANGE = 50.
000485 IF(RANGE.LE.20.) X RANGE = 20.
000486 IF(RANGE.LE.10.) X RANGE = 10.
000487 IF(RANGE.LE. 5.) X RANGE = 5.
000488 XMAX = XMIN + X RANGE
000489 XINC = X RANGE/100.
000490 IF(PRDAMP) GO TO 154
000491 IF(UNMAG) GO TO 80
000492 154 IF(.NOT.SW(1)) CALL PAGE
000493 IF(NPT.EQ.0) GO TO 79
000494 CALL PRNPLT(X,Y,XMAX,XINC,RMX,YINC,0,0,NPT)
000495 PRINT 39
000496 CALL PAGE
000497 79 IF(NPTZ.EQ.0) GO TO 80
000498 CALL PRNPLT(XZ,YZ,XMAX,XINC,RMX,YINC,0,0,NPTZ)
000499 PRINT 39
000500 39 FORMAT(11H REAL ROOTS)
000501 CALL PARAM(99)
000502 80 IF(NPTC.EQ.0) GO TO 48
000503 IF(.NOT.SW(1)) CALL PAGE
000504 CALL PRNPLT(XC,YR,XMAX,XINC,RMX,YINC,0,0,NPTC)
000505 CALL PARAM(99)
000506 PRINT 40
000507 40 FORMAT(28H REAL PART OF COMPLEX ROOTS.)
000508 CALL PAGE
000509 YMAX = IFIX(YI(MAXGR0) + 1.)
000510 YINC = YMAX/50.
000511 CALL PRNPLT(XC,YI,XMAX,XINC,YMAX,YINC,0,0,NPTC)
000512 CALL PARAM(99)
000513 PRINT 41
000514 41 FORMAT(29H IMAG. PART OF COMPLEX ROOTS.)
000515 C FIND PHI(P) FOR THE FASTEST-GROWING MODE ON EACH BRANCH
000516 137 NC1 = NC - 1
000517 IF(NPRNT.NE.0) CALL PAGE
000518 CALL SETCH(1.,42.,1,0,1,0,0)
000519 IF(IGV.LT.2) GO TO 145
000520 DO 131 I = 1,NC1
000521 MXGR0I = MXGR0(I)
000522 OMEGA = CMPLX(YR(MXGR0I),YI(MXGR0I))
000523 KYAI = XC(MXGR0I)
000524 CYAI = KYAI
000525 KYSQ = KYAI*KYAI
000526 CHI = KYSQ + PMAX*PMAX*KOSQ
000527 MINQ = 2.*REAL(OMEGA)
000528 CALL QINT(CHI)
000529 ZERO = DISP(OMEGA)
000530 CALL SAVPHI
000531 PHI(NRTSV,NPP+1) = OMEGA
000532 PHI(NRTSV,NPP+2) = CMPLX(KYAI,0.)
000533 IF(MXGR0I.EQ.MAXGR0) CALL DETAIL(NRTSV)
000534 CALL TIMECHK(A00T,0.,ELAPSED)
000535 PRINT 78, ELAPSED
000536 SUMPHI = 0.
000537 DO 133 J = 1,NPP
000538 ABSPHI(J) = CABS(PHI(NRTSV,J))
000539 SUMPHI = SUMPHI + ABSPHI(J)**2
000540 133 IF(ABSPHI(J).NE.0.) ANGPHI(J) = 57.29*AIMAG(CL0G(PHI(NRTSV,J)))
000541 GOOD(NRTSV) = .TRUE.
000542 IBRANCH(NRTSV) = I
000543 NRTSV = NRTSV + 1
000544 PHNORM = 1./SQRT(SUMPHI)
000545 DO 132 J = 1,NPP
000546 ABSPHI(J) = ABSPHI(J)*PHNORM
000547 PRINT 136, I, OMEGA, KYAI
000548 WRITE(IGRAPH,136) I, OMEGA, KYAI
000549 136 FORMAT(31H FASTEST-GROWING WAVE OF BRANCH, 13, 9H OMEGA = ,2E21.12
000550 /8H KYAI = ,E22.13)
000551 PRINT 134, (ABSPHI(J),J=1,NPP)
000552 WRITE(IGRAPH,134) (ABSPHI(J),J=1,NPP)
000553 134 FORMAT(6E12.4)
000554 PRINT 135, (ANGPHI(J),J=1,NPP)
000555 WRITE(IGRAPH,135) (ANGPHI(J),J=1,NPP)
000556 135 FORMAT(6F12.2)
000557 WRITE(IGRAPH,159)
000558 159 FORMAT(" ")
000559 131 CONTINUE
000560 GO TO 147
000561 145 IF(SINGLX) GO TO 48
000562 DO 146 I = 1,NC1
000563 MXGR0I = MXGR0(I)
000564 KYAI = XC(MXGR0I)
000565 OMEGA = CMPLX(YR(MXGR0I),YI(MXGR0I))
000566 KYSQ = KYAI*KYAI
000567 XX = XLC(I+1)*SIDE(I)
000568 IF(XX.LT.0.) XX = XX + 1
000569 PRINT 148, I, OMEGA, KYAI, XX

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000570
000571      WRITE(1GRAPH,148) I, OMEGA, KYAI, XX
000572      FORMAT(31H FASTEST-GROWING WAVE OF BRANCH, I3, 9H OMEGA = ,2E20.12
000573      . /8H KYAI = ,E20.12,5H X/L=,F6.3)
000574      IF(.NOT.UNMAG) GO TO 146
000575      CALL XLSET(XX,XKO,EPsi,EPSE,NSP,NSP1,NSPEC,EPS,DREL,RH,KOAI)
000576      ZERO = DISP(OMEGA)
000577      DFDW = 1.E+04*DISP(OMEGA + .0001)
000578      KXSQ = .002
000579      D2FDK2 = 1.E+03*DISP(OMEGA)
000580      KXSQ = 0.
000581      XX = XX + .0001
000582      CALL XLSET(XX,XKO,EPsi,EPSE,NSP,NSP1,NSPEC,EPS,DREL,RH,KOAI)
000583      DFDX = 1.E+04*DISP(OMEGA)*A1L
000584      TRZERO = 1.E+12*CABS2(ZERO)
000585      IF(CABS2(DFDW).LT.TRZERO.OR.CABS2(D2FDK2).LT.TRZERO.OR.CABS2(DFDX)
000586      . LT.TRZERO) GO TO 151
000587      D2WDK2 = D2FDK2/DFDW
000588      Dwdx = DFDX/DFDW
000589      SPREAD = SQRT(CABS(D2WDK2)/AIMAG(OMEGA))
000590      CHANGE = CABS(OMEGA/Dwdx)
000591      ERROR = AIMAG(OMEGA)*SPREAD/CHANGE
000592      GAMMA = AIMAG(OMEGA) - ERROR
000593      WRITE(1GRAPH,150) SPREAD,CHANGE,GAMMA
000594      PRINT 150, SPREAD,CHANGE,GAMMA
000595      150 FORMAT(1H DURING ONE GROWTH PERIOD, A WAVE PACKET
000596      . SPREADS A DISTANCE OF ",E12.3" IN LARMOR RADII", THE FREQUENCY
000597      . FOR A GIVEN KYAI CHANGES OVER A DISTANCE OF ",E12.3," IN LARMOR RA
000598      . DI"/" GAMMA PROBABLY CLOSER TO ",E12.3")
000599      GO TO 153
000600      151 PRINT 152, ZERO, DFDW, D2FDK2, DFDX
000601      152 FORMAT(" SOMETHING WRONG, DISP = ",2E22.13/"DFDW, D2FDK2, DFDX = ",6E
000602      . 18.11)
000603      153 CONTINUE
000604      146 CONTINUE
000605      C PLOT THE EIGENFUNCTIONS PHI(X) IF DESIRED.
000606      48 CALL EIGPLT
000607      CALL TIMECHK(A00T,0.,ELAPSED)
000608      PRINT 78, ELAPSED
000609      IF(NOCRT.NE.0) CALL EXIT
000610      C DO THE CRT PLOT OF THE REAL PART OF ROOTS.
000611      XMIN = IFIX(SKYAI)
000612      XMAX = IFIX(FKYAI+1.)
000613      IF(XMAX.EQ.FKYAI+1.) XMAX = FKYAI
000614      IF(XMAX-XMIN.GT.100.) XMAX = 10.*IFIX(XMAX/10.+1.)
000615      IF(XMAX.EQ.FKYAI+10.) XMAX = FKYAI
000616      YMAX = IFIX(RMX-.5)+1.5
000617      IF(YMAX.EQ.RMX+1.) YMAX = RMX
000618      YMIN = IFIX(RMIN)-1.E-06
000619      NX2 = XMAX-XMIN
000620      IF(NX2.GT.100) NX2 = NX2/10
000621      NX3 = 1
000622      IF(NX2.LT.10) NX3 = 2
000623      IF(NX2.LT.5) NX3 = 5
000624      NY2 = 2.* (YMAX - YMIN)
000625      CALL MAPS(XMIN,XMAX,YMIN,YMAX,0.11328,1.0,0.30,1.0)
000626      CALL PAGE
000627      IF(.NOT.SW31) TEXTURE = 3.
000628      IF(PRDAMP) GO TO 155
000629      IF(UNMAG) GO TO 66
000630      155 IF(NR.LE.1) GO TO 64
000631      NR = NR - 1
000632      DO 65 J = 1, NR
000633      IMIN = NRCUT(J) + 1
000634      IMAX = NRCUT(J+1)
000635      NUM = MINO(IMAX - IMIN + 1, 500)
000636      PRINT 77, J, NUM
000637      77 FORMAT(14H PLOTTING ROOT,14,120,7H POINTS)
000638      K = 0
000639      DO 72 I = IMIN,IMAX
000640      K = K + 1
000641      YPLOT(K) = Y(I)
000642      IF(YPLOT(K).LT.YMIN) YPLOT(K) = YMIN
000643      XPLOT(K) = X(I)
000644      72 IF(K.GT.500) GO TO 65
000645      65 CALL TRACET(TEXTURE,XPLOT,YPLOT,NUM)
000646      64 IF(NZ.LE.1) GO TO 66
000647      NZ = NZ - 1
000648      DO 67 J = 1,NZ
000649      IMIN = NZCUT(J) + 1
000650      IMAX = NZCUT(J+1)
000651      NUM = MINO(IMAX - IMIN + 1, 500)
000652      IF(SINGLX.OR.PMAX.GT.0) PRINT 77, J, NUM
000653      IF(.NOT.SINGLX.AND.PMAX.EQ.0) PRINT 126, J, NUM, XLR(J+1)
000654      126 FORMAT(14H PLOTTING ROOT,14,120,7H POINTS, 6H X/L =,F5.2)
000655      K = 0
000656      DO 73 I = IMIN, IMAX
000657      K = K + 1
000658      YPLOT(K) = YZ(I)
000659      IF(YPLOT(K).LT.YMIN) YPLOT(K) = YMIN
000660      XPLOT(K) = XZ(I)
000661      73 IF(K.GT.500) GO TO 67
000662      67 CALL TRACET(TEXTURE,XPLOT,YPLOT,NUM)
000663      66 IF(NC.LE.1) GO TO 68
000664      NC = NC - 1
000665      C USE DOTTED LINE FOR COMPLEX ROOTS.

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000666 TEXTURE = 2,
000667 IF(.NOT.SW31) TEXTURE = 0.
000668 DO 69 J = 1, NC
000669 IMIN = NCCUT(J) + 1
000670 IMAX = NCCUT(J+1)
000671 NUM = MINO(IMAX - IMIN + 1, 500)
000672 IF(SINGLX.OR.PMAX.GT.0) PRINT 77, J, NUM
000673 IF(.NOT.SINGLX.AND.PMAX.EQ.0) PRINT 126, J, NUM, XLC(J+1)
000674 K = 0
000675 DO 74 I = IMIN, IMAX
000676 K = K + 1
000677 YPLOT(K) = YR(I)
000678 IF(YPLOT(K).LT.YMIN) YPLOT(K) = YMIN
000679 XPLOT(K) = XC(I)
000680 74 IF(K.GT.500) GO TO 69
000681 69 CALL TRACET(TEXTURE,XPLOT,YPLOT,NUM)
000682 68 TEXTURE = 0.
000683 TVRNGE = TVXMAX - TVXMIN
000684 FACTX= TVRNGE/(XMAX-XMIN)
000685 TVRNGE = TVYMAX - TVYMIN
000686 FACTY = TVRNGE/(YMAX - YMIN)
000687 C LIST THE PARAMETERS UNDER THE CRT PLOT.
000688 CALL PARAM(98)
000689 CALL SETCH(1, 7., 1, 0, 1, 0, 0)
000690 WRITE(IGRAPH, 46)
000691 46 FORMAT(19H REAL PART OF ROOTS)
000692 CALL FRAME(1)
000693 C DO THE CRT PLOT OF THE IMAGINARY PART OF ROOTS.
000694 IF(NPTC.EQ.0) GO TO 47
000695 NY2 = IFIX(YI(MAXGR0) + 1.)
000696 YMAX = NY2
000697 YMIN = 0.
000698 NY2 = 2.*NY2
000699 CALL MAPS(XMIN,XMAX,YMIN,YMAX,0.11328,1.0,0.30,1.0)
000700 IF(NC.LT.1) GO TO 70
000701 DO 71 J = 1, NC
000702 IMIN = NCCUT(J) + 1
000703 IMAX = NCCUT(J+1)
000704 NUM = MINO(IMAX - IMIN + 1, 500)
000705 K = 0
000706 DO 75 I = IMIN, IMAX
000707 K = K + 1
000708 YPLOT(K) = YI(I)
000709 IF(YPLOT(K).LT.YMIN) YPLOT(K) = YMIN
000710 XPLOT(K) = XC(I)
000711 75 IF(K.GT.500) GO TO 71
000712 71 CALL TRACET(TEXTURE,XPLOT,YPLOT,NUM)
000713 70 FACTY = TVRNGE/(YMAX - YM1N)
000714 CALL PARAM(98)
000715 CALL SETCH(1, 9., 1, 0, 1, 0, 0)
000716 WRITE(IGRAPH, 44) YR(MAXGR0), YI(MAXGR0), XC(MAXGR0), XLGMX
000717 WRITE(IGRAPH, 158) GAMK2, XC(MGAMK2)
000718 WRITE(IGRAPH, 41)
000719 47 CALL FRAME(1)
000720 CALL PLATE
000721 CALL TIMECHK(A00T, 0., ELAPSED)
000722 PRINT 78, ELAPSED
000723 CALL EXIT
000724 END

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000725
000726
000727 C SUBROUTINE XLSET(XL,XKO,EPSI,EPSE,NSP,NSP1,NSPEC,EPS,DREL,RH,KOAI)
000728 C DOES EVERYTHING THAT HAS TO BE DONE WHEN A NEW VALUE OF X/L IS USED.
000729 REAL KOAI
000730 DIMENSION EPS(NSPEC), DREL(NSPEC), RH(NSPEC)
000731 DATA PI/3.141592653589/
000732 XKO = 2.*PI*XL
000733 DO 115 I = 1, NSP
000734 DREL(I) = 1. + EPSI*RH(I)*COS(XKO)
000735 115 EPS(I) = -EPSI*RH(I)*KOAI*SIN(XKO)/DREL(I)
000736 DO 100 I = NSP1, NSPEC
000737 DREL(I) = 1. + EPSE*RH(I)*COS(XKO)
000738 100 EPS(I) = -EPSE*RH(I)*KOAI*SIN(XKO)/DREL(I)
000739 RETURN
000740 END

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000740
 000741 C SUBROUTINE DETAIL(N)
 000742 C CALCULATES DETAILED INFORMATION ON ONE ROOT, PHI, RH σ E, AND RH σ I.
 000743 C BEFORE CALLING THIS ROUTINE, IT IS NECESSARY TO CALL DISP AND SAVPHI
 000744 C WHICH CALCULATE ARH AND PHI, USED IN THIS SUBROUTINE. OMEGA AND KYAI MUST
 000745 C BE STORED IN PHI(N,NPP+1) AND PHI(N,NPP+2) RESPECTIVELY, BEFORE CALLING
 000746 C THIS SUBROUTINE.
 000747 C LOGICAL DTCALC
 000748 C COMPLEX A(20,20), PHI(18, 22), PHNORM, RHNORM
 000749 C COMPLEX ARH(20,20,4), OMEGA, RH σ E(20), RH σ I(20)
 000750 C COMPLEX PHI1(20)
 000751 C REAL KYAI
 000752 C COMMON/CIO/ ICR, IHSP, IGRAPH
 000753 C COMMON/CDETL/ DTCALC, ARH
 000754 C COMMON /PHIC/ A, NRTSV, PHI
 000755 C COMMON/CSPEC/ RLARM(4), AMASS(4), CHARG(4), JAY(4), DENSE(4), NSPEC
 000756 C COMMON/PMX/NPP
 000757 C COMMON/CNSP/ NSP, NSP1
 000758 C COMMON/CTVY/TVY
 000759 C COMMON/TVTUNE/LPENON, LPENOFF, ITALICS, IWINK, INTENSE, IRIGHT, IUP
 000760 C DATA PI/3.1415926535/
 000761 C PRINT 19, A(1,1),A(1,2)
 000762 C NP1 = NPP - 1
 000763 C DO 20 I = 2, NP1
 000764 C 20 PRINT 19, A(I,I-1), A(I,I), A(I,I+1)
 000765 C PRINT 19, A(NPP,NP1), A(NPP,NPP)
 000766 C 19 FORMAT(6E13.4)
 000767 C DO 22 J = 1, NSPEC
 000768 C PRINT 23, J
 000769 C 23 FORMAT(/"MATRIX FOR SPECIES", 13/)
 000770 C PRINT 19, ARH(1,1,J), ARH(1,2,J)
 000771 C DO 21 I = 2, NP1
 000772 C 21 PRINT 19, ARH(I,I-1,J), ARH(I,I,J), ARH(I,I+1,J)
 000773 C 22 PRINT 19, ARH(NPP,NP1,J), ARH(NPP,NPP,J)
 000774 C KYAI = REAL(PHI(N,NPP+2))
 000775 C C CALCULATE RH σ E(P) RH σ I(P)
 000776 C DO 15 I = 1, NPP
 000777 C RH σ E(I) = 0.
 000778 C 15 RH σ I(I) = 0.
 000779 C NP1 = NPP - 1
 000780 C DO 14 J = NSP1, NSPEC
 000781 C RH σ E(1) = ARH(1, 1,J)*PHI(N, 1) + ARH(1, 2,J)*PHI(N, 2)
 000782 C +RH σ E(1)
 000783 C 14 RH σ E(NPP) = ARH(NPP,NP1,J)*PHI(N,NP1) + ARH(NPP,NPP,J)*PHI(N,NPP)
 000784 C +RH σ E(NPP)
 000785 C DO 16 J = 1, NSP
 000786 C RH σ I(1) = ARH(1, 1,J)*PHI(N, 1) + ARH(1, 2,J)*PHI(N, 2)
 000787 C +RH σ I(1)
 000788 C 16 RH σ I(NPP) = ARH(NPP,NP1,J)*PHI(N,NP1) + ARH(NPP,NPP,J)*PHI(N,NPP)
 000789 C +RH σ I(NPP)
 000790 C DO 17 I = 2, NP1
 000791 C DO 17 J = NSP1, NSPEC
 000792 C 17 RH σ E(I) = ARH(I,I-1,J)*PHI(N,I-1) + ARH(I,I,J)*PHI(N,I) + ARH(I,I+
 000793 C .1,J)*PHI(N,I+1) + RH σ E(I)
 000794 C DO 18 J = 1, NSP
 000795 C 18 RH σ I(I) = ARH(I,I-1,J)*PHI(N,I-1) + ARH(I,I,J)*PHI(N,I) + ARH(I,I+
 000796 C .1,J)*PHI(N,I+1) + RH σ I(I)
 000797 C 1 CONTINUE
 000798 C C NORMALIZE PHI AND RH σ
 000799 C SUM = 0.
 000800 C DO 3 I = 1, NPP
 000801 C 3 SUM = SUM + CABS2(PHI(N,I))
 000802 C PHNORM = CMPLX(SQRT(SUM),0.)
 000803 C RHNORM = CMPLX(4.*PI,0.)*PHNORM
 000804 C DO 4 I = 1, NPP
 000805 C PHI(N,I) = PHI(N,I)/PHNORM
 000806 C RH σ I(I) = RH σ I(I)/RHNORM
 000807 C 4 RH σ E(I) = RH σ E(I)/RHNORM
 000808 C C THIS GIVES RH σ *AI**2 IN SAME UNITS AS PHI
 000809 C WRITE(IGRAPH,13)
 000810 C 13 FORMAT(9X,"PHI(P)",16X,"RH σ E(P)",17X,"RH σ I(P)",12X,"P")
 000811 C DO 6 I = 1, NPP
 000812 C IP = I - (NPP+1)/2
 000813 C WRITE(IGRAPH,7) PHI(N,I),RH σ E(I),RH σ I(I),IP
 000814 C 7 FORMAT(6E12.4,15)
 000815 C 6 CONTINUE
 000816 C DO 10 I = 1, NPP
 000817 C 10 PHI1(I) = PHI(N,I)
 000818 C CALL PLOT(PHI1,NPP,PHIMAX)
 000819 C CALL SETCH(1.,10.,1,0,1,0,0)
 000820 C WRITE(IGRAPH,11)
 000821 C 11 FORMAT(/"POTENTIAL FROM X = 0 TO X = L, FROM Y = 0 TO Y = 2PI/KY")
 000822 C WRITE(IGRAPH,9) PHI(N,NPP+1),KYAI
 000823 C CALL PARAM(98)
 000824 C 9 FORMAT(9H OMEGA = ,2E15.6,8H KYAI = ,E15.6)
 000825 C CALL PLOT(RH σ E,NPP,RHEMAX)
 000826 C RHEMAX = RHEMAX/PHIMAX
 000827 C NAME = 9HELECTRON
 000828 C CALL SETCH(1.,10.,1,0,1,0,0)
 000829 C WRITE(IGRAPH,12) NAME,RHEMAX
 000830 C 12 FORMAT(/1X,A9,"CHARGE DENSITY, MAXIMUM = ",E12.4,14H *PHIMAX/AI**2
 000831 C .)
 000832 C WRITE(IGRAPH,9) PHI(N,NPP+1),KYAI
 000833 C CALL PARAM(98)
 000834 C CALL PLOT(RH σ I,NPP,RHIMAX)
 000835 C NAME = 9HN
 000836 C CALL SETCH(1.,10.,1,0,1,0,0)
 000837 C WRITE(IGRAPH,12) NAME,RHIMAX
 000838 C WRITE(IGRAPH,9) PHI(N,NPP+1),KYAI
 000839 C CALL PARAM(98)
 000840 C CALL FRAME(1)
 000841 C CALL SETCH(1.,42.,1,0,1,0,0)
 000842 C RETURN
 000843 C END

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000844 SUBROUTINE PLT(F, NP, FMAX)
000845 EXTERNAL PLFUNC
000846 COMPLEX F(20), FTWIDL(20)
000847 DIMENSION C(11)
000848 COMMON/COMPLCT/ NPP, FTWIDL, FMAX
000849 DATA K1, K2, NX, NY /-11, 6, 100, 50/
000850 NPP = NP
000851 CALL FRAME(1)
000852 C(1) = -1.0
000853 C(2) = 1.0
000854 DG_1 = 1., NP
000855 DG_2 = 1., NP
000856 1 FTWIDL(I) = F(I)
000857 CALL MAPS(0., 1., 0., 1., 0., 11328, 1.0, 0.30, 1.0)
000858 FMAX1 = 1.
000859 FMAX = 0.
000860 DG_2 * Y = 1.50
000861 Y = FLOAT(IY)/50.
000862 DG_3 * IX = 1/100.
000863 X = FLOAT(IX)/100.
000864 GENERIC PLFUNC
000865 FXY = PLFUNC(X, Y)
000866 3 IF(FXY > FMAX) FMAX = FXY
000867 CONTINUE
000868 FMAX1 = FMAX
000869 CALL LCURVS1(K1, C, K2, NX, NY)
000870 RETURN
000871 END

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000872 SUBROUTINE LCURVS1(K1, C, K2, NX, NY)
000873 EXTERNAL PLFUNC
000874 DIMENSION C(1)
000875 CALL LCURVS(K1, C, K2, PLFUNC, NX, NY)
000876 RETURN
000877 END

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000879 GENERIC PLFUNC
000880 FUNCTION PLFUNC(X, Y)
000881 COMPLEX F(20), EIKY, EIPKO, FP
000882 INTEGER PMAX
000883 COMMON/COMPLCT/ NP, F, FMAX
000884 DATA P1/3.141592653589/
000885 PMAX = (NP-1)/2
000886 FP = 0.
000887 DG_1 * J = 1 NP
000888 P = J - PMAX - 1
000889 PKO = 2.*X*X*P1*P
000890 EIPKO = CEXP(CMPLX(O., PKO))
000891 1 FP = FP + F(J)*EIPKO
000892 YY = 2.*P1*Y
000893 EIKY = CEXP(CMPLX(O., YY))
000894 PLFUNC = REAL(FP*EIKY)/FMAX
000895 RETURN
000896 END

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C      SUBROUTINE FOLLOW(XO,YO,PHIZP)
THIS SUBROUTINE FOLLOWS A GIVEN ROOT THROUGH INCREASING VALUES OF KYAI.
THE STARTING POINTS FOR THE SEARCH FOR THE ROOT AT EACH NEW VALUE OF
KYAI (DONE BY *MRAF*) ARE DETERMINED BY MAKING A PARABOLIC FIT FOR THE
LAST 3 VALUES OF KYAI AND EXTENDING THIS PARABOLA TO THE NEW KYAI.
IF NO ROOT IS FOUND WITHIN ERRMAX OF THE STARTING POINT P3, THE INCREMENT
DELT2 IS CUT IN HALF AND WE TRY AGAIN. THIS IS ALSO DONE IF THE ONLY
ROOT FOUND IS IMPLAUSIBLE(BECAUSE THE EIGENFUNCTION CHANGES TOO DRASTICALLY
OR OMEGA CHANGES TOO MUCH). THE INCREMENT IS INCREASED IF THE ROOT IS
FOUND VERY CLOSE TO THE STARTING POINT (LESS THAN ERRMIN) AND THERE IS VERY
LITTLE CHANGE IN THE EIGENFUNCTION, BUT THE RELATIVE INCREMENT DK(=DELT2/
KYAI) IS NEVER MORE THAN DMAX, IF DK FALLS BELOW DMIN, WE GIVE UP
FOLLOWING THIS ROOT AND RETURN.
EXTERNAL DISP
LOGICAL SW(6), SW7, CV(2), WARN, DEJAVU, PHIZ(200), PHIZP, ZEH(100)
LOGICAL REALZ, FLIP, GOOD(18), PAIR, A00T, SW71, SW31
LOGICAL CMPPR, CMCRIT, FLIPC
LOGICAL UNMAG
COMPLEX P1,P2,P3,R00T,F00T, FUNC,H,Y0,Y1,Y2,A,B,C,Y3
COMPLEX YY(2), YINIT
COMPLEX PHIOLD(20), PHINEW(20), PHIVLD(20)
COMPLEX YSTART
COMPLEX YREV
INTEGER EIGV, PMAX
REAL KYAI, KYSQ, KOSQ
DIMENSION X(2000), Y(2000), XC(1000), YR(1000), YI(1000), XZ(4000),
YZ(4000)
COMMON/C10/ ICR, IHSP, IGRAPH
COMMON/CFAST/DK1, FKYAI1, NPTC, Y1, YR, XC, KYD, YMAX,
YZ, XZ, Y, X, NPT, NPTZ, ZEH, IGV, A00T, NF0L, FKYAI2, YMIN
COMMON/CMRAF/SW, RTC, ITC, EP3, FRMAX, XRMAX, H, R00T, FUNC, F00T, EIGV,
SW7, START, RMX, NFL, CYAI
COMMON/DIS/QF, KYSQ, KOSQ, EPSF(4), MASS, KYAI, KOAI, MASQ, PMAX, OMPSQ
AEAI, KMAX(4), AMASQ(4), EPS(4), KMIN(4)
COMMON/CPHCK/ PHINEW, PHZP
COMMON/PMX/NP
COMMON/FOLEIG/ GOOD, IBRANCH(18)
COMMON/CMRAF2/ ERRMAX, NRTSU, SW31, SW71
COMMON/CF0L/YSTART(100), XSTART(100), NSTART, YEND(100), XEND(100),
NSTRT1
COMMON/CCHECK/XCRIT(100), YCRIT(100), NCRT, DEJAVU, Y2, N, PZCRIT(100)
COMMON/CCMP/ CMPPR, CMCRIT(100)
COMMON/CPHZ/ PHIZ
COMMON/CQN/MINQ
COMMON/CMAG/ UNMAG
DATA GOOD/10*.FALSE./
DATA FRAMES/3./
DATA A00T/.FALSE./
DATA NSTART/0/
DATA NCRT/0/
DATA NGROW/0/
DATA SUM2/0/
DATA SUM2MX/0/
CALL TIMECHK(A00T, FRAMES, ELAPSED)
IF(A00T) RETURN
C      FKYAI1 IS THE VALUE OF KYAI READ IN. FKYAI2 IS A SMALLER VALUE USED
FOR REAL ROOTS WHICH WE ARE NOT INTERESTED IN FOLLOWING SO FAR.
FKYAI = FKYAI2
IF(XO.GE.FKYAI2) FKYAI = FKYAI1
IF(FKYAI2.GT.FKYAI1) FKYAI = FKYAI1
BASE = .5*X0
BASE2 = .25*FKYAI + XO
PHZP = SGNL(1., PHIZP)
FLIP = .FALSE.
FLIPC = .FALSE.
PAIR = .FALSE.
DK = DK1
ERRMAX = .003
ERRMIN = .0005
SUM2MX = NP*.01
SPREAD = .001
YINIT = Y0
DKMAX = DK1
DKMIN = 1.E-10
IF(SW31) GO TO 110
IF(AIMAG(Y0).LE.0.) GO TO 15
FKYAI = FKYAI1
NGROW = NGROW + 1
PRINT 55, NGROW
GO TO 15
110 IF(REALZ(Y0)) GO TO 15
FKYAI = FKYAI1
NCRT = NCRT + 1
PRINT 55, NCRT
C      55 FORMAT(13H GROWING ROOT, 14, 7H BEGINS)
IF THE ROOT IS ALREADY COMPLEX AT INITIAL KYAI, GIVE HARMLESS NONSENSE
VALUES TO XCRIT, YCRIT, AND PZCRIT (USED BY *CHECK*) FOR THIS ROOT.
PZCRIT(NCRT) = 0.
YCRIT(NCRT) = -1.
XCRIT(NCRT) = -1.
CMCRIT(NCRT) = .TRUE.
15 IF(.NOT.SW71) GO TO 134
YREV = CMPLX(AIMAG(Y0), REAL(Y0))
IF(REALZ(YREV)) GO TO 134
NCRT = NCRT + 1
PRINT 135, NCRT

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000995 135 FORMAT(13H MOVING ROOT,14,7H BEGINS)
000996 PZCRIT(NCRIT) = 0.
000997 YCRIT(NCRIT) = -1.
000998 XCRIT(NCRIT) = -1.
000999 CMCRIT(NCRIT) = .FALSE.
001000 C FIND FIRST AND SECOND DERIVATIVES OF ROOT WITH RESPECT TO KYAI
001001 134 DELT1 = 1.E-05*X0
001002 DELT2 = 1.E-04*X0
001003 IF(SW31.EQ.NFOL.LE.NSTRT1) GO TO 116
001004 DELT1 = 1.E-10*X0
001005 DELT2 = 1.E-09*X0
001006 DK = 1.E-09
001007 116 P3 = Y0
001008 P2 = Y0 - (0.,001)
001009 P1 = Y0 - (.001,0.)
001010 16 KYAI = X0 + DELT1
001011 IF(WARN(0)) RETURN
001012 KYSQ = KYAI*KYAI
001013 CYAI = KYAI
001014 CHI = KYSQ + PMAX*PMAX*KOSQ
001015 MINQ = 2.*REAL(P3)
001016 CALL QINT(CHI)
001017 CALL QFKCAL(QF,KMAX,KMIN,P3+3,P3)
001018 CALL MRAF(DISP,YY,CV,2,P1,P2,P3,1.E-06,1.E-12,25)
001019 C IF NO PLAUSIBLE ROOT IS FOUND, REDUCE DELT1 AND TRY AGAIN.
001020 IF(.NOT.CV(1)) GO TO 29
001021 Y1 = YY(1)
001022 IF(.NOT.CV(2)) GO TO 59
001023 IF(PHZP.EQ.SGNL(1,PHIZ(1)))GO TO 59
001024 IF(PHZP.NE.SGNL(1,PHIZ(2)))GO TO 291
001025 Y1 = YY(2)
001026 59 IF(AIMAG(Y1).LT.-1.E-06.AND.SW31) GO TO 292
001027 IF(REAL(Y1).LT.-1.E-06.AND.SW71) GO TO 294
001028 GO TO 48
001029 IWHY = 10 $ GO TO 29
001030 IWHY = 11 $ GO TO 29
001031 IWHY = 12 $ GO TO 29
001032 IWHY = 14 $ GO TO 29
001033 29 IF(DELT1.LT.1.E-10) GO TO 58
001034 DELT1 = DELT1/10.
001035 IF(SW(1)) PRINT 56,DELT1,IWHY
001036 56 FORMAT(17H DELT1 REDUCED TO E22.13,11H FOR REASON,14)
001037 IF(SW(1).AND.IWHY.EQ.1) PRINT 57,PHIZP,PHIZ(1)
001038 57 FORMAT(9H PHIZP IS,L5,11H PHIZ(1) IS,L5)
001039 GO TO 16
001040 48 IF(IGV.EQ.0) GO TO 68
001041 DO 31 I = 1,NP
001042 PHIOLD(I) = PHINEW(I)
001043 31 PHIOLD(I) = PHINEW(I)
001044 68 A = (0.,0.)
001045 B = (Y1 - Y0)/DELT1
001046 C = Y0 + B*DELT1
001047 ERROR = .001
001048 Y2 = Y1
001049 GO TO 27
001050 C 8 IF(WARN(0)) RETURN
001051 C EVEN IF EIGV WAS ORIGINALLY 3 OR 4, WE ONLY LET IT BE EQUAL TO ITS
001052 C ORIGINAL VALUE EVERY SO OFTEN, OTHERWISE WE WILL BE PLOTTING A
001053 C RIDICULOUS NUMBER OF EIGENFUNCTIONS.
001054 IF(IGV.EQ.0) GO TO 53
001055 IF((KYAI/BASE).LT.(1.+DKMAX)) GO TO 40
001056 EIGV = IGV
001057 GO TO 53
001058 40 EIGV = 2
001059 53 IF(KYAI.LT.BASE2) GO TO 41
001060 BASE2 = BASE2 + .25*FKYAI
001061 C CHECK THE TIME EVERY SO OFTEN, TO MAKE SURE WE ARE NOT ALMOST OUT OF TIME
001062 CALL TIMECHK(AOOT,FRAMES,ELAPSED)
001063 PRINT 54, ELAPSED, KYAI
001064 54 FORMAT(5X,8H TIME IS,F8.3,1OH AT KYAI =,F8.3)
001065 IF(AOOT) RETURN
001066 41 CALL QFKCAL(QF,KMAX,KMIN,P3+3,P3)
001067 CALL MRAF(DISP,YY,CV,2,P1,P2,P3,1.E-06,1.E-12,25)
001068 Y2 = YY(1)
001069 Y3 = YY(2)
001070 IF(.NOT.CV(1)) GO TO 90
001071 C WE CHANGE LOGICAL VARIABLES TO REAL VARIABLES, SO WE CAN USE THEM
001072 C IN IF(A.EQ.B) STATEMENTS;
001073 PHZ1 = SGNL(1,PHIZ(1))
001074 PHZ2 = SGNL(1,PHIZ(2))
001075 IF(.NOT.SW31) GO TO 121
001076 RL2 = SGNL(1,REALZ(Y2))
001077 RL3 = SGNL(1,REALZ(Y3))
001078 RLI = SGNL(1,REALZ(YINIT))
001079 121 IF(.NOT.SW71) GO TO 120
001080 YREV = CMPLX(AIMAG(Y2),REAL(Y2))
001081 AIM2 = SGNL(1,REALZ(YREV))
001082 YREV = CMPLX(AIMAG(Y3),REAL(Y3))
001083 AIM3 = SGNL(1,REALZ(YREV))
001084 YREV = CMPLX(AIMAG(YINIT),REAL(YINIT))
001085 AIM1 = SGNL(1,REALZ(YREV))
001086 120 IF(.NOT.CV(2)) GO TO 14
001087 C IF TWO PLAUSIBLE ROOTS, GO TO 20
001088 IF(PHZ1.EQ.PHZP.AND.PHZ2.EQ.PHZP) GO TO 20
001089 C NO PLAUSIBLE ROOTS
001090 IF(PHZ1.EQ.PHZ2) GO TO 91

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001091 C ONE PLAUSIBLE ROOT AND ONE IMPLAUSIBLE ONE, THROW OUT THE LATTER.
 001092 IF(PHZ1.EQ.PHZP) GO TO 14
 001093 Y2 = Y3
 001094 PHIZ(1) = PHIZ(2)
 001095 PHZ1 = PHZ2
 001096 GO TO 14
 001097 C IF ONE OF THE ROOTS IS MUCH CLOSER THAN THE OTHER TO THE PREDICTED R
 001098 C USE THAT ONE.
 001099 20 IF(CABS2(Y2 - P3).LT.,01*CABS2(Y3 - P3)) GO TO 14
 001100 IF(.NOT.SW71) GO TO 117
 001101 CMPPR = .FALSE.
 001102 IF(AIM2.NE.AIM3) GO TO 122
 001103 IF(AIM2.GT.0..AND.REAL(Y3)*REAL(Y2).LT.0.) GO TO 123
 001104 IF(AIM1.GT.0..AND.AIM2.GT.0.) GO TO 117
 001105 IF(AIM1.LT.0..AND.AIM2.LT.0.) GO TO 124
 001106 IF(AIM2.GT.0.) GO TO 123
 001107 IF(REAL(Y2).LT.0.) Y2 = CMPLX(0.,AIMAG(Y2))
 001108 IF(REAL(Y3).LT.0.) Y3 = CMPLX(0.,AIMAG(Y3))
 001109 GO TO 13
 001110 123 IF(REAL(Y3).GT.0..AND.REAL(Y2).LT.0.) Y2 = Y3
 001111 C SEE IF WE HAVE A NEGATIVE CONJUGATE PAIR
 001112 IF(CABS2(CONJG(Y3)+YY(1)).GT.,01*CABS2(Y3-YY(1))) GO TO 126
 001113 GO TO 127
 001114 C IN THE CASE OF AN IRREVERSIBLE DISP. REL., WE ASSUME THERE ARE NO
 001115 C MULTIPLE ROOTS, SO IF THERE ARE TWO EQUALLY PLAUSIBLE ROOTS, WE REDUCE
 001116 C DK AND TRY AGAIN.
 001117 117 CMPPR = .TRUE.
 001118 IF(.NOT.SW31) GO TO 100
 001119 C IF THE ROOT CHANGES FROM REAL TO COMPLEX OR VICE VERSA, WE DONT
 001120 C TRUST THE NEW ROOT UNLESS THERE ARE TWO OF THEM.
 001121 IF(RL2.NE.RL3) GO TO 92
 001122 IF(RL2.GT.0..AND.AIMAG(Y3).GT.0..AND.AIMAG(Y2).LT.0.) Y2 = Y3
 001123 IF(RL1.EQ.RL2) GO TO 14
 001124 IF(REALZ(Y2)) GO TO 13
 001125 C SEE IF WE HAVE A CONJUGATE PAIR.
 001126 IF(CABS2(CONJG(Y3)-YY(1)).GT.,01*CABS2(Y3-YY(1))) GO TO 93
 001127 C SEE IF EIGENFUNCTION CHANGES TOO MUCH, BUT SET PAIR = .TRUE. SO WE WILL
 001128 C RETURN HERE.
 001129 C IF THE TWO ROOTS, Y2 AND Y3, ARE CLOSE TO ZERO, AND THEY HAVE
 001130 C NOT SWITCHED FROM BEING PURELY REAL TO BEING PURELY IMAGINARY
 001131 C OR VICE VERSA, THEN WE DO NOT HAVE A NEW PAIR, BUT RATHER
 001132 C TWO ROOTS WHICH CROSS EACH OTHER AT OMEGA = 0 WITHOUT INTERACTING.
 001133 127 IF(AIM1.NE.RL1.AND.AIM2.LT.0..AND.RL2.LT.0.) GO TO 14
 001134 IF(AIM1.NE.RL1.AND.AIM1.EQ.AIM2.AND.RL1.EQ.RL2.AND.P3.EQ.
 001135 .5.E-04) GO TO 14
 001136 PAIR = .TRUE.
 001137 IF(IGV.GE.2) GO TO 36
 001138 61 PAIR = .FALSE.
 001139 C IF WE REACH THE BEGINNING OF A PAIR, CHECK TO SEE IF WE
 001140 C HAVE ARRIVED HERE PREVIOUSLY BY ANOTHER ROUTE.
 001141 CALL CHECK
 001142 IF(.NOT.DEJAVU) GO TO 23
 001143 IF(CMPPR) PRINT 24, N
 001144 24 FORMAT(29H WE HAVE REACHED GROWING ROOT, 14)
 001145 IF(.NOT.CMPPR) PRINT 128, N
 001146 128 FORMAT(29H WE HAVE REACHED MOVING ROOT, 14)
 001147 RETURN
 001148 23 NCRIT = NCRIT + 1
 001149 IF(NCRIT.GT.100) RETURN
 001150 C RECORDING THE BEGINNING OF A NEW GROWING (OR MOVING) ROOT.
 001151 YINIT = Y2
 001152 YCRIT(NCRIT) = REAL(Y2)
 001153 IF(.NOT.CMPPR) YCRIT(NCRIT) = AIMAG(Y2)
 001154 XCRIT(NCRIT) = KYAI
 001155 PZCRIT(NCRIT) = PHZP
 001156 CMCRIT(NCRIT) = CMPPR
 001157 C GET READY TO FOLLOW THE NEW GROWING (OR MOVING) ROOT.
 001158 FKYAI = FKYAI1
 001159 YO = Y2
 001160 IF(CMPPR) DELT1 = .1*AIMAG(YO)**2
 001161 IF(.NOT.CMPPR) DELT1 = .1*REAL(YO)**2
 001162 DELT2 = DELT1
 001163 P3 = YO
 001164 P2 = YO + (0.,.1)*AIMAG(YO)
 001165 P1 = YO - (0.,.1)*AIMAG(YO)
 001166 X0 = KYAI
 001167 CALL TIMECHK(A00T, FRAMES, ELAPSED)
 001168 IF(CMPPR) PRINT 21, NCRIT, YCRIT(NCRIT), XCRIT(NCRIT), ELAPSED
 001169 21 FORMAT(13H GROWING ROOT, 14, 19H BEGINS AT OMEGA = ,E22.13,
 001170 .8H KYAI = E22.13, 5X, 8H TIME IS, F8.3)
 001171 IF(.NOT.CMPPR) PRINT 129, NCRIT, YCRIT(NCRIT), XCRIT(NCRIT), ELAPSED
 001172 129 FORMAT(13H MOVING ROOT, 14, 19H BEGINS AT GAMMA = ,E22.13,
 001173 .8H KYAI = E22.13, 5X, 8H TIME IS, F8.3)
 001174 IF(A00T) RETURN
 001175 GO TO 16
 001176 13 NSTART = NSTART + 1
 001177 C RECORD THE END OF A GROWING(OR MOVING) ROOT, AND ADD THE TWO NEW REAL
 001178 C (OR PURELY IMAGINARY) ROOTS TO THE LIST OF ROOTS TO BE FOLLOWED LATER
 001179 C OR, IF THIS IS THE END OF A GROWING ROOT AND WE ARE USING AN IRREVERSIBLE
 001180 C DISPERSION RELATION, ADD THE DAMPED ROOT TO THE LIST.
 001181 YSTART(NSTART) = Y2

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001182 XSTART(NSTART) = KYAI
001183 ZEH(NSTART) = PHIZ(1)
001184 IF(.NOT.SW31.AND.AIMAG(Y1).GT.0..AND.CMPPR) GO TO 111
001185 NSTART = NSTART + 1
001186 YSTART(NSTART) = Y3
001187 XSTART(NSTART) = KYAI
001188 ZEH(NSTART) = PHIZ(2)
001189 IF(.NOT.SW31.AND.CMPPR) GO TO 115
001190 49 YEND(NCRIT) = REAL(Y2)
001191 IF(.NOT.CMPPR) YEND(NCRIT) = AIMAG(Y2)
001192 XEND(NCRIT) = KYAI
001193 IF(CMPPR) PRINT 22, NCRIT, YEND(NCRIT), XEND(NCRIT)
001194 22 FORMAT(13H GROWING ROOT,14,17H ENDS AT OMEGA = ,E22.13,
001195 .8H KYAI = ,E22.13)
001196 IF(.NOT.CMPPR) PRINT 130, NCRIT, YEND(NCRIT), XEND(NCRIT)
001197 130 FORMAT(13H MOVING ROOT,14,17H ENDS AT GAMMA = ,E22.13,
001198 .8H KYAI = ,E22.13)
001199 111 RY2 = REAL(Y2)
001200 PRINT 22, NGROW, RY2, KYAI
001201 115 Y2 = Y1
001202 RETURN
001203 C IF WE HAVE FOUND ONLY ONE ROOT, SEE IF HAS CHANGED TOO MUCH IN SOME WAY
001204 C (E.G. FROM REAL TO COMPLEX OR VICE VERSA, OR IN ITS EIGENFUNCTION),
001205 C AND IF SO, REDUCE DK.
001206 14 IF(AIM2.LT.0..AND.RL2.LT.0.) GO TO 132
001207 IF(.NOT.SW31) GO TO 131
001208 IF(RL2.NE.RL1) GO TO 94
001209 131 IF(.NOT.SW71) GO TO 132
001210 IF(AIM2.NE.AIM1) GO TO 133
001211 132 IF(REAL(Y2).LT.-1.E-06.AND.SW71) GO TO 95
001212 IF(AIMAG(Y2).LT.-1.E-06.AND.SW31) GO TO 96
001213 IF(PHZ1.NE.PHZP) GO TO 97
001214 C FOR PHI(0) = 0 ROOTS, PHINEW IS NORMALIZED IN SUCH A WAY THAT PHI(-NP)
001215 C (=PHINEW(1)) ALWAYS HAS POSITIVE REAL PART (SEE DEFINITION OF ARNM
001216 C IN *MRAF*). IF PHI(-NP) HAS SWITCHED FROM -I TO +I, MULTIPLY PHIOLD
001217 C BY -1 SO IT IS NORMALIZED IN THE SAME WAY AS PHINEW, AND WE CAN COMPARE
001218 C THEM.
001219 IF(IGV.EQ.0) GO TO 11
001220 IF(.NOT.PHZP) GO TO 36
001221 IF(AIMAG(PHINEW(1))*AIMAG(PHIOLD(1)).LT.0.) GO TO 35
001222 GO TO 36
001223 35 IF(ABS(AIMAG(PHINEW(1))),GT.ABS(REAL(PHINEW(1)))) GO TO 37
001224 GO TO 36
001225 37 DO 38 I = 1, NP
001226 PHIOLD(I) = -PHIVLD(I)
001227 PHIOLD(I) = -PHIVLD(I)
001228 FLIP = .TRUE.
001229 36 SUM2 = 0.
001230 C SEE HOW MUCH THE EIGENFUNCTION HAS CHANGED, AND, IF DESIRED, PRINT
001231 C BUT THE COMPONENTS WHICH HAVE CHANGED DRAMATICALLY.
001232 DO 30 I = 1, NP
001233 DIFF2 = CABS2(PHINEW(I)-PHIOLD(I)-(PHIOLD(I)-PHIVLD(I))*(DELT2/
001234 .DELT1))
001235 SUM2 = SUM2 + DIFF2
001236 IF(DIFF2.LE.,01) GO TO 30
001237 33 IF(SW(1)) PRINT 34, I, PHINEW(I), PHIOLD(I), PHIVLD(I)
001238 34 FORMAT(8H PHINEW(,12,6H) = ,2E14.6,10H PHIOLD = ,4E14.6)
001239 30 CONTINUE
001240 IF(SW(1)) PRINT 62, SUM2
001241 62 FORMAT(7H SUM2 = E14.6)
001242 C IF THE EIGENFUNCTION HAS CHANGED TOO MUCH(I.E. IF SUM2 IS TOO LARGE)
001243 C REDUCE DK AND TRY AGAIN.
001244 IF(SUM2.GT.SUM2MX) GO TO 63
001245 IF(PAIR) GO TO 61
001246 FLIP = .FALSE.
001247 IF(.NOT.FLIPC) GO TO 11
001248 FLIPC = .FALSE.
001249 Y1 = -Y1
001250 YO = -YO
001251 GO TO 11
001252 63 IF(PAIR) GO TO 103
001253 C SOMETIMES PHI(0) PASSES THROUGH ZERO EVEN FOR A PHI(0).NE.0 ROOT,
001254 C IN WHICH CASE PHINEW AND PHIOLD WILL BE NORMALIZED DIFFERENTLY. SEE
001255 C IF THIS IS THE CASE.
001256 IF(FLIPC) GO TO 72
001257 IF(.NOT.FLIP.AND..NOT.PHZP) GO TO 37
001258 IF(FLIP) GO TO 75
001259 C SOMETIMES TWO ROOTS PASS THROUGH EACH OTHER AT OMEGA = 0 WITHOUT
001260 C INTERRACTING, IN WHICH CASE THE PHI(I) OF ONE ROOT IS THE COMPLEX
001261 C CONJUGATE OF THE PHI(I) OF THE OTHER ROOT. IF THIS IS THE CASE,
001262 C SWITCH TO FOLLOWING THE OTHER ROOT.
001263 74 IF(.SW31.AND.SW71.AND.CABS2(Y2).LT.1.E-06)GO TO 70
001264 GO TO 98
001265 C IF ROOT IS NO GOOD AND WE HAVE MULTIPLIED PHIOLD BY -1, MULTIPLY IT
001266 C BACK AGAIN.
001267 75 DO 39 I = 1, NP
001268 PHIOLD(I) = -PHIVLD(I)
001269 39 PHIOLD(I) = -PHIOLD(I)
001270 FLIP = .FALSE.
001271 GO TO 74
001272 70 DO 71 I = 1, NP
001273 PHIOLD(I) = CONJG(PHIVLD(I))
001274 71 PHIOLD(I) = CONJG(PHIOLD(I))
001275 FLIPC = .TRUE.
001276 GO TO 36

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001277 C IF ROOT IS NO GOOD AND WE HAVE REPLACED PHIOLD BY ITS COMPLEX
001278 C CONJUGATE, REPLACE IT BACK AGAIN.
001279 72 D0 73 I = 1, NP
001280 PHIVLD(I) = CONJG(PHIVLD(I))
001281 73 PHIOLD(I) = CONJG(PHIOLD(I))
001282 FLIPC = .FALSE.
001283 GO TO 136
001284 11 ERROR = CABS(P3 - Y2)
001285 C IF THE ERROR IN ESTIMATING THE LAST ROOT(VIZ. P3 - Y2) IS VERY SMALL AND
001286 C THE EIGENFUNCTION HAS NOT CHANGED TOO MUCH, INCREASE DK.
001287 IF(ERROR.GT.ERRMIN) GO TO 12
001288 IF(SUM2.GT..01) GO TO 12
001289 DK3 = DKMAX
001290 DK2 = DKMAX
001291 IF((ERROR/ERRMIN).GT.(DK/DKMAX)**3) DK3 = DK*(ERRMIN/ERROR)**(1./
001292 .3.)
001293 IF((SUM2.GT..01).GT.(DK/DKMAX)**2) DK2 = DK*SQRT(.01/SUM2)
001294 DK4= AMIN1(DK3,DK2)
001295 C DON'T LET DK INCREASE TOO RAPIDLY, OR WE MAY GET ON THE WRONG ROOT.
001296 IF(DK4.GT.10.*DK) DK4= 10.*DK
001297 DK = DK4
001298 IF(SW(1)) PRINT 28, DK
001299 28 FORMAT(16H DK INCREASED TO E12.6)
001300 C IF THE NEW ROOT Y2 IS OUTSIDE THE PRESENT FREQUENCY RANGE, EXPAND THE
001301 C RANGE TO INCLUDE IT (INCREASING YMAX OR DECREASING YMIN) AND CALCULATE
001302 C VALUES OF QF, KMAX, AND KMIN (USED IN *DISP*).
001303 12 IF(UNMAG.AND..NOT.REALZ(Y2).AND.AIMAG(Y2).LT.0.) GO TO 105
001304 IF(ABS(REAL(Y2)).LE.YMAX) GO TO 104
001305 YMAX = ABS(REAL(Y2))
001306 GO TO 105
001307 104 IF(ABS(REAL(Y2)).GE.YMIN) GO TO 106
001308 YMIN = ABS(REAL(Y2))
001309 105 CONTINUE
001310 106 IF(IGV.EQ.0) GO TO 69
001311 64 D0 32 I = 1, NP
001312 PHIVLD(I) = PHIOLD(I)
001313 32 PHIOLD(I) = PHINEW(I)
001314 C MAKE A NEW PARABOLIC FIT
001315 69 A = Y2/(DELT2*SUM) - Y1/(DELT1*DELT2) + Y0/(DELT1*SUM)
001316 B = (Y1 - Y0)/DELT1 + A*DELT1
001317 C = Y0 - A*DELT1*DELT1 + B*DELT1
001318 C LET *EIGPLT* KNOW THAT THIS IS A GOOD ROOT, SO IT WILL PLOT THE EIGE
001319 IF(EIGV.LE.2) GO TO 67
001320 IF(EIGV.EQ.4) GOOD(NRTSU) = .TRUE.
001321 IF(EIGV.EQ.3.AND.AIMAG(Y2).GE.1.E-05) GOOD(NRTSU) = .TRUE.
001322 IF(EIGV.GE.3.AND.GOOD(NRTSU)) GO TO 66
001323 GO TO 67
001324 66 BASE = KYAI
001325 C KEEP TRACK OF THE NUMBER OF FRAMES TO BE PLOTTED, SINCE THIS IS USED
001326 C BY *TIMECHK*.
001327 FRAMES = FRAMES + 2.
001328 IBRANCH(NRTSU) = NFOL
001329 67 IF(SW(1)) PRINT 60, EIGV, NRTSU, GOOD(NRTSU), BASE
001330 60 FORMAT(7H EIGV =,I4,8H NRTSU =,I4,15,10X,8H BASE =,E22.13)
001331 C PRINT OUT INFORMATION ON ROOT, IF DESIRED.
001332 X1 = X0 + DELT1
001333 IF(SW(1)) PRINT 7, A, B, C, X1
001334 7 FORMAT(43H OMEGA = A*DELT**2 + B*DELT + C, WHERE A = ,2F10.5/38X,
001335 .5H B = ,2F10.5/38X,5H C = ,2F10.5,14H DELT = KYAI -,F15.10)
001336 IF(SW31) GO TO 107
001337 C IF THE DISPERSION RELATION IS IRREVERSIBLE, AND THE GROWTH RATE HAS
001338 C CHANGED SIGN, TAKE APPROPRIATE MEASURES, SINCE WE WANT TO DISTINGUISH
001339 C GROWING ROOTS FROM DAMPED ROOTS IN THE PLOT.
001340 IF(AIMAG(Y1).LE.0..AND.AIMAG(Y2).GT.0.) GO TO 108
001341 CMPPR = .TRUE.
001342 IF(AIMAG(Y1).GT.0..AND.AIMAG(Y2).LE.0.) GO TO 13
001343 IF(AIMAG(Y2).GT.0.) GO TO 17
001344 GO TO 109
001345 108 CALL TIMECHK(AOOT,FRAMES,ELAPSED)
001346 NGRW = NGRW + 1
001347 RY2 = REAL(Y2)
001348 PRINT 21, NGRW, RY2, KYAI, ELAPSED
001349 GO TO 17
001350 107 IF(.NOT.REALZ(Y2)) GO TO 17
001351 109 IF(PHIZ(1)) GO TO 18
001352 IF(NPT.EQ.0) GO TO 52
001353 C DON'T BOTHER RECORDING ROOT FOR PLOTTING UNLESS IT IS A REASONABLE DISTANCE
001354 C FROM PREVIOUS ROOT.
001355 DGRPH= ((KYAI-X(NPT))/FKYAI)**2 + ((REAL(Y2)-Y(NPT))/YMAX)**2
001356 IF(DGRPH.LT.3.E-05) GO TO 19
001357 C RECORD REAL ROOT, PHIZ = .FALSE.
001358 52 NPT = NPT + 1
001359 Y(NPT) = REAL(Y2)
001360 X(NPT) = KYAI
001361 IF(NPT.GE.2000) RETURN
001362 GO TO 19
001363 18 IF(NPTZ.EQ.0) GO TO 51
001364 DGRPH= ((KYAI-XZ(NPTZ))/FKYAI)**2 + ((REAL(Y2)-YZ(NPTZ))/YMAX)**2
001365 IF(DGRPH.LT.4.E-06) GO TO 19
001366 C RECORD REAL ROOT, PHIZ = .TRUE.
001367 51 NPTZ = NPTZ + 1
001368 YZ(NPTZ) = REAL(Y2)
001369 XZ(NPTZ) = KYAI
001370 IF(NPTZ.GE.4000) RETURN
001371 GO TO 19

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001372 17 IF(NPTC.EQ.0) GO TO 50
001373 IF(ABS(AIMAG(Y2))-YI(NPTC),GT.,01) GO TO 50
001374 DGRPH=((KYAI-XC(NPTC))/FKYAI)**2+((REAL(Y2)-YR(NPTC))/YMAX)**2
001375 IF(DGRPH.LT.4.E-06) GO TO 19
001376 C RECORD COMPLEX ROOT
001377 50 NPTC = NPTC + 1
001378 YR(NPTC) = REAL(Y2)
001379 YI(NPTC) = AIMAG(Y2)
001380 XC(NPTC) = KYAI
001381 IF(NPTC.GE.1000) RETURN
001382 19 YO = Y1
001383 YI = Y2
001384 XO = XO + DELT1
001385 DELT1 = DELT2
001386 DELT2 = DK*KYAI
001387 C INCREASE KYAI AND PREDICT WHERE ROOT WILL BE (P3).
001388 27 KYAI = KYAI + DELT2
001389 IF(KYAI.GT.FKYAI) RETURN
001390 SUM = DELT1 + DELT2
001391 P3 = A*XSUM*SUM + B*XSUM + C
001392 IF(SW71.AND.SW31.AND.CABS2(P3).LT.1.E-06) P3 = .0005
001393 C IF THE PREDICTED NEW ROOT IS TOO FAR FROM THE OLD ROOT, EITHER RELATIVELY
001394 OR ABSOLUTELY, THE PREDICTION IS UNRELIABLE, SO REDUCE DK AND TRY AGAIN.
001395 IF(CABS2(Y2-P3).GT.1.) GO TO 45
001396 IF(CABS2(Y2 - P3).LT.1.E-06) GO TO 26
001397 IF(REAL(P3).EQ.0.AND.AIMAG(P3).EQ.0.) GO TO 45
001398 IF(CABS2(Y2/P3 -(1.,0.)).LT..04)GO TO 26
001399 45 KYAI = KYAI - DELT2
001400 DELT2 = .5*DELT2
001401 DK = DELT2/KYAI
001402 IF(SW(1)) PRINT 42, DK
001403 42 FORMAT(15H DK REDUCED TO , E12.6,41H BECAUSE Y2 IS RELATIVELY TOO
001404 . FAR FROM P3 )
001405 IF(DK.LT.DKMIN) GO TO 46
001406 GO TO 27
001407 26 SPREAD = AMAX1(ERROR,.001)
001408 P2 = P3 - (0.,1.)*SPREAD
001409 P1 = P3 - (1.,0.)*SPREAD
001410 CYAI = KYAI
001411 KYSQ = KYAI*KYAI
001412 CHI = KYSQ + PMAX*PMAX*KOSQ
001413 MINQ = 2.*REAL(P3)
001414 C SUBROUTINE *QINT* PRINTS OUT THE NEW KYAI IF DESIRED AND CALCULATES
001415 C THE PARAMETERS QMAX AND NMAX USED IN THE DISPERSION FUNCTION CALCULATION
001416 CALL QINT(CHI)
001417 IF(SW(1).AND.NOT.SW(2)) PRINT 65, P3
001418 65 FORMAT(5H P3 =,2E22.13)
001419 GO TO 8
001420 C IF DK HAS BEEN REDUCED, PRINT THIS FACT(IF DESIRED) AND TELL WHY. THIS
001421 INFORMATION IS INVALUABLE FOR DEBUGGING.
001422 90 IWHY = 0 $ GO TO 9
001423 91 IWHY = 1 $ GO TO 9
001424 92 IWHY = 2 $ GO TO 9
001425 93 IWHY = 3 $ GO TO 9
001426 94 IWHY = 4 $ GO TO 9
001427 95 IWHY = 5 $ GO TO 9
001428 96 IWHY = 6 $ GO TO 9
001429 97 IWHY = 7 $ GO TO 9
001430 98 IWHY = 8 $ GO TO 9
001431 99 IWHY = 9 $ GO TO 9
001432 100 IWHY = 100$ GO TO 9
001433 122 IWHY = 122 $ GO TO 9
001434 124 IWHY = 124 $ GO TO 9
001435 126 IWHY = 126 $ GO TO 9
001436 133 IWHY = 133 $ GO TO 9
001437 136 IWHY = 136 $ GO TO 9
001438 103 PAIR = .FALSE.
001439 IWHY = 13 $ GO TO 9
001440 9 KYAI = KYAI - DELT2
001441 DK = .5*DK
001442 IF(DK.LT.DKMIN) GO TO 46
001443 DELT2 = DK*KYAI
001444 IF(SW(1)) PRINT 10, DK, IWHY
001445 10 FORMAT(15H DK REDUCED TO , E12.6,11H FOR REASON,14)
001446 IF(.NOT.SW(1)) GO TO 27
001447 IF(IWHY.EQ.1.OR.IWHY.EQ.7) PRINT 43,PHZP,PHIZP,PHZ1,
001448 .PHIZ(1),PHZ2,PHIZ(2)
001449 43 FORMAT(8H PHZP = ,E22.13,L5/8H PHZ1 = ,E22.13,L5/8H PHZ2 = ,E22.13
001450 .L5)
001451 GO TO 27
001452 58 Y2 = Y1
001453 C IF DK OR DELT1 IS LESS THAN DMIN, GIVE UP ON THIS ROOT.
001454 46 PRINT 47, IWHY
001455 47 FORMAT(" DK IS LESS THAN DMIN, FOR REASON ",I4/" EITHER
001456 . QMAX AND NMAX (IN SUBROUTINES QINT AND QCALC) ARE TOO SMALL "
001457 ./" OR ZEE IS NOT ACCURATE ENOUGH, OR WE HAVE ENCOUNTERED A TOPO-"
001458 .//LOGICAL SITUATION WHICH THE PROGRAM CANNOT HANDLE")
001459 IF(IWHY.NE.100) RETURN
001460 C WE HAVE REACHED A CRITICAL POINT, IN THE IRREVERSIBLE CASE, CHECK IF
001461 C WE'VE BEEN HERE BEFORE. IF NOT, GO JUST PAST IT AND USE THE TWO NEW
001462 C ROOTS AS STARTING POINTS.
001463 CALL CHECK
001464 IF(.NOT.DEJAVU) GO TO 112
001465 PRINT 113, N
001466 113 FORMAT(31H WE HAVE REACHED CRITICAL POINT, 14)

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001467      RETURN      KYAI + 10. *DELT2 / ((DELT1/DELT2) *CABS((Y1-Y2)/(Y0-Y1))-1.)
001468      KYSQ = KYAI * KYAI
001469      CYAI = KYAI
001470      CALL MRAF(DISP YY, CV(2), P1, P2, P3, 1, E-06, 1, E-12, 25)
001471      IF( NOT CV(1) ) GO TO 114
001472      IF( SGNL(1, PHIZ(1)) .NE. PHZP ) RETURN
001473      Y2 = YY(1)
001474      Y3 = YY(2)
001475      NCRIT = NCRIT + 1
001476      IF( NCRIT .GT. 100 ) RETURN
001477      YCRIT(NCRIT) = REAL(Y2)
001478      XCRIT(NCRIT) = KYAI
001479      PZCRIT(NCRIT) = PHZP
001480      PRINT 114, NCRIT, Y2, KYAI
001481      FORMAT(42H WE HAVE REACHED A NEW CRITICAL POINT, NO., 14, 12H AT GM)
001482      GA = .2E22.13, 8H KYAI = , E22.13,
001483      GO TO 13
001484      END
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001486      SUBROUTINE TIMECHK(AOOT,ELAPSD)
001487      C CHECKS TO SEE IF WE ARE ALMOST OUT OF TIME. MAKES SURE THERE WILL BE
001488      C ENOUGH CUS LEFT OVER AFTER EXECUTION TO MAKE CRT PLOTS. FRAMES IS
001489      C NUMBER OF FRAMES TO BE PLOTTED (EMPIRICALLY 12 FRAMES IN THIS PROGRAM)
001490      C TAKE ABOUT 1 CU.) AOOT IS SET = TRUE. IF WE ARE ALMOST OUT OF TIME,
001491      C ELAPSED IS ELAPSED TIME IN SECONDS. ONE CU (AS USED AT LBL) IS ABOUT 0.25 SECONDS ON THE CDC7600.
001492      C LOGICAL UNMAG
001493      COMMON/CMAG/UNMAG
001494      LOGICAL AOOT
001495      DATA AOOT /0/
001496      DATA ELAPSED /0./
001497      DATA LTIM1/0/
001498      DATA LTIM2/0./
001499      DATA LTIM3/0./
001500      DATA LTIM4/0./
001501      CALL DOTIM(LTIM1,LTIM2,LTIM3,LTIM4)*1.E-06
001502      ELAPSED = ELAPSED + FLOAT(LTIM1)
001503      LEFT = 4.E-06*FLOAT(LTIM2)
001504      NEED = 30. + 15.*FLOAT(NPP) + FRAMES/12.
001505      IF(LEFT .LT. NEED) AOOT = .TRUE.
001506      ELAPSD = ELAPSED
001507      RETURN
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001490      C
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001493      C
001494      C
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001502      C
001503      C
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001509 SUBROUTINE CHECK(XCHECK,YCRIT(100),NCRIT,DEJAVU,Y2,N,PZCRIT(100))
001510 C CHECKS TO SEE IF A COMPLEX ROOT HAS ALREADY BEEN REACHED BY ANOTHER ROUTE.
001511 C IF IT HAS, WE SET DEJAVU = .TRUE.
001512 C
001513 COMMON/CPHCK/PHINew(20)
001514 COMMON/CCMP/CMCRIT(100)
001515 COMMON/DIS/QF,KYSQ,KOSQ,EPsf(4)
001516 REAL KYAI
001517 COMPLEX Y2
001518 COMMON/CHECK/XCRIT(100),YCRIT(100),NCRIT,DEJAVU,Y2,N,PZCRIT(100)
001519 COMMON/CPHCK/PHINew(20)
001520 COMMON/CCMP/CMCRIT(100)
001521 COMMON/DIS/QF,KYSQ,KOSQ,EPsf(4)
001522 REAL KMAX(4),AMASQ(4),EPS(4),KMIN(4)
001523 IF(NCRIT .LE. 0) GO TO 3
001524 DO 1 I = 1, NCRIT
001525 IF(PZCRIT(I) .NE. PHZP) GO TO 1
001526 C THERE ARE TWO TYPES OF CRITICAL POINTS CHARACTERIZED BY CMPPR = .TRUE. AND
001527 C CMPPR = FALSE. THE FORMER CONSIST OF TWO REAL ROOTS TURNING INTO
001528 C A CONJUGATE PAIR. THE LATTER CONSIST OF TWO PURELY IMAGINARY ROOTS
001529 C TURNING INTO A NEGATIVE CONJUGATE PAIR.
001530 IF(SGNL(1, CMCRIT(I)) .NE. SGNL(1, CMPPR)) NE_SGNL(1, CMPPR) GO TO 1
001531 IF(ABS(KYAI) - XCRIT(I)).LT..01*KYAI) GO TO 2
001532 1 CONTINUE = .FALSE.
001533 2 RETURN
001534 2 Y = REAL(Y2)
001535 2 IF(NOT CMPPR) Y = AIMAG(Y2)
001536 2 IF(ABS(Y - YCRIT(I)).GT..005) GO TO 3
001537 2 N = 1
001538 2 DEJAVU = .TRUE.
001539 2 RETURN
001540 2 END
001541 2

```

001542
001543      LOGICAL REALZ
001544      FUNCTION REALZ(Z)
001545      COMPLEX Z
001546      REALZ = .TRUE.
001547      PREC = 1.E-06
001548      IF(ABS(AIMAG(Z)).GT.PREC) REALZ = .FALSE.
001549      RETURN
001550      END

```

```

001551
001552
001553      SUBROUTINE QINT(CHI)
001554      C INTERFACE BETWEEN *QCALC* AND *ROOTS* OR *FOLLOW*)
001555      INTEGER QMAX
001556      LOGICAL SW(6)
001557      REAL KYAI
001558      COMPLEX H, ROOT, FUNC, FROOT
001559      COMMON/CMRAF/SW, RTC, ITC, EP3, FRMAX, XRMAX, H, ROOT, FUNC, FROOT, EIGV,
001560      SW7, START, RMX, NFL, KYAI
001561      COMMON/CRBESJ/ QMAX(4), NMAX(4)
001562      COMMON/CSPEC/ RLARM(4), AMASS(4), CHARG(4), JAY(4), DENSE(4), NSPEC
001563      DO 1 I = 1, NSPEC
001564      IF(RLARM(I).EQ.0.) GO TO 1
001565      CHI2 = CHI*RLARM(I)*RLARM(I)
001566      IF(JAY(I).EQ.0.) GO TO 2
001567      CALL QCALC(CHI2, QMAX(I), NMAX(I), 1)
001568      GO TO 3
001569      2 CALL QCALC(CHI2, QMAX(I), NMAX(I), 0)
001570      NMAX(I) = NMAX(I) + JAY(I)
001571      3 IF(SW(1)) PRINT 7, KYAI, QMAX(I), NMAX(I), I
001572      7 FORMAT(7H KYAI =, E22.13, 8H QMAX =, I4, 8H NMAX = , I4, 12H FOR SPECIE
001573      S, 13)
001574      1 CONTINUE
001575      RETURN
001576      END

```

```

001577
001578
001579      SUBROUTINE PARAM(N1)
001580      C THIS ROUTINE WRITES A LIST OF THE PARAMETERS ON PRINTER(N1=99) OR CRT(N1=98)
001581      INTEGER PMAX, RMAX, TYPE
001582      REAL LINE
001583      LOGICAL SINGLX, UNMAG
001584      COMMON/CIO/ ICR, IHSP, IGRAPH
001585      COMMON/CBETA/ BETA
001586      COMMON/CPARAM/ RMAX, AIL, EPSI, EPSE, NSPEC, DFUI, DFUE, EP, SINGLX, XL(10
001587      ), NXL
001588      COMMON/CRGAM/R, GAM, RE, GAME, R1, RE1, AEAI1
001589      COMMON/CSPEC/ RLARM(4), AMASS(4), CHARG(4), JAY(4), DENSE(4), XXXX
001590      COMMON/CDFU/ DFU(4), DRDL(4)
001591      COMMON/VTUNE/LPENON, LPENOFF, ITALICS, IWINK, INTENSE, IRIGHT, IUP
001592      COMMON/DIS/QF, KYSQ, KOSQ, EPSF(4), MASS, KYAI, KOAI, MASQ, PMAX, CMPSQ
001593      , AEAI, KMAX(4), AMASQ(4), EPS(4), KMIN(4)
001594      COMMON/CMAG/UNMAG
001595      IF(N1.EQ.98) N = IGRAPH
001596      IF(N1.EQ.99) N = IHSP
001597      TYPE = 6H LOCAL
001598      IF(PMAX.GT.0) TYPE = 6H
001599      IF(UNMAG) TYPE = 6H UNMAG
001600      IF(NSPEC.GT.0) GO TO 36
001601      C PMAX = 0 MEANS WE ARE USING THE LOCAL APPROXIMATION
001602      IF(PMAX.EQ.0) GO TO 4
001603      WRITE(N,3) TYPE, PMAX, AIL, CMPSQ, EPSI, EPSE, MASS, AEAI, DFUI, DFUE
001604      3 FORMAT(A6, 6H PMAX=, I2, 5H AIL=, F6.3, 7H CMPSQ=, F8.1, 6H EPSI=,
001605      , F6.3, 6H EPSE=, F6.3, 6H MASS=, F9.2, 7H AE/AI=, F7.4, 6H DFUI=,
001606      , F6.4, 6H DFUE=, F6.4)
001607      GO TO 5
001608      4 IF(.NOT.SINGLX) GO TO 7
001609      WRITE(N,6) CMPSQ, EP, MASS, AEAI, DFUI, DFUE, BETA
001610      6 FORMAT(14H LOCAL APPROX. 9H CMPSQ =, F9.3, 8H EPS =, F7.3,
001611      , 8H MASS =, F9.3/9H AE/AI =, F8.4, 7H DFUI =, F6.4, 7H DFUE =, F6.4,
001612      , 6H BETA =, F5.2)
001613      GO TO 5
001614      7 WRITE(N,8) TYPE, AIL, CMPSQ, MASS, AEAI, DFUI, DFUE, (XL(I), I=1, NXL)
001615      8 FORMAT(5H SINE A6, 5H AIL=, F7.4, 7H CMPSQ=, F7.1, 6H MASS=, F7.1, 7H AE/
001616      , AI=, F5.3, 6H DFUI=, F6.4/6H DFUE=, F6.4, 5H X/L=, 1OF4.2)

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001617      5 CONTINUE
001618      IF(R.GT.0.) GO TO 19
001619      WRITE(N,30)
001620      30 FORMAT(26H RING DISTRIBUTION OF IONS)
001621      GO TO 23
001622      19 IF(GAM.GT.0.) GO TO 31
001623      WRITE(N,32)
001624      32 FORMAT(16H MAXWELLIAN IONS)
001625      GO TO 23
001626      31 WRITE(N,24) R,GAM
001627      24 FORMAT(16H MIRROR RATIO = ,F7.2,8H GAMMA= ,F6.3,9H FOR IONS)
001628      23 CONTINUE
001629      IF(AEAI.GT.0.) GO TO 25
001630      WRITE(N,26)
001631      26 FORMAT(15H COLD ELECTRONS)
001632      GO TO 27
001633      25 IF(RE.GT.0.) GO TO 28
001634      WRITE(N,29)
001635      29 FORMAT(31H RING DISTRIBUTION OF ELECTRONS)
001636      GO TO 27
001637      28 IF(GAME.GT.0.) GO TO 33
001638      WRITE(N,34)
001639      34 FORMAT(21H MAXWELLIAN ELECTRONS)
001640      GO TO 27
001641      33 WRITE(N,35) RE,GAME
001642      35 FORMAT(16H MIRROR RATIO = ,F7.2,9H GAMMA = ,F6.3,14H FOR ELECTRONS
001643      )
001644      27 CONTINUE
001645      RETURN
001646      36 IF(N.EQ.1GRAPH) CALL SETCH(30.,7.,1,0,1,0,0)
001647      IF(PMAX.EQ.0.AND.SINGLX) WRITE(N,37) BETA
001648      37 FORMAT(22H LOCAL APPROX.,BETA =,F5.2)
001649      IF(N.EQ.1GRAPH) CALL SETCH(1,6,1,0,1,0,0)
001650      IF(PMAX.EQ.0.AND.NOT.SINGLX) WRITE(N,41) TYPE,A1L,EPSI,EPSE,
001651      (XL(I),I=1,NXL)
001652      41 FORMAT(5H SINE,A6,5H A1L=,F7.4,6H EPSI=,F6.3,6H EPSE=,F6.3/5H X/L=
001653      .10F4.2)
001654      IF(PMAX.GT.0) WRITE(N,40) PMAX,A1L,EPSI,EPSE
001655      40 FORMAT(6H PMAX=,13,5H A1L=,F7.4,6H EPSI=,F6.3,6H EPSE=,F6.3)
001656      WRITE(N,42)
001657      42 FORMAT("SPECIES GYRORADIUS MASS DIFFUSION J DENSITY DENS.GRA
001658      .D. 0MPSQ GYRFREQ.")
001659      NSPEC1 = MIN0(NSPEC,4)
001660      IF(N1.EQ.99) NSPEC1 = NSPEC
001661      DO 38 I = 1, NSPEC1
001662      WP2 = 0MPSQ*DENSE(I)*CHARG(I)**2/AMASS(I)
001663      WC = CHARG(I)/AMASS(I)
001664      WRITE(N,39) I,RLARM(I),AMASS(I),DFU(I),JAY(I),DENSE(I),EPS(I),
001665      WP2,WC
001666      39 FORMAT(15,3E10.2,15,4E10.2)
001667      38 CONTINUE
001668      RETURN
001669      END

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001670
001671      SUBROUTINE RHCALC(R,GAM,KOA,RHE)
001672      C CALCULATES THE RATIO OF THE ACTUAL PARTICLE DENSITY TO THE GUIDING
001673      C CENTER DENSITY AND STORES IT IN RHE. R IS THE MIRROR RATIO (R.LT.0
001674      C IS USED TO INDICATE A RING DISTRIBUTION), GAM IS THE DEGREE TO
001675      C WHICH THE LOSS CONE IS EMPTY AND KOA IS KO*LARMOR RADIUS.
001676      REAL KOA,KOSQ,KOSQR,J2(100)
001677      KOSQ = KOA*KOA
001678      IF(R.GT.0.) GO TO 1
001679      C RING DISTRIBUTION
001680      CALL QCALC(KOSQ,N,N,1)
001681      CALL BESSJ(KOA,N,J2)
001682      RHE = J2(1)
001683      RETURN
001684      C MAXWELLIAN OR LOSS-CONE DISTRIBUTION
001685      1 RHE = EXP(-.5*KOSQ)
001686      IF(GAM.GT.0.) GO TO 2
001687      RETURN
001688      C LOSS-CONE DISTRIBUTION
001689      2 KOSQR = KOSQ/R
001690      RHE = (R*RHE - GAM*EXP(-.5*KOSQR))/(R - GAM)
001691      RETURN
001692      END

```

```

001693
001694
001695 C COMPLEX DISP
001696 C FUNCTION DISP (OMEGA)
001697 C THIS ROUTINE CALCULATES THE DISPERSION FUNCTION
001698 C COMPLEX OMEGA, OMSQ, DETC, DO, D1, A(20,20), AP, BP, APP, BPP
001699 1 DEPOLE, SUM1, SUM2, DIV, DENOM, DN, PHI(18,22), OMEGA1, W, OMEGD
001700 C COMPLEX MAXW2, RING2, TERM(4)
001701 INTEGER P, PMAX, QMAX
001702 REAL MASS, KOAI, KOSQ, KYAI, KYSQ, MASQ, KPSQ, KXSQ
001703 LOGICAL DTACALC
001704 LOGICAL UNMAG
001705 COMPLEX ARH(20,20,4)
001706 COMMON/CBETA/ BETA
001707 COMMON/DIS/QF, KYSQ, KOSQ, EPSF(4), MASS, KYAI, KOAI, MASQ, PMAX, OMPSQ
001708 , AEAI, KMAX(4), AMASQ(4), EP(4), KMIN(4)
001709 COMMON/PHIC/ A, NRTSV, PHI
001710 COMMON/PMX/NPP
001711 COMMON/APBP/N, M, P
001712 COMMON/CCHIP/CHIP(4), AP(4), BP(4), OMEGA1, APP(4), BPP(4)
001713 COMMON/CDETL/ DTACALC, ARH
001714 COMMON/CSPEC/ RLARM(4), AMASS(4), CHARG(4), JAY(4), DENSE(4), NSPEC
001715 COMMON/CRBESJ/QMAX(4), NMAX(4)
001716 COMMON/CDFU/ DFU(4), DREL(4)
001717 COMMON/CMAG/UNMAG
001718 COMMON/CKXSQ/ KXSQ
001719 DATA DTACALC/. TRUE./
001720 DISP = (0., 0.)
001721 OMEGA1 = OMEGA
001722 OMSQ = OMEGA*OMEGA
001723 C IF YOU ARE RIGHT ON A SINGULARITY, MOVE OFF IT=
001724 4 DO 103 I = 1, NSPEC
001725 OMEGD = OMEGA + (0., 1.)*KYSQ*DFU(I)
001726 IF(CABS2(OMEGD).LT.1.E-26, AND.KOAI.NE.0.) GO TO 100
001727 IF(CABS2(OMEGD).LT.1.E-26, AND.DFU(I).NE.0.) GO TO 100
001728 W = OMEGD*AMASS(I)/CHARG(I)
001729 AW = ABS(REAL(W))
001730 DW = 1.E-13*AW
001731 IF(ABS(AIMAG(W)).GT.DW) GO TO 103
001732 IW = IFIX(AW)
001733 IF(AW - IW.GT.DW, AND.IW + 1. - AW.GT.DW) GO TO 103
001734 100 OMEGA = OMEGA + 3.E-13*AMAX1(1.,REAL(OMEGA))
001735 OMEGA1 = OMEGA
001736 OMSQ = OMEGA*OMEGA
001737 GO TO 102
001738 C 103 CONTINUE
001739 C DEPOLE IS USED TO GET RID OF ZEROS IN THE DENOMINATORS
001740 102 DEPOLE = (1., 0.)
001741 DO 2 I = 1, NSPEC
001742 OMEGD = OMEGA + (0., 1.)*KYSQ*DFU(I)
001743 IF(KOAI.EQ.0..AND.PMAX.GT.0) GO TO 23
001744 IF(EP(I).EQ.0..AND.PMAX.EQ.0) GO TO 23
001745 IF(I.EQ.1) GO TO 22
001746 IF(PMAX.EQ.0.AND.EP(I-1).EQ.0,) GO TO 22
001747 IF(DFU(I).EQ.DFU(I-1)) GO TO 23
001748 22 DEPOLE = OMEGD*DEPOLE
001749 23 IF(KMAX(I).EQ.0) GO TO 2
001750 KMX = KMAX(I)
001751 JI = KMIN(I)
001752 IF(PMAX.GT.0) GO TO 11
001753 DO 1 J = JI, KMX
001754 1 DEPOLE = DEPOLE*(OMEGD - J/AMASS(I))
001755 GO TO 2
001756 11 DO 12 J = JI, KMX
001757 12 DEPOLE = DEPOLE*(OMSQ - J*J/AMASQ(I))
001758 C 2 CONTINUE
001759 C THE FACTOR QF IS PUT IN TO MAKE DEPOLE ON THE ORDER OF 1
001760 DEPOLE = DEPOLE*QF
001761 IF(PMAX.GT.0) DEPOLE = DEPOLE*QF
001762
001763 C IF(PMAX.EQ.0) GO TO 10
001764 C CALCULATE DISP USING SINUSOIDAL DENSITY PROFILE IF PMAX.GT.0
001765 P=-PMAX-1
001766 M=1
001767 NP = PMAX+1
001768 C THE LOOP OVER ROWS IN THE DETERMINANT STARTS HERE
001769 C N IS THE INDEX OF THE ROWS, RUNNING FROM 1 TO 2PMAX +1
001770 C M IS THE COLUMN INDEX, WITH VALUES N-1,N,N+1
001771 DO 9 N=1, NP
001772 P=P+1
001773 C THIS SKIPS THE 1,0 ELEMENT WHICH IS NOT NEEDED
001774 IF(N.EQ.1) GO TO 40
001775 C THIS IS THE CALCULATION OF THE M=N-1 OR LEFT ELEMENTS
001776 A(N,M) = 0.
001777 DO 3 I = 1, NSPEC
001778 3 ARH(N,M,I) = EPSF(I)*(APP(I) + BPP(I))
001779 A(N,M) = A(N,M) + ARH(N,M,I)
001780 A(N,M) = A(N,M)*DEPOLE
001781 M=M+1
001782 C THIS IS THE CALCULATION OF THE DIAGONAL ELEMENTS
001783 40 CONTINUE
001784 CALL ABCALC
001785 A(N,M) = KYSQ + P*P*KOSQ
001786 DO 8 I = 1, NSPEC
001787 8 ARH(N,M,I) = OMPSQ*AP(I)*CHARG(I)**2*DENSE(I)/AMASS(I)
001788 A(N,M) = A(N,M) + ARH(N,M,I)
001789 A(N,M) = A(N,M)*DEPOLE
001790 M=M+1
001791 C THIS IS THE CALCULATION OF THE M=N+1 OR RIGHT ELEMENTS
001792 IF(N.EQ.NP) GO TO 60
001793 CALL ABCALC

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001793      A(N,M) = 0.
001794      DO 5 I = 1, NSPEC
001795      ARH(N,M,I) = EPSF(I)*(AP(I) - BP(I))
001796      5 A(N,M) = A(N,M) + ARH(N,M,I)
001797      A(N,M) = A(N,M)*DEPOLE
001798      M=M-1
001799      60 CONTINUE
001800      C 9 CONTINUE
001801      WE MAKE USE OF THE FACT THAT A(P,P') = A(-P',-P)
001802      N1 = NP
001803      NN1 = N1
001804      NP = 2*PMAX
001805      IF(NP.LT.NN1) GO TO 104
001806      DO 20 N = NN1,NP
001807      A(N,N+1) = A(N1-1,N1)
001808      A(N+1,N) = A(N1,N1-1)
001809      A(N+1,N+1) = A(N1-1,N1-1)
001810      DO 21 I = 1, NSPEC
001811      ARH(N,N+1,I) = ARH(N1-1,N1,I)
001812      ARH(N+1,N,I) = ARH(N1,N1-1,I)
001813      21 ARH(N+1,N+1,I) = ARH(N1-1,N1-1,I)
001814      20 N1 = N1-1
001815      C  THE DETERMINANT OF THE COEFFICIENTS, DETC, IS DONE HERE
001816      104 IF(.NOT.DTCALC) RETURN
001817      DETC=A(1,1)
001818      DN = 1
001819      IF(PMAX.EQ.0) GO TO 70
001820      DO 7 N=2,NPP
001821      DO=DN
001822      DN=DETC
001823      7 DETC=A(N,N)*DN-A(N,N-1)*A(N-1,N)*DO
001824      70 DISP=DETC/OMEGA
001825      RETURN
001826      C  CALCULATE DISP USING THE LOCAL APPROXIMATION IF PMAX.EQ.0
001827      10 KPSQ = KYSQ + KXSQ
001828      DO 15 I = 1, NSPEC
001829      OMEGD = OMEGA + (0., 1.)*KYSQ*DFU(I)
001830      IF(DENSE(I).EQ.0.) GO TO 110
001831      EPS = EP(I)
001832      IF(RLARM(I).GT.0.) GO TO 16
001833      C  SPECIES I IS COLD
001834      TERM(I) = -KPSQ - (1.+.5*BETA)*EPS*KYAI*CHARG(I)/(AMASS(I)*OMEGD)
001835      GO TO 13
001836      16 IF(JAY(I).GE.0) GO TO 17
001837      TERM(I) = RING2(OMEGA,KYAI,EPS,RLARM(I),AMASS(I),CHARG(I),NMAX(I),
001838      QMAX(I),OMEGD)
001839      GO TO 18
001840      17 EPSI = 2.*EPSF(I)*AMASS(I)/(OMPSQ*CHARG(I)**2*DENSE(I)*DREL(I))
001841      C  EPSI IS THE EPSI OR EPSE (DEPENDING ON WHETHER SPECIES I IS IONS OR
001842      C  ELECTRONS) USED IN *ROOTS*, DIVIDED BY DREL (=N(X)/NO). IT IS NEEDED
001843      C  IN *MAXW2* WHEN WE ARE USING THE HIGH GROWTH RATE SINUSOIDAL DISP. REL.
001844      C  TERM(I) = MAXW2( OMEGA, KYAI, EPS, RLARM(I), AMASS(I), CHARG(I), JAY(I),
001845      C  NMAX(I), QMAX(I), OMEGD, KOAI, EPSI, KPSQ, DREL(I))
001846      18 TERM(I) = TERM(I)/RLARM(I)**2
001847      13 TERM(I) = TERM(I)*AMASS(I)*DENSE(I)*DREL(I)
001848      GO TO 15
001849      110 TERM(I) = 0.
001850      15 CONTINUE
001851      DISP = KPSQ/OMPSQ + .5*BETA
001852      DO 19 I = 1, NSPEC
001853      19 DISP = DISP - TERM(I)
001854      DISP = DISP*DEPOLE
001855      RETURN
001856      END
001857

```

```

001858
001859      COMPLEX RING2
001860      FUNCTION RING2(W,KY,E,RLARM,AMASS,CHARG,NMAX,QMAX,WD)
001861      COMMON/BSTORE/ BJ(2000)
001862      COMPLEX OMEGA,W,SUM1,SUM2,WD,OMEGD
001863      INTEGER QMAX
001864      REAL KYAI,KY,KO,KOAI,KOSQ
001865      OMEGA = W*AMASS/CHARG
001866      OMEGD = WD*AMASS/CHARG
001867      KYAI = KY*RLARM
001868      EPS = E*RLARM
001869      CALL BESSJ(KYAI,NMAX,BJ)
001870      SUM1 = 0.
001871      IF(EPS.EQ.0.) GO TO 3
001872      SUM1 = BJ(1)*BJ(1)/OMEGD
001873      3 SUM2 = 0.
001874      DO 1 I = 1, QMAX
001875      AI = I
001876      SUM1 = SUM1 + BJ(I+1)*BJ(I+1)*(1. / (OMEGD-AI) + 1. / (OMEGD+AI))
001877      1 SUM2 = SUM2 + BJ(I+1)*(BJ(I) - BJ(I+2))*AI*(1. / (OMEGD-AI) - 1. /
001878      . (OMEGD+AI))
001879      SUM2 = SUM2*(1. + OMEGA*EPS/KYAI)
001880      SUM1 = -SUM1*EPS*KYAI
001881      RING2 = SUM1 + SUM2
001882      RETURN
001883      END

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001884
001885      COMPLEX MAXW2
001886      FUNCTION MAXW2(W,KY,E,RLARM,AMASS,CHARG,JAY,NMAX,QMAX,WD,
001887      KO,EPsi,KP,DREL)
001888      COMPLEX OMEGA,W,SUM1,SUM2,TP,TN,A1,WD,OMEGD
001889      COMPLEX IXKO,VP,VPPVD,VPMVD,ZEE
001890      COMPLEX CMIX,CPIX,ZVP,ZVPP,ZVPM
001891      INTEGER QMAX
001892      REAL KYAI,KY,KYSQ,KO,KOAI,KOSQ,KP,KPSQ,KPAI
001893      LOGICAL UNMAG,SNGLX
001894      COMMON/CXK/XKO
001895      COMMON/BSTORE/ BI(2000)
001896      COMMON/CMAG/UNMAG
001897      COMMON/CSNGLX/ SNGLX
001898      OMEGA = W*AMASS/CHARG
001899      OMEGD = WD*AMASS/CHARG
001900      KYAI = KY*RLARM
001901      KYSQ = KYAI*KYAI
001902      EPS = E*RLARM
001903
001904      IF(UNMAG) GO TO 4
001905      CALL BESSI(KYSQ,NMAX,BI)
001906      SUM1 = 0.
001907      IF(EPS.EQ.0.) GO TO 3
001908      SUM1 = BI(1)/OMEGD
001909      3 SUM2 = 0.
001910      DO 2 I = 1, QMAX
001911      AI = CMPLX(FLOAT(I),0.)
001912      TP = BI(I+1)/(OMEGD - AI)
001913      TN = BI(I+1)/(OMEGD + AI)
001914      SUM2 = SUM2 + AI*(TP - TN)
001915      2 SUM1 = SUM1 + TP + TN
001916      SUM2 = SUM2*(1. + OMEGA*EPS/KYAI)
001917      SUM1 = -SUM1*EPS*KYAI
001918      MAXW2 = SUM1 + SUM2
001919      RETURN
001920      4 KOAI = KO*RLARM
001921      KOSQ = KOAI*KOAI
001922      KPSQ = KP*RLARM*RLARM
001923      KPAI = SQRT(KPSQ)
001924      VP = SQRT(.5)*OMEGD/KPAI
001925      IF(.NOT.SNGLX) GO TO 5
001926      MAXW2 = -1. - OMEGA*EPS/KYAI - SQRT(.5)*(-EPS+ OMEGD*(1.+OMEGA*EPS
001927      /KYAI)/KYAI)*ZEE(VP)
001928      RETURN
001929      5 IXKO = CMPLX(0.,XKO)
001930      VDDOTK = KOAI*KYAI/KPAI
001931      VPPVD = SQRT(.5)*(OMEGD/KPAI + CMPLX(0.,VDDOTK))
001932      VPMVD = SQRT(.5)*(OMEGD/KPAI - CMPLX(0.,VDDOTK))
001933      CPIX = CEXP(IXKO)
001934      CMIX = CEXP(-IXKO)
001935      ZVP = ZEE(VP)
001936      ZVPP = ZEE(VPPVD)
001937      ZVPM = ZEE(VPMVD)
001938      EXPL = EXP(-.5*KOSQ)
001939      MAXW2 = EXPL*(.5*CMIX*VPPVD*ZVPP + .5*CPIX*VPMVD*ZVPM )
001940      MAXW2 = -1. - MAXW2*EPsi - VP*ZVP/DREL
001941      RETURN
001942      END

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001943
001944      SUBROUTINE QFKCAL(QF,KMAX,KMIN,RMX,RMIN)
001945      LOGICAL UNMAG
001946      DIMENSION KMAX(4), KMIN(4)
001947      COMMON/CSPEC/ RLARM(4),AMASS(4),CHARG(4),JAY(4),DENSE(4),NSPEC
001948      COMMON/CMAG/UNMAG
001949      Q = 1.
001950      DO 11 I = 1, NSPEC
001951      IF(UNMAG) GO TO 87
001952      IF(DENSE(I).EQ.0.) GO TO 87
001953      IF(I.EQ.1) GO TO 91
001954      DO 85 J = 2, I
001955      85 IF(AMASS(I).EQ.AMASS(J - 1).AND.DENSE(J-1).NE.0.) GO TO 87
001956      91 KMAX(I) = RMX*AMASS(I)
001957      KMIN(I) = (RMIN - 2.)*AMASS(I)
001958      IF(KMIN(I).LT.1) KMIN(I) = 1
001959      GO TO 88
001960      87 KMAX(I) = 0
001961      88 IF(KMAX(I).EQ.0) GO TO 11
001962      KMX = (KMAX(I) - KMIN(I))/2 + 1
001963      DO 86 K = 1, KMX
001964      86 Q = FLOAT(K)*Q/AMASS(I)
001965      11 CONTINUE
001966      QF = 1. / (Q*Q)
001967      RETURN
001968      END

```

```

001969      SUBROUTINE QCALC(CHI,QMAX,NMAX,N)
001970      INTEGER QMAX
001971      COMMON/CQN/MINQ
001972      IF(N.GT.0) GO TO 1
001973      C THIS IS USED FOR A MAXWELLIAN DISTRIBUTION OF IONS,
001974      C QMAX IS MADE LARGE ENOUGH SO THAT MODIFIED BESSEL FUNCTIONS OF INDEX
001975      C GREATER THAN QMAX ARE LESS THAN 1.E-03
001976      C THE PARAMETER NMAX USED IN THE SUBROUTINE BESSI IS CHOSEN SO THAT
001977      C IF(CHI.LE.64.) AMAX = 28.
001978      C IF(CHI.GT.64.) AMAX = 3.5*SQRT(CHI)
001979      C NMAX = AMAX
001980      C QMAX AND NMAX MUST BE SIGNIFICANTLY MORE THAN THE HIGHEST CYCLOTRON
001981      C HARMONIC SOUGHT.
001982      C IF(NMAX.LT.MINQ) NMAX = MINQ
001983      C IF NMAX IS TOO GREAT BESSI WILL OVERFLOW.
001984      C IF(NMAX.GT.1988) NMAX = 1988
001985      C QMAX = NMAX
001986      C RETURN
001987      C THIS IS USED FOR RING DISTRIBUTIONS OF IONS.
001988      C QMAX IS MADE LARGE ENOUGH SO THAT BESSEL FUNCTIONS OF INDEX
001989      C GREATER THAN QMAX ARE LESS THAN 1.E-05.
001990      C 1 QMAX = 10
001991      C IF(CHI.GT.4.) QMAX = SQRT(CHI) + 6.5*CHI**.166667
001992      C 2 THE PARAMETER NMAX USED IN THE SUBROUTINE BESSJ IS CHOSEN SO THAT
001993      C THE BESSEL FUNCTIONS ARE GOOD TO 10 DECIMAL PLACES.
001994      C NMAX = 15
001995      C IF(CHI.GT.9.) NMAX = SQRT(CHI) + 11.*CHI**.166667
001996      C IF(NMAX.GT. 398) NMAX = 398
001997      C IF(QMAX.GT.NMAX - 2) QMAX = NMAX - 2
001998      C RETURN
001999      C END
002000

```

```

002001      SUBROUTINE BESSI(X,N,BI)
002002      DIMENSION BI(2000)
002003      N1 = N+1
002004      IF (X.LT.1.E-14) GO TO 4
002005      BI(N+2) = 0.
002006      BI(N+1) = 1.
002007      DO 1 I = 1, N
002008      M = N - I + 1
002009      AM1 = M
002010      1 BI(M) = (2.*AM1/X)*BI(M+1) + BI(M+2)
002011      SUM = BI(1)/2.
002012      DO 2 M = 2, N1
002013      2 SUM = SUM + BI(M)
002014      SUM = SUM + SUM
002015      DO 3 I = 1, N1
002016      3 BI(I) = BI(I)/SUM
002017      GO TO 6
002018      4 BI(1) = 1.
002019      DO 5 I = 2, N1
002020      5 BI(I) = 0.
002021      6 RETURN
002022      END
002023

```

```

002024      SUBROUTINE BESSJ (X,N,BJ)
002025      DIMENSION BJ(400)
002026      N1 = N+1
002027      IF (X.LT.1.E-14) GO TO 4
002028      BJ(N+2) = 0.
002029      BJ(N+1) = 1.
002030      DO 1 I = 1, N
002031      M = N - I + 1
002032      AM1 = M
002033      1 BJ(M) = (2.*AM1/X)*BJ(M+1) - BJ(M+2)
002034      SUM = BJ(1)/2.
002035      N2 = N/2
002036      DO 2 M = 1, N2
002037      2 SUM = SUM + BJ(M+M+1)
002038      SUM = SUM + SUM
002039      DO 3 I = 1, N1
002040      3 BJ(I) = BJ(I)/SUM
002041      GO TO 6
002042      4 BJ(1) = 1.
002043      DO 5 I = 2, N1
002044      5 BJ(I) = 0.
002045      6 RETURN
002046      END
002047

```

```

002048
002049     FUNCTION CABS2(Z)
002050     COMPLEX Z
002051     CABS2 = Z*C0NJC(Z)
002052     RETURN
002053     END

```

```

002054
002055     COMPLEX ZEE
002056     FUNCTION ZEE(X)
002057     COMPLEX X, TERM
002058     DOUBLE PRECISION RZED, IZED, RTERMD, ITERMD, RTNEW, RX2, IX2
002059     DATA PI/3.14159265359/
002060     ABX2 = CABS2(X)
002061     C IF ABS(X) IS GREATER THAN 5.7, USE THE ASYMPTOTIC FORM.
002062     IF(ABX2.GT.33.) GO TO 4
002063     ZEE = (0., 1.)*SQRT(P1)*CEXP(-X*X)
002064     IF(ABX2.GT.1.) NMAX = 2.8*ABX2 + 19.
002065     IF(ABX2.LE.1.) NMAX = 11.*ABX2 + 10.
002066     TERM = 2.*X
002067     C IF ABS(X) IS GREATER THAN 2.6, WE MUST USE DOUBLE PRECISION IF ZEE IS
002068     TO BE ACCURATE TO 1.E-12.
002069     IF(ABX2.GT.7.) GO TO 2
002070     DO 1 N = 1, NMAX
002071     ZEE = ZEE - TERM
002072     1 TERM = -TERM*2.*X*X/(2*N + 1)
002073     RETURN
002074     2 RX2 = REAL(X*X)
002075     IX2 = AIMAG(X*X)
002076     RZED = REAL(ZEE)
002077     IZED = AIMAG(ZEE)
002078     RTERMD = REAL(TERM)
002079     ITERMD = AIMAG(TERM)
002080     DO 3 N = 1, NMAX
002081     RZED = RZED - RTERMD
002082     IZED = IZED - ITERMD
002083     RTNEW = -2.* (RX2*RTERMD - IX2*ITERMD)/(2*N + 1)
002084     ITERMD = -2.* (RX2*ITERMD + IX2*RTERMD)/(2*N + 1)
002085     3 RTERMD = RTNEW
002086     RZEE = RZED
002087     AZEE = IZED
002088     ZEE = CMPLX(RZEE, AZEE)
002089     RETURN
002090     4 NMAX = 20
002091     TERM = 1./X
002092     ZEE = 0.
002093     DO 5 N = 1, NMAX
002094     ZEE = ZEE - TERM
002095     5 TERM = FLOAT(2*N-1)*TERM/(2.*X*X)
002096     RETURN
002097     END

```

```

002098
002099     SUBROUTINE ABCALC
002100     C THIS IS AN INTERFACE BETWEEN DISP AND THE ROUTINES MAXW, RING, AND
002101     COLD WHICH CALCULATE THE ALPHAS AND BETAS.
002102     DIMENSION CHIP1(4)
002103     COMPLEX AP, BP, OMEGA, W, APP, BPP
002104     REAL J1(400,4), J2(400,4)
002105     COMMON/CCHIP/CHIP(4),AP(4),BP(4), OMEGA, APP(4),BPP(4)
002106     COMMON/CSPEC/ RLARM(4),AMASS(4),CHARG(4),JAY(4),DENSE(4),NSPEC
002107     DO 5 I = 1, NSPEC
002108     IF(DENSE(I).EQ.0.) GO TO 6
002109     W = OMEGA*AMASS(I)/CHARG(I)
002110     IF(RLARM(I).EQ.0.) GO TO 7
002111     IF(JAY(I).GE.0) CALL MAXW(W,RLARM(I),AP(I),BP(I),APP(I),BPP(I),
002112     .CHIP(I),CHIP1(I),I)
002113     IF(JAY(I).LT.0) CALL RING(W,RLARM(I),AP(I),BP(I),APP(I),BPP(I),
002114     .CHIP(I),CHIP1(I),J1(I,I),J2(I,I))
002115     FACTOR = (AMASS(I)/(CHARG(I)*RLARM(I)))**2
002116     AP(I) = AP(I)*FACTOR
002117     BP(I) = BP(I)*FACTOR
002118     APP(I) = APP(I)*FACTOR
002119     BPP(I) = BPP(I)*FACTOR
002120     GO TO 5
002121     6 AP(I) = 0.
002122     BP(I) = 0.
002123     APP(I) = 0.
002124     BPP(I) = 0.
002125     GO TO 5
002126     7 CALL COLD(W,AP(I),BP(I),APP(I),BPP(I),CHIP(I),CHIP1(I))
002127     FACTOR = (AMASS(I)/CHARG(I))**2
002128     AP(I) = AP(I)*FACTOR
002129     BP(I) = BP(I)*FACTOR
002130     APP(I) = APP(I)*FACTOR
002131     BPP(I) = BPP(I)*FACTOR
002132     5 CONTINUE
002133     RETURN
002134     END

```

```

002135
002136      SUBROUTINE MAXW(CMEGA,RLARM,AP,BP,APP,BPP,LAMDP,LAMDP1,K)
002137      C THIS ROUTINE CALCULATES ALPHAS AND BETAS FOR A MAXWELLIAN DISTRIBUTI
002138      CION DIMENSION IPP(2000)
002139      C COMPLEX CMEGA, UMEGA, @MSQ, AP, BP, DIV, DENOM, SUM1, SUM2, VP, ZEE
002140      C COMPLEX APP, BPP, EIAP, EIQAP, SUM3, SUM4, VPM, VPP, ZVPP, ZVPM
002141      C REAL MASS, KOAI, KOSQ, KYAI, KYSQ, MASQ, LAMDP, LAMDP1, LAM, IPP
002142      C INTEGER PMAX, P, QMAX
002143      C LOGICAL UNMAG
002144      C COMMON/DIS/QF, CYSQ, COSQ, EPSF(4), MASS, CYAI, COAI, MASQ, PMAX, @MPGQ
002145      C , AEAI, KMAX(4), AMASQ(4), EPS(4), KMIN(4)
002146      C COMMON/APBP/N, M, P
002147      C COMMON/CRBESJ/QMAX(4), NMAX1(4)
002148      C COMMON/CMAG/ UNMAG
002149      C NQ = QMAX(K) + 1
002150      C NMAX = NMAX1(K)
002151      C KYAI = CYAI*RLARM
002152      C KYSQ = KYAI*KYAI
002153      C KOAI = COAI*RLARM
002154      C KOSQ = KOAI*KOAI
002155      C @MSQ = @MEGA*CMEGA
002156      C IF(M,NE,N) GO TO 2
002157      C IF(N, EQ, 1) LAMDP1= SQRT(KYSQ + PMAX*PMAX*KOSQ)
002158      C LAMDP = LAMDP1
002159      C LAMDP1 = SQRT(KYSQ + (P+1)*(P+1)*KOSQ)
002160      C LAM = LAMDP*LAMDP
002161      C IF(UNMAG) GO TO 7
002162      C CALL BESSI(LAM,NMAX,IPP)
002163      C SUM1 = 0.
002164      C D0 5 K1=2,NQ
002165      C Q=K1-1
002166      C DENOM = (1.,0.)/(@MSQ - Q*Q)
002167      C 5 SUM1= SUM1+ IPP(K1)*DENOM*Q*Q
002168      C AP = -2.0*SUM1
002169      C BP= 0.
002170      C APP = 0.
002171      C BPP = 0.
002172      C RETURN
002173      C 7 VP = @MEGA/SQRT(2.*LAM)
002174      C AP = 1. + VP*ZEE(VP)
002175      C BP = 0.
002176      C APP = 0.
002177      C BPP = 0.
002178      C RETURN
002179      C 2 IF(M,NE,N+1) GO TO 3
002180      C LAM = LAMDP1 * LAMDP
002181      C EXPL = EXP(-.5*(LAMDP1 - LAMDP)**2)
002182      C IF(UNMAG) GO TO 8
002183      C EIAP = (KYSQ + P*(P+1)*KOSQ -(0.,1.)*KOAI*KYAI)/LAM
002184      C CALL BESSI(LAM,NMAX,IPP)
002185      C SUM1 = 0.
002186      C SUM2 = IPP(1)/@MEGA
002187      C SUM3 = 0.
002188      C SUM4 = SUM2
002189      C EIQAP = 1.
002190      C D0 6 K1=2,NQ
002191      C Q=K1-1
002192      C EIQAP = EIQAP*EIAP
002193      C SUM1 = SUM1 + Q*IPP(K1)*(EIQAP/(@MEGA-Q) - 1. / (EIQAP*(@MEGA+Q)))
002194      C SUM2 = SUM2 + IPP(K1)*(EIQAP/(@MEGA-Q) + 1. / (EIQAP*(@MEGA+Q)))
002195      C SUM3 = SUM3 + Q*IPP(K1)*(1. / (EIQAP*(@MEGA-Q)) - EIQAP/(@MEGA+Q))
002196      C 6 SUM4 = SUM4 + IPP(K1)*(1. / (EIQAP*(@MEGA-Q)) + EIQAP/(@MEGA+Q))
002197      C AP = -EXPL*SUM1
002198      C BP = (0.,1.)*KOAI*KYAI*EXPL*SUM2
002199      C APP = -EXPL*SUM3
002200      C BPP = (0.,1.)*KOAI*KYAI*EXPL*SUM4
002201      C RETURN
002202      C 8 SQ2LM = SQRT(2.*LAM)
002203      C VP = @MEGA/SQ2LM
002204      C VPM = (@MEGA - (0.,1.)*KYAI*KOAI)/SQ2LM
002205      C VPP = (@MEGA + (0.,1.)*KYAI*KOAI)/SQ2LM
002206      C ZVPP = ZEE(VPP)
002207      C ZVPM = ZEE(VPM)
002208      C EXPL = EXP(-.5*KOSQ)
002209      C AP = EXPL*(1. + VP*ZVPP)
002210      C BP = -(0.,1.)*KOAI*KYAI*EXPL*ZVPP /SQ2LM
002211      C APP= EXPL*(1. + VP*ZVPM)
002212      C BPP= -(0.,1.)*KOAI*KYAI*EXPL*ZVPM /SQ2LM
002213      C RETURN
002214      C 3 AP = 0.
002215      C BP = 0.
002216      C APP = 0.
002217      C BPP = 0.
002218      C RETURN
002219      C END

```

```

002220
002221      SUBROUTINE RING (OMEGA, RLARM, AP, BP, APP, BPP, CHIP, CHIP1, J1, J2, K)
002222      C CALCULATES THE ALPHAS AND BETAS FOR A RING DISTRIBUTION.
002223      DIMENSION J1(1), J2(1)
002224      COMPLEX OMEGA, UMEGA, GMSQ, AP, BP, DIV, DENOM, SUM1, SUM2
002225      COMPLEX SUM3, SUM4, EIAP, EIQAP, APP, BPP
002226      REAL MASS, KOAI, KO$Q, KYAI, KYSQ, MA$Q, J1, J2, JP1, JP2
002227      INTEGER PMAX, P, QMAX
002228      COMMON/DIS/QF, CYSQ, COSQ, EPSF(4), MASS, CYAI, COAI, MASQ, PMAX, CMPSQ
002229      , AEAI, KMAX(4), AMASQ(4), EPS(4), KMIN(4)
002230      COMMON/APBP/N, M, P
002231      COMMON/CRBESJ/QMAX(4), NMAX1(4)
002232      NMAX = NMAX1(K)
002233      NQ = QMAX(K) + 1
002234      NQ1 = NQ + 1
002235      KYAI = CYAI*RLARM
002236      KYSQ = KYAI*KYAI
002237      KOAI = COAI*RLARM
002238      KOSQ = KOAI*KOAI
002239      OMSQ = OMEGA*OMEGA
002240      IF(M.NE.N) GO TO 2
002241      IF(N.EQ.1) CHIP1 = SQRT(KYSQ + PMAX*PMAX*KOSQ)
002242      IF(N.EQ.1) CALL BESSJ(CHIP1, NMAX, J2)
002243      CHIP = CHIP1
002244      DO 7 K1 = 1, NQ1
002245      7 J1(K1) = J2(K1)
002246      CHIP1 = SQRT(KYSQ + (P+1)*(P+1)*KOSQ)
002247      CALL BESSJ(CHIP1, NMAX, J2)
002248      SUM1 = 0.
002249      DO 5 K1=2, NQ
002250      Q=K1-1
002251      DENOM = (1., 0.)/(OMSQ-Q*Q)
002252      JP1 = .5*(J1(K1-1) - J1(K1+1))
002253      5 SUM1 = SUM1 + Q*Q*JP1*K1*(K1)*DENOM
002254      AP = -4.0*SUM1*CHIP
002255      BP = 0.
002256      APP = 0.
002257      BPP = 0.
002258      RETURN
002259      2 IF(M.NE.N+1) GO TO 3
002260      EIAP = (KYSQ + P*(P+1)*KOSQ - (0., 1.)*KOAI*KYAI)/(CHIP*CHIP1)
002261      SUM1 = 0.
002262      SUM2 = J1(1)*J2(1)/OMEGA
002263      SUM3 = 0.
002264      SUM4 = SUM2
002265      EIQAP = 1.
002266      DO 6 K1=2, NQ
002267      Q=K1-1
002268      EIQAP = EIQAP*EIAP
002269      JP1 = .5*(J1(K1-1) - J1(K1+1))
002270      JP2 = .5*(J2(K1-1) - J2(K1+1))
002271      SUM1 = SUM1 + Q*(CHIP*JP1*K2(K1) + CHIP1*JP2*K1(K1))*(EIQAP/
002272      *(OMEGA-Q) - 1. / (EIQAP*(OMEGA+Q)))
002273      SUM2 = SUM2 + J1(K1)*J2(K1)*(EIQAP/(OMEGA-Q) + 1. / (EIQAP*(OMEGA+Q))
002274      )
002275      SUM3 = SUM3 + Q*(CHIP*JP1*K2(K1) + CHIP1*JP2*K1(K1))*(1. / (EIQAP*
002276      *(OMEGA-Q)) - EIQAP/(OMEGA+Q))
002277      6 SUM4 = SUM4 + J1(K1)*J2(K1)*(1. / (EIQAP*(OMEGA-Q)) + EIQAP/(OMEGA+Q)
002278      )
002279      AP = -SUM1
002280      BP = (0., 1.)*KOAI*KYAI*SUM2
002281      APP = -SUM3
002282      BPP= (0., 1.)*KOAI*KYAI*SUM4
002283      RETURN
002284      3 AP = 0.
002285      BP = 0.
002286      APP = 0.
002287      BPP = 0.
002288      RETURN
002289      END

```

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002290
002291      SUBROUTINE COLD(OMEGA, AP, BP, APP, BPP, CHIP, CHIP1)
002292      C CALCULATES ALPHAS AND BETAS FOR COLD ELECTRONS
002293      COMPLEX OMEGA, OMSQ, DIV, AP, BP, APP, BPP
002294      REAL MASS, KOAI, KOSQ, KYAI, KYSQ, MASQ
002295      INTEGER PMAX, P
002296      COMMON/DIS/QF, KYSQ, KOSQ, EPSF(4), MASS, KYAI, KOAI, MASQ, PMAX, CMPSQ
002297      , AEA1, KMAX(4), AMASQ(4), EPS(4), KMIN(4)
002298      COMMON/APBP/N, M, P
002299      OMSQ = OMEGA*OMEGA
002300      IF(M.NE.N) GO TO 2
002301      IF(N.EQ.1) CHIP1 = SQRT(KYSQ + PMAX*PMAX*KOSQ)
002302      CHIP = CHIP1
002303      CHIP1 = SQRT(KYSQ + (P+1)*(P+1)*KOSQ)
002304      AP = -CHIP*CHIP/(OMSQ - 1.)
002305      BP = 0.
002306      APP = 0.
002307      BPP = 0.
002308      RETURN
002309      2 COSAP = (KYSQ + P*(P+1)*KOSQ)/(CHIP*CHIP1)
002310      SINAP = -KOAI*KYAI/(CHIP*CHIP1)
002311      AP = -CHIP*CHIP1*(COSAP + (0., 1.)*OMEGA*SINAP)/(OMSQ - 1.)
002312      APP = -CHIP*CHIP1*(COSAP - (0., 1.)*OMEGA*SINAP)/(OMSQ - 1.)
002313      IF(KOAI.NE.0.) GO TO 1
002314      BP = 0.
002315      BPP = 0.
002316      RETURN
002317      1 BP = KOAI*KYAI/OMEGA
002318      BP = CMPLX(-AIMAG(BP), REAL(BP))
002319      BPP = BP
002320      RETURN
002321      END

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002322
002323      SUBROUTINE SAVPHI
002324      C FINDS PHI(P)
002325      COMPLEX PHI(18,22), A(20,20), PHI1(19), PHI2(19)
002326      COMMON /PHIC/ A, NRTSV, PHI
002327      COMMON/PMX/ NP
002328      DATA NRTSV/1/
002329      IF(NRTSV.LT.19) GO TO 1
002330      CALL EIGPLT
002331      NRTSV = 1
002332      1 PHI1(1) = (1.0,0.0)
002333      IF((NP-1)/2.EQ.0) GO TO 5300
002334      PHI1(2) = -A(1,1)/A(1,2)
002335      DO 5301 K2 = 3, NP
002336      K1 = K2-1
002337      PHI1(K2) = -(A(K1,K1-1)*PHI1(K1-1)+A(K1,K1)*PHI1(K1))/A(K1,K2)
002338      5301 CONTINUE
002339      PHI2(NP) = PHI1(NP)
002340      PHI2(NP-1) = -A(NP,NP)*PHI2(NP)/A(NP,NP-1)
002341      DO 5302 K2 = 3, NP
002342      K1 = NP-K2+1
002343      PHI2(K1) = -(A(K1+1,K1+1)*PHI2(K1+1)+A(K1+1,K1+2)*PHI2(K1+2))
002344      /A(K1+1,K1)
002345      5302 CONTINUE
002346      DO 5303 K1 = 1, NP
002347      PHI(NRTSV,K1) = 0.5*(PHI1(K1) + PHI2(K1))
002348      5303 CONTINUE
002349      5300 CONTINUE
002350      RETURN
002351      END

```

```

002352
002353      SUBROUTINE PAGE
002354      COMMON/CIO/ICR, IHSP, IGRAPH
002355      WRITE(IHSP,1)
002356      1 FORMAT(1H1)
002357      RETURN
002358      END

```

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002358
002359      SUBROUTINE MRAF(F, RT, CONV, NRTS, PP1, PP2, PP3, EP1, EP2, MXM)
002360      DIMENSION ARPHI(80), ABPHI(80)
002361      LOGICAL PHIZ(200), WARN
002362      LOGICAL CONV(200)
002363      LOGICAL NOCONJ, NONEG, NOPHNU
002364      LOGICAL SW1, SW2, SW3, SW4, SW5, SWR, SW7, SWR1, NREDH, SW31, SW71
002365      COMPLEX PHI(18,22), A(20,20), PHJ
002366      COMPLEX F, RT(200), PP1, PP2, PP3, P1, P2, P3, CHANGE
002367      COMPLEX H, ROOT, FUNC, FROOT
002368      COMPLEX DNR, FX1, FX2, FX3, FX21, FX32, FX321, RH0, T, X1, X2, X3, W
002369      COMPLEX PHI NEW(20)
002370      REAL EP3, FRMAX, XMAX
002371      REAL TEST, XR
002372      REAL KYA1
002373      REAL EP1, EP2
002374      INTEGER NRTS, MXM
002375      INTEGER RTC, ITC
002376      INTEGER PMAX, EIGV, FAILC
002377      INTEGER I, NCR, LNCR, NRET
002378      COMMON/CIO/ ICR, IHSP, IGRAPH
002379      COMMON/CMRAF2/ ERRMAX, NRTSU, SW31, SW71
002380      COMMON /PHIC/ A, NRTSV, PHI
002381      COMMON/PMX/NPP
002382      COMMON/CPHZ/ PHIZ
002383      COMMON/CMRAF/SW1, SW2, SW3, SW4, SW5, SWR, RTC, ITC, EP3, FRMAX, XMAX
002384      , H, ROOT, FUNC, FROOT, EIGV, SW7, START, RMX, NFL, KYA1
002385      COMMON/CPHCK/ PHI NEW, PHZP
002386      DATA SW1, SW2, SW3, SW4, SW5, SWR/6*(.FALSE.)/
002387      DATA SW7/.FALSE./
002388      DATA RTC, EP3, FRMAX, XMAX/0.0., 10., 10./
002389      DATA ERRMAX/ 1.E+20/
002390      C 'MULLER'S (METHOD FOR) ROOTS (OF A LOCALLY) ANALYTIC FUNCTION'.
002391      C NRTS ROOTS OF F(Z) WILL BE FOUND (HOPEFULLY) AND PLACED IN ARRAY
002392      C RT(NRTS).
002393      C P1, P2, P3 ARE STARTING VALUES FOR THE SEARCH (EXCEPT SEE SW5 BELOW).
002394      C ROOTS NEAREST THE STARTING VALUES WILL BE FOUND FIRST, ROUGHLY.
002395      C EP1, EP2 ARE CONVERGENCE TOLERANCE PARAMETERS.
002396      C A ROOT IS CONSIDERED TO HAVE BEEN FOUND IF..
002397      C   (1) THE MODULUS OF THE RELATIVE DIFFERENCE OF TWO ITERANTS .LT. EP1
002398      C   (2) MODULII OF THE FUNCTION AND MODIFIED FUNCTION VALUES BOTH .LT.
002399      C     EP2.
002400      C 'MODIFIED FUNCTION' MEANS F(Z)/DNR, WHERE DNR=PRODUCT (Z-RT(I)),
002401      C THE PRODUCT BEING OVER ALL PREVIOUSLY FOUND ROOTS.
002402      C IF MXM ITERATIONS ON ROOT I DOES NOT PRODUCE CONVERGENCE, ITERATION
002403      C STOPS. WHAT HAPPENS NEXT DEPENDS ON SW4 - DEFAULT PROCEDURE IS TO
002404      C SET THE REST OF THE ARRAY CONV=.FALSE. AND RETURN.
002405
002406      C IF SW1 INFORMATION ABOUT EACH ROOT FOUND IS PRINTED.
002407      C IF SW2, THEN INFORMATION ABOUT EACH ITERANT OF EACH ROOT IS PRINTED.
002408      C IF SW3, THEN THE CONJUGATE OF EACH NON-REAL ROOT FOUND IS CONSIDERED
002409      C TO BE A ROOT ALSO.
002410      C IF SW4, SOME ATTEMPT IS MADE TO CONTINUE AFTER FAILURE TO CONVERGE
002411      C ON A ROOT. THE LATEST ITERANT IS ASSIGNED TO RT(I) AND CONV(I)=
002412      C .FALSE. (ELSE CONV(I)=.TRUE.), AND WE CONTINUE NORMALLY. THE
002413      C MODIFIED FUNCTION NOW HAS A POLE AT THIS FALSE ROOT. BUT
002414      C GENERALLY WE SEEM NOW TO CONVERGE TO A ROOT, SO IT CAN BE
002415      C WORTHWHILE CONTINUING, IF THERE ARE MORE ROOTS ASKED FOR. THIS
002416      C IS ESPECIALLY TRUE IN CASES OF SLOW CONVERGENCE TO MULTIPLE ROOTS.
002417      C WHEN NRTS (GOOD OR BAD) ROOTS HAVE BEEN FOUND, MRAF WILL GO BACK
002418      C AND TRY TO RE-DO THE NONCONVERGENT ROOT ESTIMATES. ON RETURN, CONV
002419      C WILL INDICATE WHICH ROOTS ARE GOOD.
002420      C IF SW5, THE STARTING VALUES IN THE SEARCH FOR ROOT I WILL BE PP1 ETC.
002421      C PLUS WHATEVER WAS IN RT(I) ON ENTRY.
002422      C IF SW7 THE NEGATIVE CONJUGATE OF EACH ROOT FOUND IS CONSIDERED TO BE
002423      C A ROOT.
002424      C IF SWR, ONLY REAL ROOTS ARE FOUND, AND ONLY REAL ARGUMENTS ARE GIVEN
002425      C TO F, ALTHOUGH F ITSELF IS STILL A COMPLEX FUNCTION (UNLESS YOUR
002426      C COMPILER RETURNS REAL FUNCTION VALUES IN THE SAME PLACE AS THE
002427      C REAL PART OF COMPLEX FUNCTION VALUES).
002428      C IN GENERAL IT IS EASIER TO SOLVE FOR ALL ROOTS INSTEAD OF ONLY REAL
002429      C ROOTS, ESPECIALLY IF THERE ARE ROOTS NEAR REAL AXIS IN REGION OF
002430      C INTEREST.
002431      C (IN REVISED VERSION OF PROGRAM, SWR IS TEMPORARILY MADE FALSE IF THERE
002432      C IS OBVIOUSLY A COMPLEX ROOT NEARBY. IF SWR IS TRUE THEN REAL ROOTS ARE
002433      C FOUND MORE QUICKLY, SO IT IS BETTER TO SET SWR TRUE INITIALLY. - MJG
002434      C IF RTC.LT.0 ON ENTRY, WE CONTINUE WITHOUT REINITIALIZING JUST AS
002435      C THOUGH WE WERE ABOUT TO LOOK FOR ROOT ABS(RTC)+1.
002436      C THE MODIFIED FUNCTION IS NOT WELL DEFINED CLOSE TO ROOTS ALREADY
002437      C FOUND. THE RELATIVE SIZE OF THE REGION OF INDETERMINACY IS TAKEN
002438      C TO BE EP3. A STARTING VALUE IN SUCH A REGION WILL BE MOVED OUT
002439      C BEFORE CONTINUING. AN ITERANT THERE WILL BE ASSUMED TO BE ANOTHER
002440      C ROOT.
002441      C THE NORMAL ITERATION IS ALTERED IN SOME CASES WHERE THE METHOD
002442      C OTHERWISE TENDS TO GET LOST.
002443      C H IS THE DIFFERENCE BETWEEN 2 ITERANTS. THE RATIO OF TWO SUCCESSIVE
002444      C H'S NEVER EXCEEDS XMAX. IF A NEWLY FOUND H IS TOO LARGE, ITS
002445      C MAGNITUDE IS DECREASED BUT ITS DIRECTION IS PRESERVED.
002446      C IF THE RATIO OF THE MODIFIED FUNCTION AT TWO SUCCESSIVE ITERANTS
002447      C EXCEEDS FRMAX, THE LATEST ITERATION IS DISCARDED AND THE H FOR
002448      C THAT ITERATION IS NOW TAKEN TO BE THE SAME AS IN THE PRECEDING
002449      C ITERATION.
002450      C IF YOU DON'T ASSIGN ANYTHING TO A CMRAF VARIABLE YOU GET THE DEFAULT
002451      C SET BY THE DATA STATEMENTS. A COROLLARY IS THAT YOU SHOULDN'T TRY
002452      C SETTING THEM BY DATA STATEMENTS IN YOUR PROGRAM.

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002454 C THE PROCEDURE MAY BE THOUGHT OF AS A GENERATION OF A SEQUENCE Z(I)
 002455 C WHOSE LIMIT IS A ROOT OF F AND WHOSE FIRST 3 ELEMENTS ARE Z(-1)=P1,
 002456 C Z(0)=P2, Z(1)=P3. A QUADRATIC IS FITTED TO THE FUNCTION AT THREE
 002457 C ELEMENTS Z(I-2), Z(I-1), Z(I). USING NEWTON'S DIVIDED DIFFERENCES,
 002458 C Z(I+1) IS NORMALLY THAT ROOT OF THE QUADRATIC CLOSEST TO Z(I).
 002459 C SINCE THE FITTED FUNCTION, A QUADRATIC, IS ANALYTIC WE SHOULD NOT
 002460 C BE SURPRISED WHEN THE METHOD FAILS ON NON-ANALYTIC FUNCTIONS.
 002461 C THE USER CAN OFTEN HELP GREATLY BY MAKING HIS FUNCTION WELL-
 002462 C BEHAVED IN THE REGION OF INTEREST, BY MULTIPLYING HIS ORIGINAL
 002463 C FUNCTION BY ANOTHER WHICH CANCELS SINGULARITIES IN THE ORIGINAL
 002464 C WITHOUT ADDING ANYTHING MORE.
 002465 C CLOSE TO A SINGLE ROOT CONVERGENCE IS LITTLE FASTER THAN FOR THE
 002466 C SECANT METHOD, BECAUSE THE ONLY ADDITIONAL INFORMATION USED IS FROM
 002467 C X(I-2), WHICH IS A LONG WAY OFF.
 002468 C HOWEVER CONVERGENCE TO MULTIPLE ROOTS IS IMPROVED OVER THE SECANT OR
 002469 C NEWTON-RAPHSON METHODS. IN PARTICULAR CONVERGENCE TO DOUBLE ROOTS
 002470 C IS ABOUT AS FAST AS TO SIMPLE ROOTS.
 002471 C THIS METHOD IS CAPABLE OF FINDING COMPLEX ZEROS OF A FUNCTION WHICH
 002472 C IS REAL FOR REAL ARGUMENT, USING REAL STARTING VALUES. THIS IS NOT
 002473 C TRUE OF, FOR INSTANCE, NEWTON-RAPHSON OR THE SECANT METHOD.
 002474 C
 002475 C THIS PROGRAM BEGAN AS A FORTRAN TRANSLATION OF CACM ALGORITHM 196,
 002476 C INCORPORATING CHANGES SUGGESTED BY J. TRAUB AND THE CERTIFICATION
 002477 C APPEARING IN THE CACM, JAN. 1968, P12, THEN SOME REMAINING GLITCHES
 002478 C WERE REMOVED AND NEW FEATURES ADDED BY
 002479 C A.B. LANGDON, EECS, BERKELEY, FEB. 1968.
 002480 C
 002481 C CABS2(Z)=CABS(Z)**2=REAL(Z)**2+AIMAG(Z)**2
 002482 C (AVoids TIME WASTED IN SQRT IN CABS)
 002483 C
 002484 C
 002485 C ANP = NPP
 002486 C IZ = (ANP + 1.)/2.
 002487 C P1 = CMPLX(REAL(PP1),AIMAG(PP1))
 002488 C P2 = CMPLX(REAL(PP2),AIMAG(PP2))
 002489 C P3 = CMPLX(REAL(PP3),AIMAG(PP3))
 002490 C LNCR=0
 002491 C NPHNU = .FALSE.
 002492 C FAILC = 0
 002493 C EP3 = 1.E-13
 002494 C SWR1 = SWR
 002495 C IF (SW7 .AND. SW1) PRINT 512
 002496 C 512 FORMAT (61H NEGATIVE CONJUGATE OF A CONVERGED ROOT IS CONSIDERED A
 002497 C ROOT.)
 002498 C IF(RTC.LT.0) GO TO 100
 002499 C RTC=0
 002500 C DO 99 I=1,NRTS
 002501 C PHI(Z(I)) = .TRUE.
 002502 C 99 CONV(I)=.TRUE.
 002503 C 100 RTC=IABS(RTC)
 002504 C
 002505 C INITIALIZE SEARCH FOR NEXT ROOT.
 002506 C 10 ITC=0
 002507 C IF EIGV = 0, PHI(P) IS NOT CALCULATED.
 002508 C IF EIGV = 2, PHI(P) IS CALCULATED FOR ALL ROOTS
 002509 C IF EIGV = 3, PHI(P) IS CALCULATED FOR ALL ROOTS, AND PHI(X) IS
 002510 C PLOTTED FOR UNSTABLE ROOTS.
 002511 C IF EIGV = 4, PHI(X) PLOTTED FOR ALL ROOTS.
 002512 C NOCONJ=.FALSE.
 002513 C NONEG = .FALSE.
 002514 C SWR = SWR1
 002515 C IF SW5, START SEARCH NEAR RT(RTC+1)
 002516 C IF(.NOT. SW5) GO TO 9
 002517 C P1=PP1+START
 002518 C P2=PP2+START
 002519 C P3=PP3+START
 002520 C 9 CONTINUE
 002521 C SET FX1=FROOT(P1) ETC.
 002522 C I=RTC+1
 002523 C IF(SW2) PRINT 498, I
 002524 C 498 FORMAT(5H ROOT,13,23H SEARCH STARTING POINTS)
 002525 C ROOT=P1
 002526 C NRET=1
 002527 C GO TO 200
 002528 C 1 FX1=FROOT
 002529 C X1=P1
 002530 C IF(SW2) PRINT 499, NRET, ROOT, FROOT
 002531 C 499 FORMAT(3H Z,11,1H=,2E22.13,19H MODIFIED FUNCTION=,2E22.13)
 002532 C ROOT=P2
 002533 C NRET=2
 002534 C GO TO 200
 002535 C 2 FX2=FROOT
 002536 C X2=P2
 002537 C IF(SW2) PRINT 499, NRET, ROOT, FROOT
 002538 C ROOT=P3
 002539 C NRET=3
 002540 C GO TO 200
 002541 C 3 FX3=FROOT
 002542 C X3=P3
 002543 C THE FUNCTION WILL BE CONSIDERED SMALL (FOR PURPOSES OF CONVERGENCE TEST)
 002544 C WHEN IT IS SMALL COMPARED TO F12, EVEN IF THIS IS NOT OF ORDER UNITY
 002545 C F12 = AMIN1(CABS2(FX3),CABS2(FX2))
 002546 C F12 = AMIN1(F12,CABS2(FX1))
 002547 C IF(SW2) PRINT 499, NRET, ROOT, FROOT
 002548 C PREPARE FIRST MULLER-TRAUB ITERATION.
 002549 C H=X3-X2
 002550 C FX21=(FX2-FX1)/(X2-X1)
 002551 C IF P3= A ROOT WE GET FX3/FX2=0/0 LATER, SO CHECK THAT NOW.
 002552 C GO TO 200

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002553 C DO MULLER-TRAUB ITERATION. SEE P212 OF TRAUB'S BOOK.
002554 11 CONTINUE
002555 NREDH = .FALSE.
002556 FX32=(FX3-FX2)/H
002557 FX321=(FX32-FX21)/(X3-X1)
002558 W=FX32+H*FX321
002559 C IF W IS SO BIG THAT T WILL OVERFLOW, GIVE UP ON THIS ROOT.
002560 IF(ABS(REAL(W)).GT.1.E+150.OR.ABS(AIMAG(W)).GT.1.E+150) GO TO 33
002561 T=CSQRT(W*W-(4.,0.)*FX3*FX321)
002562 RHO=W+T
002563 T = W-T
002564 IF( CABS2(T).GT.CABS2(RHO) ) RHO=T
002565 H=-2.*FX3/RHO
002566 C EVEN IF SWR IS ORIGINALLY TRUE, IF WE SMELL AN OBVIOUS COMPLEX
002567 ROOT, WE TEMPORARILY MAKE SWR FALSE AND FIND IT.
002568 IF(.NOT.SWR) GO TO 12
002569 RH = ABS(REAL(H))
002570 AIH = ABS(AIMAG(H))/RH
002571 IF(RH.LE.1.E-02.AND.AIH.GE.1.E+02) SWR = .FALSE.
002572 IF(.NOT.SWR) NREDH = .TRUE.
002573 IF( SWR ) H=REAL(H)
115 12 ITC=ITC+1
002574 X1=X2
002575 X2=X3
002576 FX1=FX2
002577 FX2=FX3
002578 FX21=FX32
002579 C IF NEW H IS TOO MUCH LARGER THAN LAST H REDUCE ITS MAGNITUDE TO THE
002580 C MAXIMUM ALLOWED KEEPING ITS DIRECTION THE SAME.
002581 IF(.NOT.NREDH) GO TO 35
002582 IF(CABS2(H+X3).LT.RMX*RMX) GO TO 13
002583 XR = CABS2(H)/CABS2(X2-X1)
002584 GO TO 36
002585 35 XR = CABS2(H)/CABS2(X2-X1)
002586 IF(XR.LT.XRMAX*XRMX) GO TO 13
002587 36 IF( SW2 ) PRINT 496, H
002588 496 FORMAT(30H (X3-X2)/(X2-X1) TOO LARGE. H=,2E22.13,17H WILL BE REDUC
002589 .ED.)
002590 H=H*(XRMAX/SQRT(XR))
002591 13 X3=X2+H
002592 IF(CABS2(X3 - P3).LT.ERRMAX*ERRMAX) GO TO 40
002593 IF(SW2) PRINT 41
002594 41 FORMAT(19H X3 TOO FAR FROM P3)
002595 I = RTC + 1
002596 GO TO 33
002597 C CHECK FOR CONVERGENCE,
002598 40 DUE TO CLOSE RELATIVE SPACING OF ITERATES.
002600 IF(REAL(X2).EQ.0.0.AND.AIMAG(X2).EQ.0.) GO TO 45
002601 IF(CABS2(X3/X2 - 1.).LT.EP2*EP2) GO TO 22
002602 45 IF(CABS2(X3 - X2).LT.EP2*EP2) GO TO 22
002603 IF(REAL(X1).EQ.0.0.AND.AIMAG(X1).EQ.0.) GO TO 46
002604 IF(CABS2(X3/X1 - 1.).LT.EP2*EP2) GO TO 22
002605 46 IF(CABS2(X3 - X1).LT.EP2*EP2) GO TO 22
002606 ROOT=X3
002607 NRET=4
002608 GO TO 200
002609 4 FX3=FR00T
002610 C IF NEW ITERATE GIVES MUCH LARGER FUNCTION MODULUS,
002611 HALVE THE STEP AND TRY AGAIN.
002612 IF(ABS(REAL(FX3)).GT.1.E+150.OR.ABS(AIMAG(FX3)).GT.1.E+150)GO TO
002613 44
002614 IF( CABS (FX3)/CABS (FX2).LT.FRMAX ) GO TO 103
002615 44 IF( SW2 ) PRINT 497, X3,FUNC,FR00T
002616 497 FORMAT(36H FZ3/FZ2 TOO LARGE. Z3 ADJUSTED FROM,2E22.13/
002617 .11H FUNCTION=,2E22.13,20H, MODIFIED FUNCTION=,2E22.13)
002618 H=.5*XH
002619 GO TO 13
002620 C ITERATION COMPLETE.
002621 103 CONTINUE
002622 C ITERATION OUTPUT
002623 I=RTC+1
002624 IF( SW2 ) PRINT 500, I,ITC,X3,FUNC,FR00T
002625 500 FORMAT(6H ROOT ,13.12H,ITERATION I3,16H, ROOT ESTIMATE=,2E22.13/
002626 .11H FUNCTION=,2E22.13,20H, MODIFIED FUNCTION=,2E22.13)
002627 C CHECK FOR CONVERGENCE
002628 20 DUE TO FUNCTION BEING VERY SMALL.
002629 20 IF( CABS2(FX3)+CABS2(FUNC).LE.EP2*EP2 ) GO TO 22
002630 C NOT CONVERGED YET. SHOULD WE ITERATE AGAIN.
002631 IF(CABS2(X3).GT.RMX*RMX.AND.CABS2(H).LT..25.AND.ITC.GE.5)GO TO 33
002632 C IF ROOT-SEARCH SEEMS TO BE GOING OFF TO INFINITY, STOP IT.
002633 IF(CABS2(X3).GT.RMX*RMX.AND.ITC.GE.5.AND.CABS2(X2-X1).GT..25.AND.
002634 .CABS2(H).GT.CABS2(X2-X1)) GO TO 33
002635 C IF( ITC.LT.MXM ) GO TO 11
002636 C IF WE SEEM TO BE GETTING CLOSE TO A ROOT, ALLOW 10 MORE ITERATIONS
002637 BEFORE GIVING UP.
002638 IF(ITC.LT.MXM+10 .AND. CABS2(FUNC).LT.1.E-06*FI2) GO TO 11
002639 IF(ITC.LT.MXM+20 .AND. CABS2(FUNC).LT.1.E-12*FI2) GO TO 11
002640 C IF FUNCTION IS PRETTY SMALL, BUT MORE THAN EP2, SEE IF EIGENMODE
002641 IS GOOD, AND IF IT IS, CONSIDER ROOT CONVERGED.

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002642      IF(EIGV.EQ.0) GO TO 33
002643      IF (CABS2(FUNC).GT.1.E-14) GO TO 33
002644      CALL SAVPHI
002645      IF(CABS2(PHI(NRTSV,1) - (1.,0.)).LT..0001) GO TO 22
002646      C NO, WE HAVE TRIED LONG ENOUGH;
002647      33 IF( SW1 ) PRINT 502, I, ITC
002648      502 FORMAT(28H FAILURE TO CONVERGE ON ROOT,I3,I10,11H ITERATIONS )
002649      CONV(I)=.FALSE.
002650      FAILC = FAILC + 1
002651      C UNLESS SW4 FAILURE TO CONVERGE MEANS WE MUST STOP AFTER SETTING
002652      C THE REST OF THE ARRAY CONV = .FALSE..
002653      IF( SW4 ) GO TO 22
002654      RTC=RTC+1
002655      43 RT(RTC)=X3
002656      D0 21 I=RTC,NRTS
002657      21 CONV(I)=.FALSE.
002658      RETURN
002659      C RECORD THE FINDING OF A ROOT.
002660      22 CONTINUE
002661      IF(.NOT.SW7 .OR. .NOT.SW3 .OR..NOT. CONV(I)) GO TO 30
002662      L = 0
002663      IF (REAL(X3).LT.0. .OR. AIMAG(X3).LT.0.) L = 1
002664      RX3 = ABS(REAL(X3))
002665      AX3 = ABS(AIMAG(X3))
002666      X3 = CMPLX(RX3, AX3)
002667      IF (L.EQ. 1) FUNC = F(X3)
002668      30 RTC=RTC+1
002669      RT(RTC)=X3
002670      IF (SW1 .AND. .NOT. NONEG .AND. .NOT. NOCONJ) PRINT 501,RTC,X3,ITC
002671      501 FORMAT(6H ROOT ,I3,4H IS=,2E22.13,1H,,15,11H ITERATIONS)
002672      IF (.NOT. CONV(RTC)) GO TO 5304
002673      IF(NONEG.OR.NOCONJ) GO TO 5305
002674      IF(EIGV.EQ.0) GO TO 5304
002675      24 CALL SAVPHI
002676      NRTSU = NRTSV
002677      C IF PHI(1) DOES NOT EQUAL 1 THEN SOMETHING IS WRONG WITH OUR
002678      C CRITERION FOR HAVING FOUND A ROOT
002679      PHJ = PHI(NRTSU, 1)
002680      IF(ABS(AIMAG(PHJ)).LE.,01.AND.ABS(REAL(PHJ)-1.).LE.,01) GO TO 38
002681      IF(SW1) PRINT 513, PHJ
002682      513 FORMAT (37H ROOT NOT GOOD, UNNORMALIZED PHI(1) = , 2E12.4)
002683      CONV(I) = .FALSE.
002684      FAILC = FAILC + 1
002685      GO TO 5304
002686      38 IF(EIGV.GT.3) GO TO 39
002687      IF(AIMAG(RT(RTC)).LT.1.E-05.OR.EIGV.LT.3) GO TO 34
002688      C PHI(X) FOR THIS ROOT WILL BE PLOTTED AT END OF RUN.
002689      39 PHI(NRTSV, NPP+1)= RT(RTC)
002690      PHI(NRTSV, NPP+2) = CMPLX(KYAI,0.)
002691      NRTSV = NRTSV + 1
002692      34 PHJ = PHI(NRTSU,IZ)
002693      C CALCULATE AND PRINT OUT ABS.VAL. AND ARG. OF PHI(P) S.
002694      SUM = 0.
002695      D0 26 I = 1, NPP
002696      SUM = SUM + CABS2(PHI(NRTSU,I))
002697      ABPHI(I) = CABS(PHI(NRTSU,I))
002698      IF (ABPHI(I).LE.1.E-20) GO TO 32
002699      ARPHI (I) = 57.296*AIMAG(CL0G(PHI(NRTSU, I)))
002700      GO TO 26
002701      32 ARPHI(I) = 0.
002702      26 CONTINUE
002703      C PHIZ = .TRUE. IFF PHI(0) = 0. THE PURPOSE OF PHIZ IS EXPLAINED IN *ROOTS*
002704      C FOLLOWING STATEMENT 76
002705      IF(CABS2(PHJ)/SUM.GT.1.E-11) PHIZ(RTC) = .FALSE.
002706      PHPLUS = CABS2(PHI(NRTSV,IZ+1))
002707      PHMIN = CABS2(PHI(NRTSV,IZ-1))
002708      IF(CABS2(PHJ).GT.1.E-04*PHPLUS) PHIZ(RTC) = .FALSE.
002709      IF(CABS2(PHJ).GT.1.E-04*PHMIN) PHIZ(RTC) = .FALSE.
002710      ABNM = SQRT(SUM)
002711      I = IZ
002712      ARNM = ARPHI(I)
002713      IF (ABPHI(I) .LE. .1E-03) ARNM = .5*ARPHI(NPP)
002714      D0 31 I = 1 NPP
002715      ABPHI(I) = ABPHI(I)/ABNM
002716      ARPHI(I) = ARPHI(I) - ARNM
002717      IF (ARPHI(I) .LE. -180.) ARPHI(I) = ARPHI(I) + 360.
002718      IF (ARPHI(I) .GT. 180.) ARPHI(I) = ARPHI(I) - 360.
002719      IF(NRTS.GT.2) GO TO 31
002720      C DON'T CALCULATE PHINEW UNLESS THIS IS THE FIRST GOOD ROOT WE HAVE FOUND.
002721      IF(NOPHNU) GO TO 31
002722      IF(PHZP.NE.SGNL(1,PHIZ(RTC))) GO TO 31
002723      IF(AIMAG(RT(RTC)).LT.-1.E-06.AND.SW31) GO TO 31
002724      IF( REAL(RT(RTC)).LT.-1.E-06.AND.SW71) GO TO 31
002725      C PHINEW IS USED BY *FOLLOW* IN COMPARING EIGENFUNCTIONS OF OLD AND NEW KYAI.
002726      42 PHINEW(I) = ABPHI(I)*CEXP(ARPHI(I)*(0.,1.)/57.296)
002727      IF(I.EQ.NPP) NOPHNU = .TRUE.
002728      31 CONTINUE
002729      IF(.NOT.SW1) GO TO 5304
002730      PRINT 507, (ABPHI(I), I = 1, NPP)
002731      507 FORMAT (10E12.4/10E12.4)
002732      PRINT 506, (ARPHI(I), I = 1, NPP)
002733      506 FORMAT (10F12.2/10F12.2)
002734      5304 IF(.NOT.SW3) GO TO 47

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002735      START = ABS(REAL(X3))
002736      IF(START.GE.RMX) START = 1.5
002737      47 IF(ITC.GT.0) GO TO 5305
002738      C  IF ONE OF THE STARTING POINTS WAS A ROOT (I.E. ITC = 0), THEN CHANGE
002739      C  THE STARTING POINTS, OTHERWISE WE WILL GET THE SAME ROOT AGAIN NEXT
002740      C  CHANGE = .15*(P2 - P1)
002741      C  P1 = P1 + CHANGE
002742      C  P2 = P2 + CHANGE
002743      C  P3 = P3 + CHANGE
002744      5305 CONTINUE
002745      C  QUIT IF ENOUGH ROOTS ARE FOUND, OR IF WE ARE ALMOST OUT OF TIME.
002746      C  IF(WARN(0)) RETURN
002747      C  IF( RTC.GE.NRTS ) GO TO 300
002748      C  IF(FAILC.GT.NFL) RETURN
002749      C  IF SW7, THE NEGATIVE CONJUGATE OF A CONVERGENT ROOT FOUND IS TO BE
002750      C  REGARDED AS A ROOT.
002751      C  28 IF(.NOT. SW7 .OR. NONNEG .OR. ABS(REAL(X3)).LT.EP1) GO TO 29
002752      C  IF(SW1) PRINT 514
002753      514 FORMAT(62H NEGATIVE CONJUGATE OF LAST ROOT WILL BE CONSIDERED NEXT
002754      , ROOT.)
002755      ITC = 0
002756      NONNEG = .TRUE.
002757      X3 = -1.*CONJG(X3)
002758      ROOT = X3
002759      IF(.NOT.CONV(RTC)) CONV(RTC+1) = .FALSE.
002760      PHIZ(RTC+1) = PHIZ(RTC)
002761      GO TO 30
002762      29 NONNEG = .FALSE.
002763      C  IF SW3, THE CONJUGATE OF A CONVERGENT NON-REAL ROOT IS TO BE
002764      C  REGARDED AS A ROOT ALSO, IF NOT ALREADY USED.
002765      C  23 IF(.NOT. SW3 .OR. ABS(AIMAG(X3)).LT.EP1 .OR. NOCONJ ) GO TO 10
002766      C  IF( SW1 ) PRINT 503
002767      503 FORMAT(53H CONJUGATE OF LAST ROOT WILL BE CONSIDERED NEXT ROOT.)
002768      ITC=0
002769      NOCONJ=.TRUE.
002770      X3=CONJG(X3)
002771      ROOT=X3
002772      IF(.NOT.CONV(RTC)) CONV(RTC+1) = .FALSE.
002773      PHIZ(RTC+1) = PHIZ(RTC)
002774      NRET=5
002775      C  GO TO 200
002776      5 GO TO 30
002777      C  EVALUATES FROOT
002778      C  WHERE (ROOT-RT(1))*...*(ROOT-RT(RTC))*FROOT=F(ROOT)
002779      C  RETURNS TO STATEMENT NUMBER NRET.
002780      C  SPECIAL TREATMENT WHEN ROOT IS CLOSE TO AN EARLIER FOUND ROOT IS
002781      C  DESCRIBED AT HEAD OF PROGRAM.
002782      200 CONTINUE
002783      IF(WARN(0)) RETURN
002784      FUNC=F(ROOT)
002785      IF( SWR ) FUNC=REAL(FUNC)
002786      DNR=(1.,0.)
002787      IF(RTC.EQ.0) GO TO 202
002788      TEST=EP3*EP3*CABS2(ROOT)
002789      DO 203 I=1,RTC
002790      IF( CABS2(ROOT-RT(I)).GE.TEST ) GO TO 201
002791      T=.333333333*(P1+P2+P3)+EP1
002792      IF( NRET.NE.1 ) GO TO 210
002793      P1=2.*P1-T
002794      ROOT=P1
002795      GO TO 200
002796      210 IF( NRET.NE.2 ) GO TO 211
002797      P2=2.*P2-T
002798      ROOT=P2
002799      GO TO 200
002800      211 IF( NRET.NE.3 ) GO TO 212
002801      P3=2.*P3-T
002802      ROOT=P3
002803      GO TO 200
002804      201 DNR=DNR*(ROOT-RT(I))
002805      203 CONTINUE
002806      202 FROOT=FUNC/DNR
002807      204 GO TO (1,2,3,4,5), NRET
002808      212 IF( SW1 ) PRINT 504
002809      504 FORMAT(71H ITERANT CLOSE TO ROOT FOUND BEFORE. ACCEPT IT AS A ROOT
002810      , WITHOUT TEST.)
002811      FROOT=0,
002812      GO TO 22
002813
002814      C  TERMINATION PROCEDURE.
002815      C  INCLUDES CAPABILITY OF REDOING 'BAD ROOTS' -ONES WHICH HADN'T
002816      C  CONVERGED.
002817
002818      C  HOW MANY GOOD ROOTS ARE THERE..
002819      300 NCR=0
002820      DO 301 I=1,NRTS
002821      IF( CONV(I) ) NCR=NCR+1
002822      301 CONTINUE
002823      C  IF ALL ROOTS ARE GOOD, OR IF WE HAVEN'T BEEN ASKED TO REDO BAD ONES,
002824      C  OR IF WE HAVE HAD NO LUCK THE LAST TIME THROUGH THE ROOTFINDING CODE,
002825      C  WE QUIT.
002826      IF( NCR.EQ.NRTS .OR. .NOT.SW4 .OR. NCR.LE.LNCR ) RETURN
002827

```

```

002828 C FIND FIRST BAD ROOT.
002829 DO 302 I=1,NRTS
002830 IF( .NOT.CONV(I) ) GO TO 303
002831 302 CONTINUE
002832 C IF IT IS THE LAST ROOT WE WOULD ONLY BE REPEATING THE SAME NON-
002833 C CONVERGENT ITERATIONS IF WE TRIED AGAIN.
002834 303 IF( I.EQ.NRTS ) RETURN
002835 C MOVE LAST ROOT INTO 1ST BAD ROOTS PLACE.
002836 C GO BACK AND TRY TO FIND A NEW LAST ROOT. GOOD LUCK.
002837 IF( SW1 ) PRINT 505, I
002838 505 FORMAT(48H WILL ATTEMPT TO RE-DO UNCONVERGED ROOT ESTIMATE,I3)
002839 X3=RT(NRTS)
002840 RT(NRTS)=RT(I)
002841 RT(I)=X3
002842 CONV(I)=CONV(NRTS)
002843 RTC=NRTS-1
002844 LNCR=NCR
002845 CONV(NRTS)=.TRUE.
002846 GO TO 28
002847
002848 C
002849 END

```

```

002849
002850 C SUBROUTINE EIGPLT
002851 PLOTS EIGENFUNCTIONS
002852 COMPLEX GMEGA, PHI(18,22), A(20,20), F(100),IPXKO
002853 INTEGER PMAX
002854 REAL KYAI
002855 LOGICAL GOOD(18)
002856 DIMENSION X(100), Y(100)
002857 DATA KYAI/0./
002858 DATA NDY /10/
002859 COMMON/CIO/ICR, IHSP, IGRAPH
002860 COMMON/PHIC/ A, NRTSV, PHI
002861 COMMON/PMX/NP
002862 COMMON/FOLEIG/ GOOD, IBRANCH(18)
002863 COMMON/TVPOL/XMIN,XMAX,YMIN,YM, TVXMIN,TVXMAX,TVYMIN,TVYMAX
002864 COMMON/TVTUNE/LPENON,LPEOFF,ITALICS,IWINK,INTENSE,IRIGHT,IUP
002865 NDY1 = NDY - 1
002866 CALL PAGE
002867 PRINT 10, NRTSV
002868 10 FORMAT(8H NRTSV =,I4)
002869 PRINT 11, GOOD
002870 11 FORMAT(20I5)
002871 IF(NRTSV.EQ.1) RETURN
002872 NRTSU = NRTSV - 1
002873 PMAX = (NP-1)/2
002874 PI = 3.141592653589
002875 DO 3 N = 1, NRTSU
002876 IF(.NOT.GOOD(N)) GO TO 3
002877 GMEGA = PHI(N, NP+1)
002878 KYAI = REAL(PHI(N, NP+2))
002879 SUM = 0.
002880 DO 6 J = 1, NP
002881 6 SUM = SUM + CABS2(PHI(N, J))
002882 SUM = SQRT(SUM)
002883 DO 7 J = 1, NP
002884 7 PHI(N, J) = PHI(N, J)/SUM
002885 DO 1 I = 1, 100
002886 AI = I
002887 X(I) = AI/100.
002888 XK0 = 2.*PI*X(I)
002889 F(I) = (0., 0.)
002890 DO 2 J = 1, NP
002891 P = J - PMAX - 1
002892 IPXKO = CMPLX(0., XK0*P)
002893 2 F(I) = F(I) + PHI(N, J)*CEXP(IPXKO)
002894 1 Y(I) = F(I)*CONJG(F(I))
002895 YM = Y(1)
002896 DO 5 I = 2, 100
002897 5 YM = AMAX1(YM, Y(I))
002898 XMAX = 1.
002899 YMIN = 0.
002900 XMIN = 0.
002901 CALL MAPS(XMIN, XMAX, YMIN, YM, 0.11328, 1.0, 0.15, 1.0)
002902 CALL TRACE(X, Y, 100)
002903 CALL SETCH(1, 2, 1, 0, 1, 0, 0)
002904 WRITE(IGRAPH, 4) GMEGA
002905 4 FORMAT(34H PLOT OF PHI**2 VS. X FOR GMEGA = ,2E22.13)
002906 WRITE(IGRAPH, 8) KYAI, IBRANCH(N)
002907 8 FORMAT(8H KYAI = ,E12.6,10X,7H BRANCH,I4)
002908 CALL FRAME(1)
002909 C DO PLCT OF PHI(X, Y)
002910 FM = SQRT(YM)
002911 YM = NDY
002912 CALL MAPS(XMIN, XMAX, YMIN, YM, 0.11328, 1.0, 0.15, 1.0)
002913 DO 12 K = 1, NDY1
002914 FLK = K

```

```

002915      PHASE = 2.*3.1415926535*FLK/YM
002916      DO 13 I = 1,100
002917      13 Y(I) = FLK + REAL(F(I)*CEXP((0.,1.)*PHASE))/FM
002918      12 CALL TRACE(X,Y,100)
002919      CALL SETCH(1,1,,1,0,1,0,0)
002920      WRITE(IGRAPH,14)
002921      14 FORMAT(51H PLOT OF PHI(X,Y) FOR ONE WAVELENGTH IN Y DIRECTION)
002922      CALL FRAME(1)
002923      PRINT 9, OMEGA, KYAI, IBRANCH(N)
002924      9 FORMAT(35H EIGENFUNCTION PLOTTED FOR OMEGA = ,2E10.2,8H KYAI = ,E1
002925      .0.3,10X,7H BRANCH,14)
002926      3 CONTINUE
002927      RETURN
002928      END

```

```

002929
002930      SUBROUTINE PRNPLT(X,Y,XMAX,XINCR,YMAX,YINCR,ISX,ISY,NPTS)
002931      COMMON/C18/ ICR,IHSP,IGRAPH
002932      DIMENSION X(NPTS),Y(NPTS),IGRID(105),XAXIS(11)
002933      INTEGER BLANK,DOT,STAR,IGRID,PLUS
002934      DATA BLANK,DOT,STAR,PLUS / 1H,1H.,1H*,1H+ /
002935      901 FORMAT(14X,105A1)
002936      902 FORMAT(1XE10.2,2X,1H+,105A1,1H+)
002937      903 FORMAT(15X,103(1H,))
002938      904 FORMAT(7X,11(F10.0),2H (,I4,5H PTS) )
002939      905 FORMAT(16X,11(1H+,9X))
002940      9800 FORMAT(46H SCALING ERROR IN PRNPLT, EXECUTION TERMINATED )
002941      IF(XINCR.EQ.0..OR.YINCR.EQ.0.) GO TO 800
002942      YAXMIN=0.01*YINCR
002943      XAXMIN=0.01*XINCR
002944      IZERO=YMAX/YINCR+1.5
002945      JZERO=103.5-XMAX/XINCR
002946      IF(JZERO.GT.103.0R.JZERO.LT.4) JZERO=2
002947      PRINT 905
002948      PRINT 903
002949      DO 10 I=1,51
002950      IF ( I.NE.IZERO) GO TO 16
002951      DO 14 J=1,105
002952      14 IGRID(J)=PLUS
002953      GO TO 15
002954      16 DO 11 J=1,105
002955      11 IGRID(J)=BLANK
002956      15 IGRID(JZERO)=PLUS
002957      IGRID(104)=DOT
002958      IGRID(2)=DOT
002959      DO 12 K=1,NPTS
002960      12 ITEST =(YMAX-Y(K))/YINCR+1.5
002961      IF(ITEST .NE. 1) GO TO 12
002962      J=103.5-(XMAX-X(K))/XINCR
002963      IF(J.GT.103) J=105
002964      IF(J.LT.3) J=1
002965      IGRID(J)=STAR
002966      12 CONTINUE
002967      IF(MOD(I,10).EQ.1) GO TO 13
002968      PRINT 901,IGRID
002969      GO TO 10
002970      13 YAXIS=YMAX-(I-1)*YINCR
002971      IF(ABS(YAXIS).LT.YAXMIN) YAXIS=0.
002972      PRINT 902,YAXIS,(IGRID(J),J=1,105)
002973      10 CONTINUE
002974      PRINT 903
002975      PRINT 905
002976      DO 20 M=1,11
002977      XAXIS(M)=XMAX-XINCR*(FL0AT(11-M))*10.0
002978      IF(ABS(XAXIS(M)).LT.XAXMIN)XAXIS(M)=0.
002979      20 CONTINUE
002980      PRINT 904,XAXIS,NPTS
002981      RETURN
002982      800 PRINT 9800
002983      CALL EXIT
002984      END

```

```

002985
002986      SUBROUTINE TRACET(TEXTURE,X,Y,NPT)
002987      REAL TEXTURE,X(1),Y(1)
002988      INTEGER NPT
002989      IF(TEXTURE.EQ.0.0) CALL TRACE(X,Y,NPT)
002990      IF(TEXTURE.NE.0.0) CALL TRACEP(X,Y,NPT,3)
002991      RETURN
002992      END

```

002993 FUNCTION SGNL(A,L)
002994 LOGICAL L
002995 IF(L) B = -1.
002996 IF(.NOT.L) B = 1.
002997 SGNL = SIGN(A,B)
002998 RETURN.
002999 END

003001 LOGICAL WARN
003002 FUNCTION WARN(N)
003003 WARN = .FALSE.
003004 RETURN
003005 END
003006

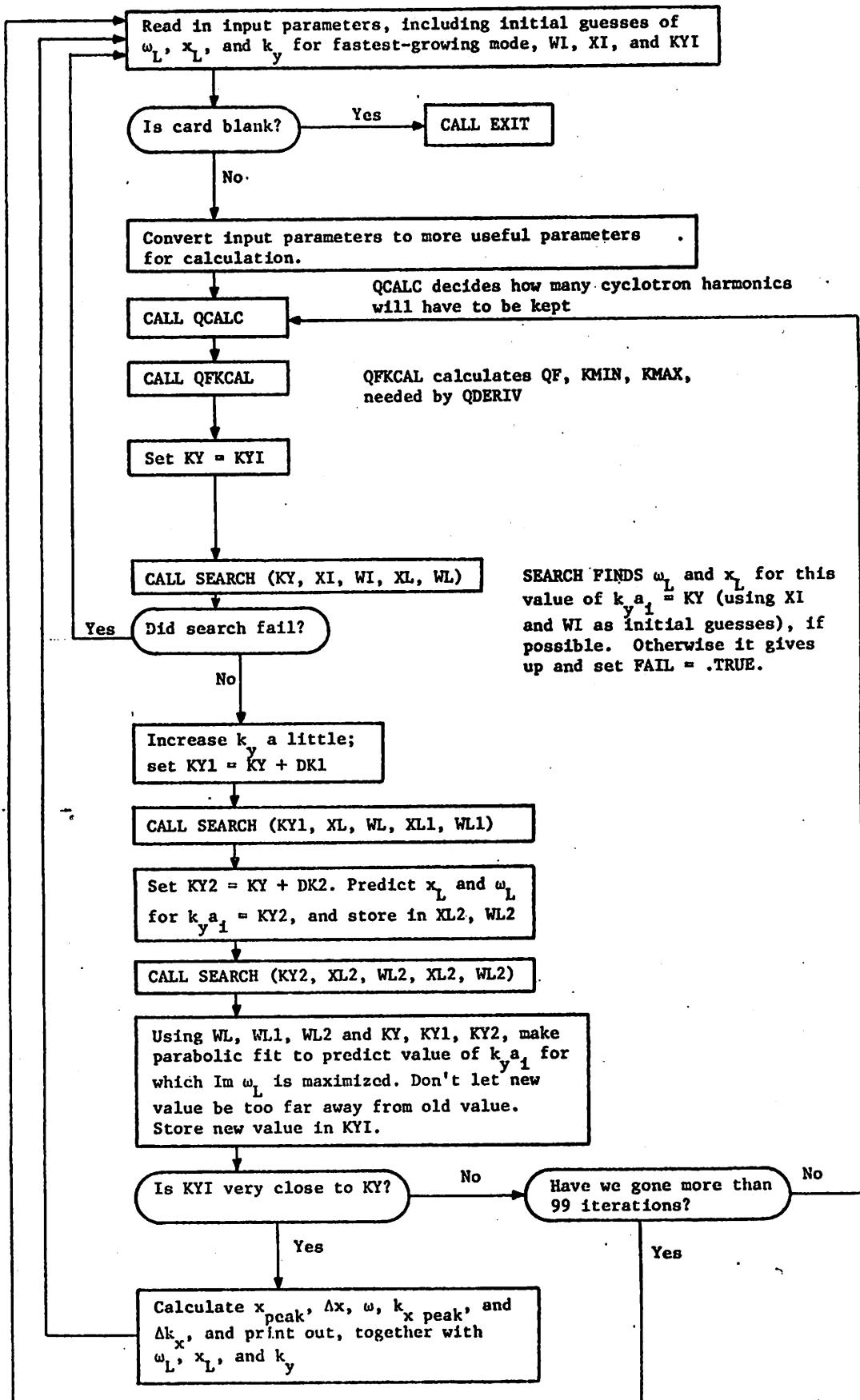
An outline of the program LOCAL and its subroutines is shown in the flow chart. LOCAL was used to find the normal modes and frequencies using the local method. In contrast to ROOTS, which was used for the nonlocal method, all branches $\omega(k_y)$ were not calculated, and "smart" root-finders and branch-followers were not used in LOCAL. Instead, a Newton-Raphson iteration scheme was used to find the solutions $x = x_L$ and $\omega = \omega_L$ to the simultaneous equations $D(x, \omega, k_x = 0) = 0$ and $\partial D / \partial x = 0$. Only the mode with the highest growth rate was sought. The Newton-Raphson iteration method worked well only if initial guesses of x_L and ω_L were reasonably close to the correct solutions. The mode found as the fastest-growing mode was really only the local maximum of $\text{Im } \omega(k_y)$ closest to the initial value of k_y chosen. The limitations in LOCAL were tolerable because ROOTS could be used to make good estimates of x_L , ω_L and k_y for initial guesses in LOCAL.

The routine QDERIV shown in the flow chart was similar to the subroutine DISP used with ROOTS, but instead of calculating $\det A_{p,p}$, it calculated

$$D(x, \omega) = G_0(\omega) + G_{-1}(\omega) \exp(-ik_0 x) + G_{+1}(\omega) \exp(ik_0 x)$$

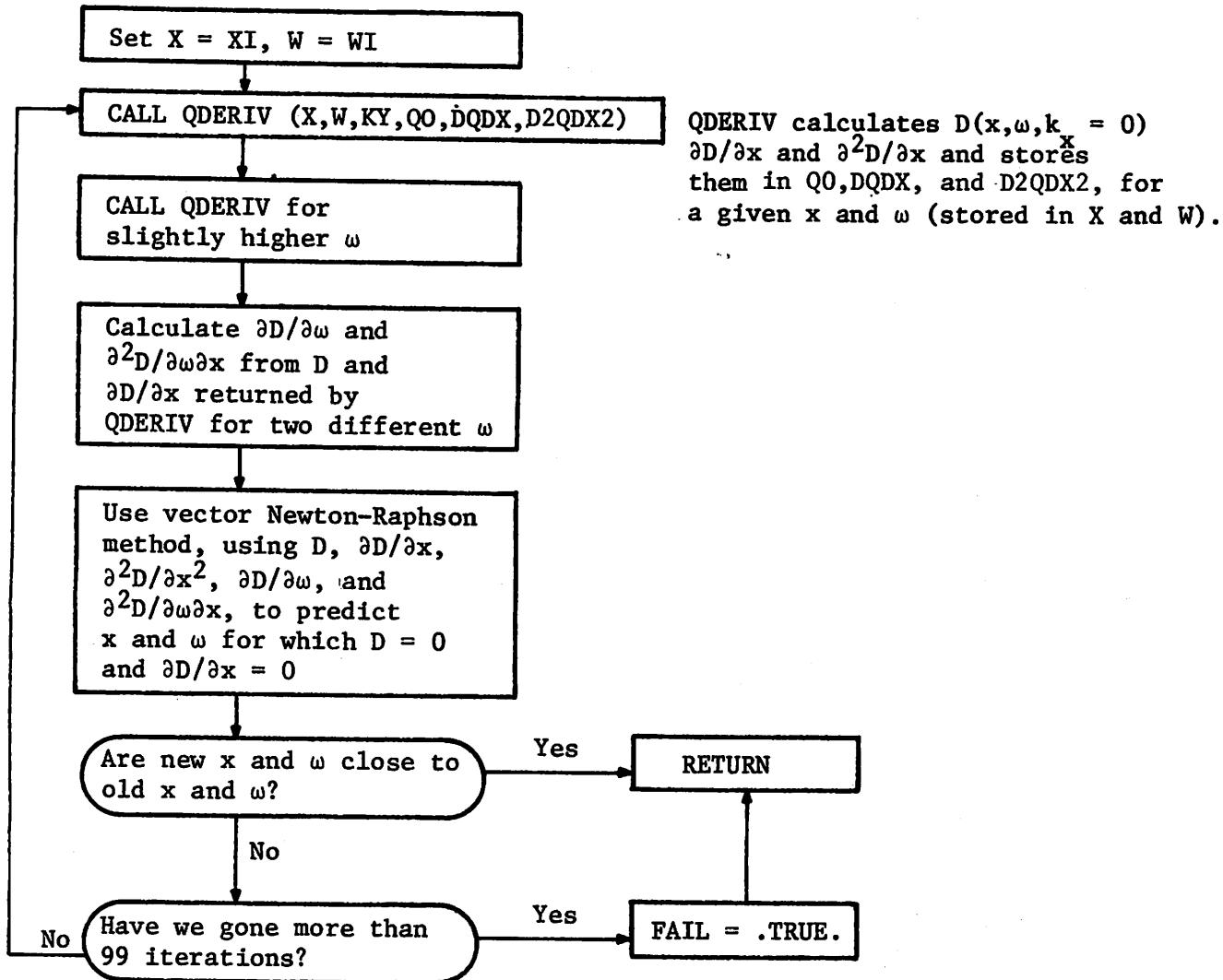
(with $k_x = 0$ assumed). Since the G's do not depend on x, the derivatives $\partial D / \partial x$ and $\partial^2 D / \partial x^2$, needed for the Newton-Raphson method, could be easily found analytically, and were also returned by QDERIV. On the other hand, the derivatives $\partial D / \partial \omega$ and $\partial^2 D / \partial x \partial \omega$ were found by calling QDERIV twice using slightly different values of ω .

FLOW CHART OF LOCAL



FLOW CHART OF SEARCH (KY, XI, WI, XL, WL)

KY is $k_y a_i$. XI and WI are the initial guesses for x_L AND ω_L (normalized to ω_{ci} and $2\pi/k_0$). XL and WL are final values of x_L and ω_L returned by SEARCH



Listing of LOCAL and Subroutines

Like ROOTS, LOCAL runs on the A-machine of the National Magnetic Fusion Energy Computer Center. However, it is not believed to contain any non-standard Fortran, except for the PROGRAM, READ, FORMAT, and FUNCTION statements.

The subroutines QFKCAL, QCALC, BESSI, BESSJ, CABS2, ZEE, ABCALC, MAXW, RING, and COLD, used by LOCAL, have been already listed with ROOTS, so they are not shown here.

C-170A BOX B05 18.55.58 09/16A 1976
 PROGRAM LOCAL (INPUT HSP, OUTPUT, TAPE10=OUTPUT)
 REAL KY, KOAI, KOSQ, KY1, KYNEW, KY1, KY2
 COMPLEX XI, WI, XL1, WL1, XL2, WL2, WIDTH, XLEW, WLNEW
 COMPLEX SLPX1, SLPX2, SLPW1, SLPW2, D2XDK2, D2WDK2
 COMPLEX DQDX, D2QDX2, DQDW, XL, WL, QO, DELW, DQDKXS
 INTEGER QMAX
 LOGICAL FAIL
 LOGICAL UNMAG
 COMMON/CMAG/UNMAG
 COMMON/DIS/QF,KYSQ, KOSQ, EPSF(4), XXX, KYAI, KOAI, XXXX, PMAX,
 CMPSQ, AEAI, KMAX(4), AMASQ(4), XXXXX(4), KMIN(4)
 COMMON/CDFU/ DFU(4), YY(4)
 COMMON/CSPEC/ RLARM(4), AMASS(4), CHARG(4), JAY(4), DENSE(4), NSPEC
 COMMON/CFAIL/ FAIL
 COMMON/CQDER/ QO, DQDX, D2QDX2, DQDW, DQDKXS
 COMMON/CRBESJ/ QMAX(4), NMAX(4)
 DATA AEAI/0./, DFU/4*0./, JAY/4*0/
 DATA RLARM/4*1./, AMASS/4*1./, CHARG/4*1./, DENSE/4*1./, AMASQ
 /4*1./
 DATA ICR/2/
 PRINT 17
 17 FORMAT(1H1)
 GO TO 18
 15 CONTINUE
 18 READ (ICR, 16) AIL, R, CMPSQ, XI, WI, KYI, UNMAG
 16 FORMAT(8F5.0, 11)
 IF(AIL.EQ.0.) CALL EXIT
 IF(XI.NE.0..OR.WI.NE.0..OR.KYI.NE.0.) GO TO 20
 IF(FAIL) GO TO 18
 WI = WL
 XI = XL
 KYI = KY
 20 IONS = 5H MAG.
 IF(UNMAG) IONS = 6H UNMAG
 GAM = 1.
 IF(R.LE.1.) GAM = 0.
 RLARM(2) = 1./SQRT(R)
 RLARM(3) = 0.
 AMASS(3) = 1./3700.
 CHARG(3) = -1.
 DENSE(1) = R/(R - GAM)
 DENSE(2) = -GAM/(R-GAM)
 NSPEC = 3
 AMASQ(3) = AMASS(3)**2
 19 KOAI = 2.*3.1415926535*AIL
 KOSQ = KOAI**2
 EPSI = .999
 EPSI = .99
 EPSE = EPSI*(DENSE(1)*EXP(-.5*KOSQ) + DENSE(2)*EXP(-.5*KOSQ*RLARM(2)**2))
 DO 1 I = 1, 2
 1 EPSF(1) = .5*EPSI*CMPSQ*DENSE(1)
 EPSF(3) = .5*EPSE*CMPSQ/AMASS(3)
 ITER = 0
 5 KY = KY1
 RHIGH = 2.*REAL(WI)
 MINQ = RHIGH
 CHI = KY*KY
 DO 9 I = 1, NSPEC
 IF(RLARM(I).EQ.0.) GO TO 9
 CHI2 = CHI*RLARM(I)**2
 IF(JAY(I).EQ.0.) GO TO 10
 CALL QCALC(CHI2, QMAX(I), NMAX(I), 1)
 GO TO 9
 10 CALL QCALC(CHI2, QMAX(I), NMAX(I), 0)
 NMAX(I) = NMAX(I) + JAY(I)
 9 CONTINUE
 CALL QFKCAL(QF, KMAX, KMIN, RHIGH, 0.)
 CALL SEARCH(KY, XI, WI, XL, WL)
 IF(FAIL) GO TO 13
 DK1 = .001*KY
 DK2 = .01*KY
 KY1 = KY + DK1
 KY2 = KY1 + DK2
 WIDTH = CSQRT(2.*DQDKXS*AIL*AIL/D2QDX2)
 DELW = -.5*WIDTH*D2QDX2/DQDW
 WIDTH = CSQRT(WIDTH)
 CALL SEARCH(KY1, XL, WL, XL1, WL1)
 IF(FAIL) GO TO 13
 XL2 = 11.*XL1 - 10.*XL
 WL2 = 11.*WL1 - 10.*WL
 CALL SEARCH (KY2, XL2, WL2, XL2, WL2)
 IF(FAIL) GO TO 13
 SLOPE1 = (AIMAG(WL1) - AIMAG(WL))/DK1
 SLOPE2 = (AIMAG(WL2) - AIMAG(WL1))/DK2
 IF(SLOPE2.GE.SLOPE1) GO TO 3
 D2GDK2 = 2.* (SLOPE2-SLOPE1)/(DK1+DK2)
 KYNEW = KY + .5*DK1 - SLOPE1/D2GDK2
 IF(ABS(KYNEW-KY).GT.1*KY) GO TO 3
 IF(ABS(KYNEW-KY).LT..005*KY) GO TO 4
 7 ITER = ITER + 1

```

000092 IF(ITER.GT.99) GO TO 13
000093 SLPX1 = (XL1-XL)/DK1
000094 SLPX2 = (XL2-XL1)/DK2
000095 D2XDK2 = 2.* (SLPX2 - SLPX1)/(DK1+DK2)
000096 SLPW1 = (WL1 - WL)/DK1
000097 SLPW2 = (WL2 - WL1)/DK2
000098 D2WDK2 = 2.* (SLPW2-SLPW1)/(DK1+DK2)
000099 XLEW = .5*(XL+XL1) + SLPX1*(KYNEW - .5*(KY+KY1)) + .5*D2XDK2*
000100 .*(KYNEW - .5*(KY+KY1))**2
000101 IF(CABS(XLEW-XL).GT..1) GO TO 6
000102 WLNEW = .5*(WL+WL1) + SLPW1*(KYNEW - .5*(KY+KY1)) + .5*D2WDK2*
000103 .*(KYNEW - .5*(KY+KY1))**2
000104 IF(CABS(WLNEW-WL - 1.).GT..2) GO TO 6
000105 KYI = KYNEW
000106 XI = XLEW
000107 WI = WLNEW
000108 GO TO 5
000109 3 IF(SLOPE2.LE.0.) KYNEW = 9*KY
000110 IF(SLOPE2.GT.0.) KYNEW = 1.1*KY
000111 GO TO 7
000112 4 WL1 = WL + .5*DELW
000113 WL2 = WL1 + DELW
000114 XCORR = CABS(WIDTH)
000115 XPEAK = REAL(XL) + AIMAG(XL)*AIMAG(WIDTH**2)/REAL(WIDTH**2)
000116 PEAKK = AIMAG(XL)/REAL(WIDTH**2)/(2.*3.1415926535)
000117 F = SQRT ALOG(2.)*2.
000118 HWX = F/SQRT(REAL(1./WIDTH**2))
000119 HKW = F/SQRT(REAL(WIDTH**2))/(2.*3.1415926535)
000120 PRINT 14, AIL, R, GMPSQ, IONS
000121 14 FORMAT("//AIL =", E14.5, " R =", E14.5, ", GMPSQ =", E14.5, ", MASS
000122 . RATIO = 3700, "A6," IONS")
000123 PRINT 8, WL, KY, XL, XCORR, WIDTH, WL1, WL2
000124 8 FORMAT(" ACCORDING TO LOCAL APPROX. FASTEST-GROWING MODE HAS GMEG
000125 . A =", 2E14.5, ". KYAI =", E14.5/"LOCATED AT X/L =", 2E14.5, " WITH
000126 . CORRELATION LENGTH" E14.5, "(" E14.5 "+" , E14.5, " I")/" GMEG CORRE
000127 . CTED FOR FINITE WIDTH (WKB APPROX.) IS ", 2E14.5/" AND THE NEXT WKB
000128 . MODE HAS GMEG ", 2E14.5)
000129 PRINT 12, XPEAK, HWX, PEAKK, HKW
000130 12 FORMAT(" ABS.VAL.PHI(X) SQUARED HAS PEAK AT X/L =", E14.5, " AND H
000131 . ALF-WIDTH" E14.5/"ABS.VAL.PHI(KX) SQUARED HAS PEAK AT KX/K0 =", E14.5,
000132 . " AND HALF-WIDTH", E14.5)
000133 GO TO 15
000134 6 KYNEW = .5*(KYNEW + KY)
000135 GO TO 7
000136 13 PRINT 14, AIL, R, GMPSQ, IONS
000137 GO TO 15
000138 END

```

```

000139
000140 SUBROUTINE SEARCH (KY, XI, WI, XL, WL)
000141 LOGICAL FAIL, NDPOLE
000142 COMPLEX XI, WI, XL, WL, X, W, Q0, Q1, Q2, DQDX, DQDW, D2QDX2, D2QDXW, DQDX1, DET
000143 COMPLEX DQDKXS
000144 COMPLEX XDIFF, WDIFF
000145 REAL KY, KXSQ
000146 COMMON/CFAIL/ FAIL
000147 COMMON/CQDER/ Q0, DQDX, D2QDX2, DQDW, DQDKXS
000148 COMMON/CNDP/ NDPOLE
000149 COMMON/CKX/ KXSQ
000150 NDPOLE = .FALSE.
000151 KXSQ = 0.
000152 FAIL = .FALSE.
000153 ITER = 0
000154 XI = XI
000155 WI = WI
000156 2 CALL QDERIV(X, W, KY, Q0, DQDX, D2QDX2)
000157 CALL QDERIV(X, W+.001, KY, Q1, DQDX1, Q2)
000158 DQDW = 1000.* (Q1-Q0)
000159 D2QDXW = 1000.* (DQDX1 - DQDX)
000160 DET = DQDX*D2QDXW - D2QDX2*DQDW
000161 XDIFF = (-D2QDXW*Q0 + DQDW*DQDX)/DET
000162 XL = X + XDIFF
000163 WDIFF = (D2QDX2*Q0 - DQDX*DQDX)/DET
000164 WL = W + WDIFF
000165 IF(CABS(XL - X).GT..005) GO TO 1
000166 IF(CABS(WL - W).GT..005) GO TO 1
000167 NDPOLE = .TRUE.
000168 CALL QDERIV(X, W, KY, Q0, DQDX, D2QDX2)
000169 CALL QDERIV(X, W+.001, KY, Q1, DQDX1, DQDX1)
000170 KXSQ = .0001
000171 CALL QDERIV(X, W, KY, Q2, DQDX1, DQDX1)
000172 DQDW = 1000.* (Q1-Q0)
000173 DQDKXS = 10000.* (Q2-Q0)
000174 KXSQ = 0.
000175 NDPOLE = .FALSE.
000176 RETURN
000177 1 ITER = ITER + 1
000178 IF(ITER.GT.99) GO TO 4
000179 IF(CABS(XL - X).GT..1) GO TO 3
000180 IF(CABS(WL/W - 1.).GT..2) GO TO 3
000181 XI = XL
000182 WI = WL
000183 GO TO 2
000184 3 XL = .5*(XL + X)
000185 WL = .5*(WL + W)
000186 GO TO 1
000187 4 FAIL = .TRUE.
000188 PRINT 5, KY, XL, WL, Q0, DQDX
000189 5 FORMAT("SEARCH FAILED", 9E12.4)
000190 RETURN
000191 END

```

```

000192
000193      SUBROUTINE QDERIV(X, W, KY, Q, DQDX, D2QDX2)
000194      COMPLEX X, W, OMEGA, GO, GPLUS, GMINUS, APP, BPP, AP, BP, IX, DEPOLE, OMEGD, U
000195      COMPLEX Q, DQDX, D2QDX2, EIKOX
000196      INTEGER PMAX, P
000197      REAL KY, KYSQ, KYAI, KOAI, KOSQ, KXSQ
000198      LOGICAL UNMAG, NDPOLE
000199      COMMON/CMAG/UNMAG
000200      COMMON/DIS/QF KYSQ,           KOSQ, EPSF(4), XXX, KYAI, KOAI, XXXX, PMAX,
000201      .      OMPSQ, AEAI, KMAX(4), AMASQ(4), XXXX(4), KMIN(4)
000202      COMMON/CDFU/ DFU(4), YYY(4)
000203      COMMON/CSPEC/ RLARM(4), AMASS(4), CHARG(4), JAY(4), DENSE(4), NSPEC
000204      COMMON/CCHIP/ CHIP(4), AP(4), BP(4), OMEGA, APP(4), BPP(4)
000205      COMMON/APBP/N, M, P
000206      COMMON/CNDP/ NDPOLE
000207      COMMON/CKX/KXSQ
000208      DATA PI /3.1415926535/
000209      KYAI = KY
000210      KYSQ = KY*KY
000211      OMEGA = W
000212      DO 103 I = 1, NSPEC
000213      OMEGD = OMEGA + (0., 1.)*KYSQ*DFU(I)
000214      IF(CABS2(OMEGD).EQ.0..AND.KOAI.NE.0.) GO TO 100
000215      IF(CABS2(OMEGD).EQ.0..AND.DFU(I).NE.0.) GO TO 100

000216      U = OMEGD*AMASS(I)/CHARG(I)
000217      AW = ABS(REAL(U))
000218      DW = 1.E-13*AW
000219      IF(ABS(AIMAG(U)).GT.DW) GO TO 103
000220      IW = IFIX(AW)
000221      100 OMEGA = OMEGA + 3.E-13*OMEGA
000222      IF(AW - IW.GT.DW.AND.IW + 1. - AW.GT.DW) GO TO 103
000223      GO TO 102
000224      103 CONTINUE
000225      C DEPOLE IS USED TO GET RID OF ZEROS IN THE DENOMINATORS
000226      102 DEPOLE = (1., 0.)
000227      IF(NDPOLE) GO TO 5
000228      DO 2 I = 1, NSPEC
000229      OMEGD = OMEGA + (0., 1.)*KYSQ*DFU(I)
000230      IF(KOAI.EQ.0.) GO TO 23
000231      IF(I.EQ.1) GO TO 22
000232      IF(DFU(I).EQ.DFU(I-1)) GO TO 23
000233      22 DEPOLE = OMEGD*DEPOLE
000234      23 IF(KMAX(I).EQ.0) GO TO 2
000235      KMX = KMAX(I)
000236      JI = KMIN(I)
000237      DO 1 J = JI, KMX
000238      1 DEPOLE = DEPOLE*(OMEGD - J/AMASS(I))
000239      2 CONTINUE
000240      C THE FACTOR QF IS PUT IN TO MAKE DEPOLE ON THE ORDER OF 1
000241      DEPOLE = DEPOLE*QF
000242      5 PMAX = 0
000243      P = 0
000244      N = 1
000245      M = 1
000246      CALL ABCALC
000247      GO = KYSQ + KXSQ
000248      DO 3 I = 1, NSPEC
000249      3 GO = GO + AP(I)*OMPSQ*CHARG(I)**2*DENSE(I)/AMASS(I)
000250      M = 2
000251      CALL ABCALC
000252      GPLUS = 0,
000253      GMINUS = 0,
000254      DO 4 I = 1, NSPEC
000255      GPLUS = GPLUS + EPSF(I)*(APP(I) + BPP(I))
000256      4 GMINUS = GMINUS + EPSF(I)*(AP(I) - BP(I))
000257      IX = (0., 2.)*3.1415926535*X
000258      EIKOX = CEXP(IX)
000259      Q = GO + EIKOX*GPLUS + GMINUS/EIKOX
000260      DQDX = 2.*PI*(EIKOX*GPLUS - GMINUS/EIKOX)*(0., 1.)
000261      D2QDX2 = -4.*PI*PI*(Q - GO)
000262      Q = Q*DEPOLE
000263      DQDX = DQDX*DEPOLE
000264      D2QDX2 = D2QDX2*DEPOLE
000265      RETURN
000266      END

```

APPENDIX J

The characteristics of the most unstable mode are shown for various values of density $\omega_{pi}^2/\omega_{ci}^2$ and density gradient $k_0 a_i$, using the local method (shown in Table I) and the nonlocal method (shown in Table II). In all cases the mirror ratio $R = 3$ and the mass ratio $m_i/m_e = 3700$. In the table headings, x_{peak} is the value of x at which $|\phi(x)|$ is greatest; Δx is the half-width of $|\phi(x)|^2$; k_x is the value of k_x at which $|\tilde{\phi}(k_x)|^2$ is greatest; and " p_{max} needed" is the minimum value of p_{max} which is needed in order for the nonlocal method to be valid [defined by requiring $|\tilde{\phi}(\pm p_{max} k_0)| < |\tilde{\phi}(k_x \text{ peak})|/4$]. The results in the two tables are seen to be in good agreement when inequality (21) is well-satisfied. The one case in which the agreement is not very good is for $\omega_{pi}^2/\omega_{ci}^2 = 1000$ and $k_0 a_i / 2\pi = 0.40$. This set of parameters is near the border between regions D and E in Figure 6. Using the local method, the "region E instability" (at higher $\text{Re } \omega$ and k_y) has a slightly higher growth rate than the "region D instability," while the reverse is true using the nonlocal method; hence the huge discrepancy between the two tables for $\text{Re } \omega$ and $k_y a_i$ with this set of parameters.

TABLE I

$\frac{\omega_{pi}^2}{\omega_{ci}^2}$	$k_0 \frac{a_i}{2\pi}$	$\frac{Im\omega_L}{\omega_{ci}}$	$\frac{Re\omega_L}{\omega_{ci}}$	$k_y \frac{a_i}{2\pi}$	$k_0 \frac{x_{peak}}{2\pi}$	$k_0 \frac{\Delta x}{2\pi}$	$\frac{k_x \text{ peak}}{k_0}$	P_{\max} needed
10000	0.015	3.55	6.75	19.4	0.56	0.010	29.1	74
	0.03	5.94	10.65	24.5	0.57	0.015	-3.2	36
	0.06	9.39	14.88	31.4	0.57	0.023	-15.9	39
	0.12	12.26	14.67	36.3	0.57	0.044	-13.8	27
	0.18	11.62	7.83	34.0	0.56	0.070	-7.0	14
	0.21	13.65	0.	22.1	0.50	0.085	-0.7	6
	0.24	12.50	0.	24.6	0.50	0.086	4.1	9
	0.27	6.75	0.	27.7	0.50	0.092	9.1	14
	0.30	3.10	0.	0.	0.	0.188	± 12.2	14
	0.35	3.18	0.	0.	0.	0.230	± 10.7	13
	0.40	6.10	30.70	27.3	0.17	0.117	5.5	9
	0.50	10.23	24.75	29.5	0.17	0.138	3.4	7
	0.60	9.35	17.79	29.0	0.18	0.169	2.6	5
	0.70	7.13	12.33	27.1	0.20	0.207	2.2	4
1000	0.015	1.35	2.65	9.8	0.61	0.019	25.8	49
	0.3	2.27	4.31	11.9	0.62	0.026	7.2	25
	0.06	3.73	6.45	14.8	0.63	0.036	-2.1	15
	0.12	5.47	7.18	17.7	0.62	0.063	-5.2	14
	0.18	5.70	4.20	17.4	0.58	0.101	-3.3	8
	0.21	6.85	0.	11.1	0.50	0.126	-0.3	4
	0.24	6.47	0.	12.8	0.50	0.124	-2.0	6
	0.27	3.57	0.	14.8	0.50	0.131	4.6	8
	0.30	1.66	0.	0.	0.	0.258	± 6.5	8
	0.35	1.63	0.	0.	0.	0.327	± 5.5	7
	0.40	3.50	16.32	15.2	0.18	0.158	3.0	6
	0.50	5.56	13.16	16.1	0.18	0.190	1.8	4
	0.60	5.06	9.53	15.7	0.19	0.231	1.6	4
100	0.015	0.49	0.86	3.4	0.63	0.035	10.4	23
	0.03	0.72	1.49	4.7	0.65	0.045	3.9	14
	0.06	1.23	2.18	5.2	0.64	0.063	-0.2	8
	0.12	1.83	2.47	6.2	0.63	0.107	-1.6	7
	0.18	1.95	1.48	6.0	0.58	0.174	-1.1	4
	0.21	1.78	0.52	5.8	0.54	0.210	-0.7	3
	0.24	2.24	0.	4.4	0.50	0.214	0.7	3
	0.27	1.25	0.	5.2	0.50	0.224	1.6	4
10	0.03	0.15	0.65	2.19	0.70	0.077	0.7	6
	0.06	0.42	0.79	1.99	0.67	0.109	-0.2	4
	0.12	0.62	0.84	1.88	0.65	0.149	-0.7	4

TABLE II

$\frac{\omega_{pi}^2}{\omega_{ci}^2}$	$k_0 \frac{a_i}{2\pi}$	$\frac{\text{Im } \omega}{\omega_{ci}}$	$\frac{\text{Re } \omega}{\omega_{ci}}$	$k_y \frac{a_i}{2\pi}$	$k_0 \frac{x_{\text{peak}}}{2\pi}$	$k_0 \frac{\Delta x}{2\pi}$	$\frac{k_x \text{ peak}}{k_0}$	p_{max} needed
10000	0.21	12.48	0.	22.0	0.50	0.10	-1	6
	0.24	11.63	0.	24.7	0.50	0.11	3	7
	0.40	3.48	29.19	29.3	0.22	0.15	5	8
	0.50	7.75	23.21	30.0	0.21	0.19	3	5
	0.60	6.75	16.25	29.7	0.22	0.24	2	4
	0.70	4.41	10.72	28.4	0.26	0.36	2	3
	0.85	2.31	0.	26.9	0.	0.27	4	5
	1.00	1.16	0.	10.6	0.	0.42	1	2
1000	0.18	5.43	4.46	17.8	0.59	0.08	-3	9
	0.21	5.63	0.	10.7	0.50	0.12	-1	5
	0.24	5.63	0.	13.1	0.50	0.14	2	4
	0.27	3.18	0.	15.2	0.50	0.18	3	6
	0.30	1.95	0.	0.	0.	0.05	±5	8
	0.35	1.81	0.	0.	0.	0.09	±5	8
	0.40	1.76	2.13	7.5	0.13	0.14	-6	9
	0.50	3.19	11.91	17.6	0.24	0.24	2	4
	0.60	2.50	7.99	16.9	0.25	0.33	1	3
	0.70	1.16	0.	4.2	0.	0.22	0	3
	0.85	1.25	0.	6.6	0.	0.31	1	2
	1.00	0.82	0.31	7.9	0.95	0.42	1	2
100	0.06	1.19	2.17	5.4	0.65	0.06	0	7
	0.12	1.71	2.52	6.6	0.66	0.09	-1	6
	0.18	1.71	1.69	6.4	0.63	0.13	-1	5
	0.21	1.50	1.04	6.2	0.60	0.16	-1	4
	0.24	1.32	0.	4.5	0.50	0.22	0	2
	0.27	0.84	0.	5.3	0.50	0.27	1	2
	0.30	0.36	1.53	3.8	0.40	0.34	1	3
	0.35	0.39	1.68	3.1	0.33	0.38	1	2
	0.40	0.42	0.83	4.6	0.07	0.25	2,-3	5
	0.50	0.38	0.78	2.3	0.22	0.18	-1	3
	0.60	0.44	0.63	3.6	0.16	0.23	-1	3
	0.70	0.54	0.	3.6	0.	0.32	0	1
	0.85	0.42	0.35	4.6	0.95	0.39	1	1
	1.00	0.35	0.45	6.3	0.93	0.38	1	1
10	0.06	0.38	0.75	2.13	0.68	0.15	0	3
	0.12	0.52	0.80	2.17	0.68	0.16	0	3
	0.18	0.47	0.64	2.20	0.68	0.20	0	3
	0.24	0.15	0.41	2.08	0.66	0.30	0	2
	0.30	stable						
	0.50	stable						
3	0.15	stable						

APPENDIX K

Derivation of Eq. (38):

$G_{\pm 1,s}(k_x, \omega)$ is given by Eq. (35) for ions in the straight-line orbit approximation and by Eq. (36) for cold electrons. We note that $G_{+1,s} = G_{-1,s}$ for the ions if $k_y = 0$, and this is also true for the electrons if $k_y = 0$ and $k_0 \ll k_x$. Then, using Eqs. (23) and (25), we have

$$D(x, k_x, \omega) = -k_x^2 + \sum_s G_{0,s}(k_x, \omega) + 2 \cos k_0 x \sum_s G_{+1,s}(k_x, \omega) \quad (K1)$$

The condition $\partial D / \partial x = 0$ from Eq. (16) can be satisfied if and only if $k_0 x = 0$ or π in Eq. (K1). We take $k_0 x = 0$. Then Eq. (16) becomes

$$-k_x^2 + \sum_s [G_{0,s}(k_x, \omega) + 2G_{+1,s}(k_x, \omega)] = 0 \quad (K2)$$

$$-2k_x + (\partial / \partial k_x) \sum_s [G_{0,s} + 2G_{+1,s}] = 0 \quad (K3)$$

evaluated at $k_x = k_L$, $\omega = \omega_L$.

For a loss cone ion distribution we have, from Eq. (11), two ion "species", with

$$n_{0,1} = R(R-1)^{-1} n_{0,i}$$

$$n_{0,2} = -(R-1)^{-1} n_{0,i}$$

$$v_1 = v_i$$

$$v_2 = v_i R^{-1/2} \quad (K4)$$

(K8)

$$\{e_2 - e_1 + i(\pi/2) \frac{1}{2} (\omega_L/k_{V1}) [R_{1/2}(e_2 + 1) - (e_1 + 1)]\} = 0$$

$$-k_L^2 [1 + \omega_{pe}^2 (1 + A_e)/\omega_{ce}^2] + (\omega_{pe}^2/v_1^2) R_{(R-1)-1}$$

Using Eqs. (K6) and (K7), Eqs. (K2) and (K3) become

$$G_{\pm 1,e} = -\omega_{pe}^2 k_x^2 A_e / 2\omega_{ce}^2$$

$$G_{0,e} = -\omega_{pe}^2 k_x^2 / \omega_{ce}^2$$

Eq. (36) gives

For the electrons, assuming $\omega \ll \omega_{ce}$, $k_0 \ll k_x$, and $k_y = 0$,

$$[\exp(-k_0 a_1^2/2) - R_{1/2} \exp(-k_0 a_1^2/2R)]$$

$$-\exp(-k_0 a_1^2/2R) + i(\pi/2) \frac{1}{2} (\omega/k_x v_1)$$

$$G_{\pm 1,i} = -(\omega_{pe}^2/v_1^2) R_{(R-1)-1} [\exp(-k_0 a_1^2/2)$$

$$G_{0,i} = -(\omega_{pe}^2/v_1^2) R_{(R-1)-1} (1-R_{1/2}) i(\pi/2) \frac{1}{2} \omega/k_x v_1$$

Putting Eq. (K4) into Eq. (K5), and assuming $A_i = 0$,

$$[1 + i(\pi/2) \omega/k_{Vs}]$$

$$G_{\pm 1,s} \approx -(\omega_{ps}^2 A/2v_s^2) \exp(-k_0 a_s^2/2)$$

$$G_{0,s} \approx -(\omega_{ps}^2/v_s^2) [1 + i(\pi/2) \frac{1}{2} \omega/k_{Vs}]$$

in Eq. (35), which becomes

For $\omega \ll k_x v_1$ (justified posteriori), we can take $G_0, G_{\pm 1} \ll 1$

$$-2k_L [1 + \omega_{pe}^2 (1 + \Delta_e) / \omega_{ce}^2] - (\omega_{pi}^2 / v_i^2) R(R-1)^{-1} \\ i(\pi/2)^{1/2} (\omega_L^2 / k_L^2 v_i^2) [R^{1/2} (e_2 + 1) - (e_1 + 1)] = 0 \quad (K9)$$

where $e_1 \equiv \exp(-k_0^2 a_i^2 / 2)$, $e_2 \equiv \exp(-k_0^2 a_i^2 / 2R)$, and Eqs. (14a) and (K4) can be used to find Δ_e

$$\Delta_e = (Re_1 - e_2)(R - 1)^{-1} \quad (K10)$$

Simultaneously solving Eqs. (K8) and (K9) for ω_L and k_L yields Eq. (38).

We now justify the assumption that $\omega \ll k_x v_i$ by using Eq. (38) to find

$$\omega_L / k_L v_i = 0.532i(e_2 - e_1) [R^{1/2} (e_2 + 1) - (e_1 + 1)]^{-1} \quad (K11)$$

For $R = 3$ and $k_0 a_i = 2$ (typical parameters for region C in Figure 6), Eq. (K11) yields $\omega_L / k_L v_i = 0.135$. The next term in the expansion of the Z function is²⁰

$$Z(\zeta) = i\pi^{1/2} - 2\zeta + \dots \quad (K12)$$

For $k_y = 0$, $\zeta_0 = \zeta_{\pm 1} = \omega/\sqrt{2} k_x v_i$ in Eq. (35), so the relative error in $Z(\zeta)$ due to finite $\omega_L / k_L v_i$ is

$$\text{Relative error} = 2\pi^{-1/2} \zeta = (2/\pi)^{1/2} \omega_L / k_L v_i = 0.108$$

Since the approximation $Z(\zeta) \approx i\pi^{1/2}$ is good to within about 10%, Eq. (38) probably good to within about 10% as well. For $m_i/m_e \leq 3700$, this error is comparable to or less than the error due to nonlocal effects (i.e. due to finite k_0/k_x), so there is no point in using Eq. (K12) to approximate the Z function.

APPENDIX L

We consider two different configurations of plasma, a slab with ion guiding center density

$$n_i(x, y) = n_0 \exp(-x^2/L^2) \quad (L1)$$

and a column with

$$n_i(x, y) = n_0 \exp(-x^2/L^2 - y^2/L^2) \quad (L2)$$

The ion distribution function is

$$\begin{aligned} f_{0i}(x, y, v_x, v_y, v_z) &= g_i(v_\perp, v_z, v_{gc}, y_{gc}) \\ &= g_i(v_\perp, v_z, x + v_y/\omega_{ci}, y - v_x/\omega_{ci}) \end{aligned} \quad (L3)$$

To apply the Penrose criterion with $k_y = k_z = 0$, at $x = 0$, we will need

$$\begin{aligned} F(v_x) &= \int dv_y dv_z f_{0i}(0, 0, v_x, v_y, v_z) \\ &= \int dv_y g_{\perp i}(v_\perp, v_y/\omega_{ci}, -v_x/\omega_{ci}) \end{aligned} \quad (L4)$$

where $g_{\perp i}(v_\perp, x, y) \equiv \int dv_z g_i(v_\perp, v_z, x, y)$.

We take $g_{\perp i}$ to be a loss cone distribution of the form given by Eq. (11). Then Eq. (L4) becomes

$$\begin{aligned} F(v_x) &= [2\pi v_i^2 (1 - R^{-1})]^{-1} \int dv_y n_i(v_y/\omega_{ci}, -v_x/\omega_{ci}) \\ &\quad [\exp(-v_\perp^2/2v_i^2) - \exp(-Rv_\perp^2/2v_i^2)] \end{aligned} \quad (L5)$$

For a slab, $n_1(x,y)$ is given by Eq. (L1), and Eq. (L5) becomes

$$F_{\text{slab}}(v_x) = (2\pi)^{-1/2} [v_i(1 - R^{-1})]^{-1} n_0$$

$$[(1 + 2v_i^2/L^2 \omega_{ci}^2)^{-1/2} \exp(-v_x^2/2v_i^2)$$

$$-(R + 2v_i^2/L^2 \omega_{ci}^2)^{-1/2} \exp(-Rv_x^2/2v_i^2)] \quad (L6)$$

For a column, $n_1(x,y)$ in Eq. (L5) is given by Eq. (L2), and

$$F_{\text{col}}(v_x) = (2\pi)^{-1/2} [v_i(1 - R^{-1})]^{-1} n_0$$

$$[(1 + 2v_i^2/L^2 \omega_{ci}^2)^{-1/2} \exp(-v_x^2/2v_i^2 - v_x^2/L^2 \omega_{ci}^2)$$

$$-(R + 2v_i^2/L^2 \omega_{ci}^2)^{-1/2} \exp(-Rv_x^2/2v_i^2 - v_x^2/L^2 \omega_{ci}^2)] \quad (L7)$$

According to the Penrose criterion, an instability occurs when

$$\int_{-\infty}^{\infty} \frac{F(0) - F(v_x)}{v_x^2} dv_x < 0 \quad (L8)$$

(The electrons are ignored since they are unimportant for this instability.)

Both Eqs. (L6) and (L7) are of the form

$$F(v_x) = A \exp(-av_x^2) - B \exp(-bv_x^2) \quad (L9)$$

Putting Eq. (L9) into inequality (L8) yields

$$A^2 a < B^2 b \quad (L10)$$

for instability. Thus the column is marginally stable, and the slab is unstable, to electrostatic perturbations with k in the x -direction, at $x = 0$, according to the Penrose criterion.

This analysis is cruder than the analysis in Appendix K since it does not find the normal modes but assumes there is a normal mode with

$\phi(x) \approx \exp(-ik_x x)$ at $x = 0$. However, it makes the physical mechanism of the instability more clear; it is due to a relative deepening of the loss cone in $F(v_x)$ as a result of $d^2 n_i / dx^2 < 0$, and $d^2 n_i / dx^2 < d^2 n_i / dy^2$.

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